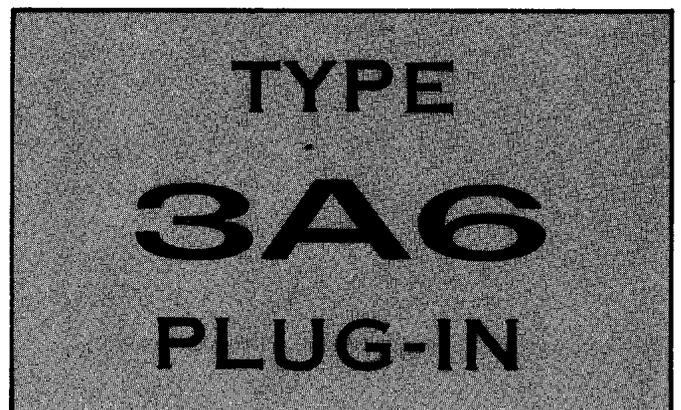


INSTRUCTION MANUAL

Serial Number _____



Tektronix, Inc.

S.W. Millikan Way • P. O. Box 500 • Beaverton, Oregon 97005 • Phone 644-0161 • Cables: Tektronix

TYPE 3A6 DUAL-TRACE AMPLIFIER

1 MEG
47 pf

VARIABLE
VOLTS/DIV

1 2 5 10

.5 .2

.1 .05 .02 .01

CALIB

POSITION

DC BAL

CH 1

AC

DC

GND

UNCAL

MODE

INV (CH 1) NORM
CH 1

CALIB

CH 2

VARIABLE
VOLTS/DIV

1 2 5 10

.5 .2

.1 .05 .02 .01

CALIB

ALTER

CHOP

ADDED

AC

DC

GND

UNCAL

DC BAL

CH 2

POSITION

DC BAL

1 MEG
47 pf

TRIGGER
CH 1 ONLY
PULL

SERIAL

TEKTRONIX, INC.
PORTLAND, OREGON, U. S. A.

SECTION 1

CHARACTERISTICS

Introduction

The Type 3A6 Dual-Trace Amplifier plug-in unit contains two identical amplifier channels. Either channel can be used independently for a single-trace display, or the two channels can be electronically switched for a dual-trace display. Also, the two channels can be added algebraically and the resultant waveform displayed on the indicator unit crt.

A signal delay line in the plug-in unit delays the signal to be displayed while the triggering signal passes to the time base undelayed. This allows the leading edge of the triggering signal to be viewed on the crt.

The Type 3A6 can be used with any of the Tektronix 560-Series Oscilloscopes* or with the Tektronix Type 129 Plug-In Unit Power Supply.

Frequency Response

Dc to 10 mc (not more than 3 db down at 10 mc) with a corresponding risetime of typically 35 nanoseconds.

Deflection Factors

Ten calibrated steps for each channel; .01, .02, .05, .1, .2, .5, 1, 2, 5 and 10 volts/division. Variable control in each channel permits continuous, uncalibrated adjustment from 0.01 to about 25 volts/division in conjunction with the step switch.

Accuracy

Within $\pm 3\%$ of indicated deflection with VARIABLE in the CALIB position.

Input Impedance

1 megohm $\pm 1\%$, paralld by about 47 pf.

Input Coupling

Ac or dc coupled, selected by front-panel switch. In the

*Cannot be used with a Type 560. Also, when used with a Type 2B67 or 3B2 time-base plug-in unit or with a Type 565 or RM565, it may not be possible to view the entire leading edge of the triggering waveform due to the delay of these time-base circuits.

AC position low-frequency response is limited to about 2 cps (0.2 cps with $10\times$ passive probe).

Maximum Input Voltage

600 volts combined dc and peak ac; 600 volts peak-to-peak ac.

Polarity Inversion

Polarity of Channel 1 can be changed to provide 180° inversion. No polarity inversion of Channel 2.

Operating Modes

Channel 1 only.

Channel 2 only.

Alternate between channels.

Chopped between channels at approximately 150 kc rate.

Added Algebraically.

Channel Isolation

50,000:1 or greater at 100 kc.

Triggering

Internal triggering signals for time base are provided from both channels or from Channel 1 only, determined by front-panel switch.

Mechanical Features

Input connectors: BNC jacks.

Construction: Aluminum alloy chassis and panel.

Accessories

Information on accessories for use with this instrument is included at the rear of the mechanical parts list.

SECTION 3

CIRCUIT DESCRIPTION

The Type 3A6 Dual-Trace Amplifier contains two identical input channels, a common output amplifier, a switching circuit, and a trigger amplifier. The output of either or both input channel amplifiers may be fed to the output amplifier, depending on the condition of the switching circuit. Thus, the switching circuit makes it possible to display one signal as a single trace on the crt, two signals alternately in a dual-trace display, or the algebraic sum or difference of two signals as a single trace. Fig. 3-1 shows a block diagram of the Type 3A6.

Input Channel Amplifier

Each input channel consists of an attenuation network, an input cathode-follower, and a two-stage push-pull amplifier with switched outputs. Input cathode followers V113 and V123 (Channel 1) and V213 and V223 (Channel 2) isolate the attenuator input circuitry from emitter followers Q133 and Q143 (Channel 1) and Q233 and Q243 (Channel 2). Q134 and Q144 (Channel 1), and Q234 and Q244 (Channel 2) drive the Output Amplifier.

The gain of the last stage in each input amplifier is set by two internal calibration adjustments: R149 (Channel 1) and R249 (Channel 2) set the gain of the stage in the .01 position of the VOLTS/DIV switches, R147 (Channel 1) and R247 (Channel 2) set the gain of the stage in the remaining posi-

tions of the VOLTS/DIV switches. The VARIABLE controls increase emitter degeneration when moved from the CALIB position.

The input attenuators are resistive dividers with capacitive compensation. The attenuators maintain an input impedance of 1 megohm paralleled by about 47 pf. With the VOLTS/DIV switches in the .01 and .02 positions, input signals are fed directly to cathode-follower stages V113 and V213. In the VOLTS/DIV switch positions which provide an input deflection factor greater than 20 mv/div (.05 to 10), the attenuator sections are stacked. In the .05 position, the 2.5× attenuator increases the basic 20 mv/div deflection factor to 50 mv/div. The 5× attenuator is used to increase the deflection factor to 100 mv/div in the .1 position. These three positions (1×, 2.5×, and 5×) are used with the 10× or 100× attenuators in the higher deflection-factor positions of the VOLTS/DIV switch.

The DC BAL controls in the grid circuit of V123 and V223 adjust the balance of each input amplifier so current does not flow through R139 (Channel 1), and R239 (Channel 2) under no-signal conditions. Otherwise, the position of a no-signal trace would shift on the crt as the VARIABLE control was turned or gain adjustments were made.

In the INV position, the INV (CH 1) NORM switch (SW155) inverts the Channel 1 output to the diode gates.

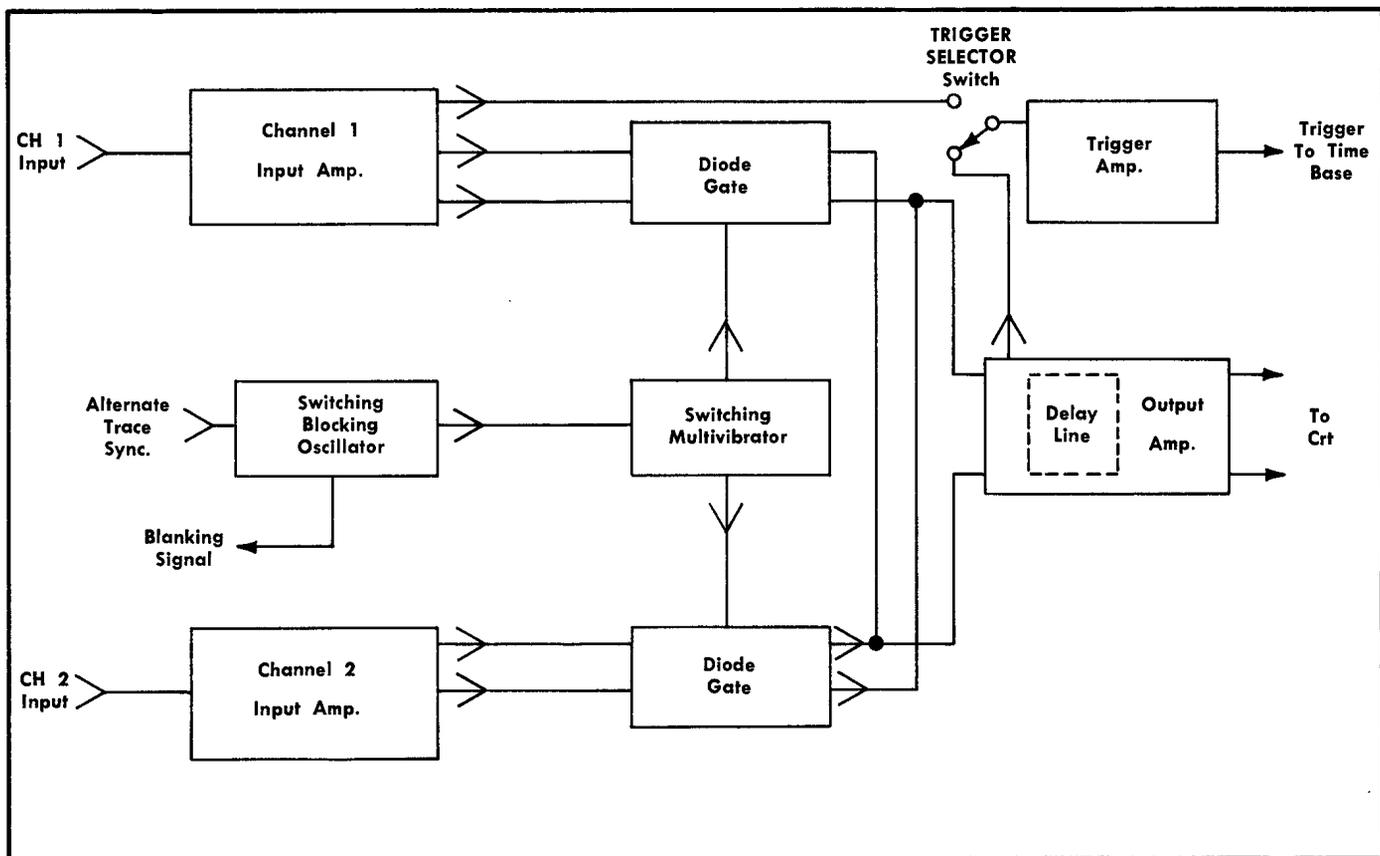


Fig. 3-1. Block diagram of Type 3A6.

Circuit Description — Type 3A6

Switching Circuit

The switching circuit consists of two diode gates, a switching multivibrator, a switching blocking oscillator, and a blanking emitter follower.

Each diode gate consists of two series diodes and two shunt diodes. In order that a signal can pass through the diode gates to the bases of Q304 and Q314 in the output amplifier, the series diodes must be forward biased, and the shunt diodes must be back biased.

In the CH 1, CH 2, and ADDED positions of the MODE switch, the switching multivibrator is inoperative (i.e. neither transistor is conducting). In the ALTER and CHOP positions of the MODE switch, the switching multivibrator operates as a bistable multivibrator. In this case, the multivibrator is switched by the blocking oscillator. The blocking oscillator operates as either a "triggered" oscillator in the ALTER mode or an "astable" (free running) oscillator in the CHOP mode.

When the MODE switch is in the CH 1 position, collector current of Q134 and Q144 flows through the series diodes. The MODE switch SW290 reverse-biases Q285 and holds it in the "off" state. Q275 is also "off", and holds the junction of D156 and D157 at -2.1 volts. Since the dc level in the signal output from Channel 1 input amplifier is -2.3 volts, the shunt diodes are back biased. The cathodes of the Channel 2 shunt diodes, D256 and D257 are held at about -4.2 volts by Q285. D256 and D257 are conducting and hold the Channel 2 output at about -3.5 volts. Since the output of the diode gates is at about -3 volts, D255 and D258 are back biased. With D255 and D258 cut off, the Channel 2 signal is not transmitted to the output amplifier. In addition, since D256 and D257 are conducting, they form a low-impedance path for any signals coming to the diode gate from the Channel 2 input amplifier.

When the MODE switch is in the CH 2 position, the conditions of the diode gate are reversed. The Channel 2 shunt diodes D256 and D257 and the Channel 1 series diodes D155 and D158 are back biased. Therefore, the signal from the Channel 2 input amplifier passes through D255 and D258 to the output amplifier and the Channel 1 signal is blocked by D155 and D158.

When the MODE switch is in either the ALTER or CHOP positions, Q275 and Q285 operate as a bistable multivibrator. Positive pulses from the switching blocking oscillator, Q260, pass through D278 or D288 to the collector of the "off" state transistor. This pulse is transmitted by either C277 or C287 to the base of the "on" transistor, turning it "off". The collector of this "off" transistor moves toward the -12.2 -volt supply, turning the other transistor "on" because of the coupling through either C277 or C287. Resistive dividers R277-R286 and R276-R287 set the levels at the transistor bases. The voltage levels allow switching action to occur when a pulse is received from the blocking oscillator.

Operation of the diode gates in ALTER and CHOP is the same as described in the CH 1 and CH 2 positions of the MODE switch. However, the multivibrator is free to switch states when it receives a trigger signal from the blocking oscillator, and thus operate the diode gates and transmit a signal to the output amplifier from Channel 1 and Channel 2 alternately. Also, in the ALTER and CHOP positions of the

MODE switch, R292 is bypassed and the collector loads, R278 and R288, of the multivibrator transistors are connected to the -12.2 -volt supply.

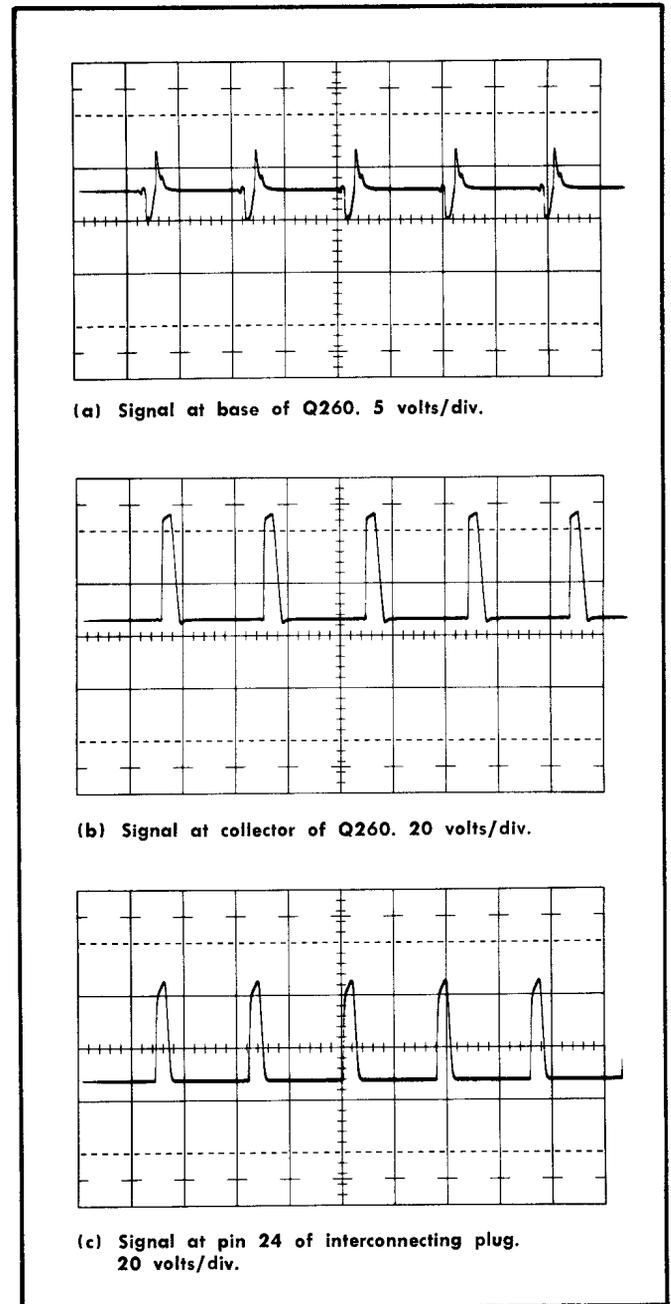


Fig. 3-2. Signals in blocking oscillator circuit. Test oscilloscope ac coupled at sweep rate of $2 \mu\text{sec}/\text{division}$.

In the CHOP and ALTER positions of the MODE switch, Q260 (switching blocking oscillator) is energized and supplies trigger pulses to the switching multivibrator. In the ALTER mode, the emitter of Q260 is connected to the -12.2 -volt supply through R261. The collector is connected to the -100 -volt supply through the collector winding of blocking oscillator transformer T263. When a positive pulse is fed from the time-base plug-in unit through terminal 3 of the interconnecting plug, the emitter voltage rises. The transistor conducts, drawing current through the collector winding of

blocking oscillator transformer T263, driving Q260 further into conduction. A normal blocking-oscillator cycle occurs, with the backswing cutting the transistor off. The transistor is biased so it does not turn on again until another sync pulse is received.

In the CHOP position of the MODE switch, the emitter of Q260 is connected to ground through R262. Normal free-running blocking oscillator action occurs. The base is forward biased since it is connected to the -12.2 -volt supply. Therefore the blocking oscillator is automatically triggered and free runs at about a 300 kc rate. Fig. 3-2 shows the blocking oscillator waveforms with the MODE switch in the CHOP position.

The positive output pulses produced by Q260 in the ALTER or CHOP position of the MODE switch are coupled to the switching multivibrator through D263 and C271. These positive pulses forward bias diode D278 or D288 to switch the multivibrator. Q260 also provides the blanking pulse to blank out the chopping transient. The emitter follower Q263 provides a fast trailing edge on the blanking pulse. Q263 is biased into operation only during the trailing edge of the blanking pulse.

When the MODE switch is in the ADDED position, current is supplied to the output amplifier through R293 and R294, holding the series diodes in both diode gates in conduction. Since the multivibrator transistors are both near cut off, the shunt diodes are back biased and thus inoperative. The signal from both Channel 1 and 2 is allowed to pass to the Output Amplifier and algebraically add or subtract depending on their polarity.

Output Amplifier

The output of the diode gate passes to the bases of Q304 and Q314. These transistors are connected as a common-emitter push-pull amplifier. The feedback networks from collector to base of Q304 and Q314 form an amplifier with low input and output impedance. R300-C300, R303-C303, R305-C305 and R307-C307 boost the gain at high frequencies to compensate for the losses in the delay line. R308 and R318 add to the low output impedance of the amplifier and match the stage to the delay line. However, the output impedance of the stage tends to increase at high frequencies. R309 and C309 are added to the circuit to compensate for this by effectively lowering the output impedance as frequency increases.

The delay line has a characteristic impedance of about 186 Ω . Signal delay through the cable is 260 nsec. The output of the delay line is coupled to the Q324-Q334, V344A-V344B stage. Since this stage has a low input impedance, R320, R321, R330, R331, C321 and C331 are added so that the delay line is terminated in its characteristic impedance.

The T-coils in the plate circuits of V344A and V344B provide high-frequency peaking. The signal from the plates of V344A and V344B are coupled directly to the control grids of the cathode followers V363A and V363B. These cathode followers drive the transistors Q364 and Q374 which in turn drive the output tubes V384 and V394. The feedback from the output stage to the bases of Q364 and Q374 reduces

the gain variation due to different tube transconductance (gm). This also increases the linear scan range of the output stage. Diodes D365 and D375 limit the voltage on the collectors of Q364-Q374 and therefore limit the dissipation of the transistors if one or the other of the output tubes (V384 or V394) cut off.

OUTPUT DC LEVEL Adjustment. This adjustment (R346) sets the operating level of the last few stages of the instrument so that the average output voltage to the deflection plates of the crt is $+190$ volts.

CALIB Adjustment. This adjustment (R389) adjusts the gain of the last stage by changing the cathode degeneration of V384 and V394. This permits the gain of the plug-in unit to be matched to the deflection factor of the indicator unit cathode-ray tube.

Trigger Amplifiers

The Type 3A6 contains a trigger amplifier to supply an internal trigger pulse to the time-base circuitry. The TRIGGER switch selects the triggering signal from either of two similar trigger pickoff amplifiers: Q164-Q174 in Channel 1 or Q404-Q414 in the Output Amplifier. Each of these trigger pickoff amplifiers is an emitter-coupled difference amplifier with double-ended input and single-ended output. The triggering signal from either pickoff amplifier circuit is obtained prior to signal delay. This allows the internal trigger signal to trigger the time-base circuitry before the vertical signal reaches the crt deflection plates.

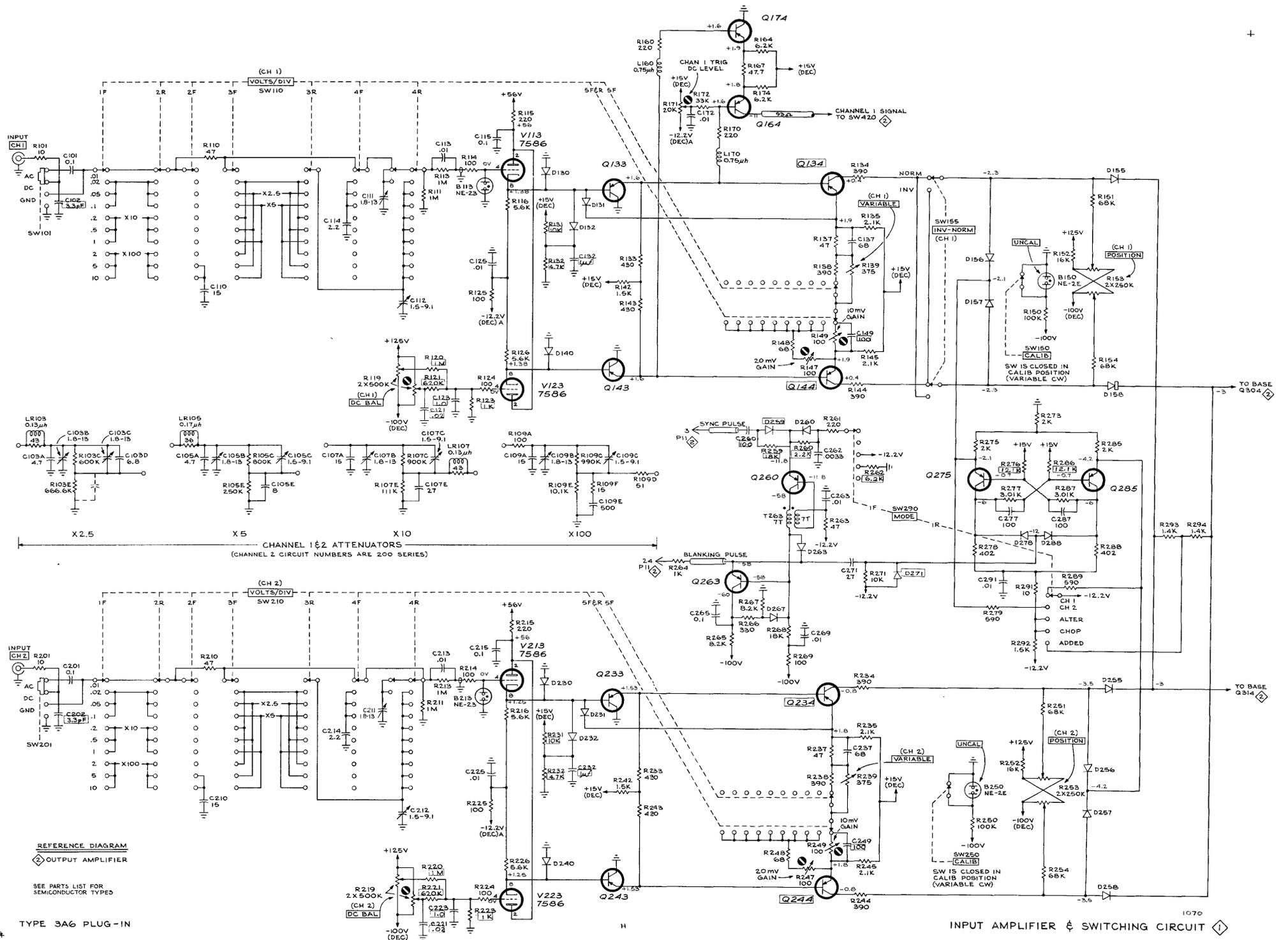
The Channel 1 trigger signal is obtained from the Q133-Q143 stage. The CHAN 1 TRIG DC LEVEL control R171 provides a means of adjusting the dc level of the Channel 1 trigger signal.

The composite trigger signal is obtained from the Q304-Q314 stage. The COMP TRIG DC LEVEL control R412 provides a means of adjusting the dc level of the composite trigger signal. The dc level of the composite trigger signal is affected by the setting of the POSITION controls. Therefore, the COMP TRIG DC LEVEL adjustment is set with the POSITION controls at midrange.

The TRIGGER switch SW420 selects the triggering signal from the output of either Q164 (Channel 1 only) or Q414 (composite). The output of the unused trigger pickoff amplifier is connected to the -12.2 supply through R420.

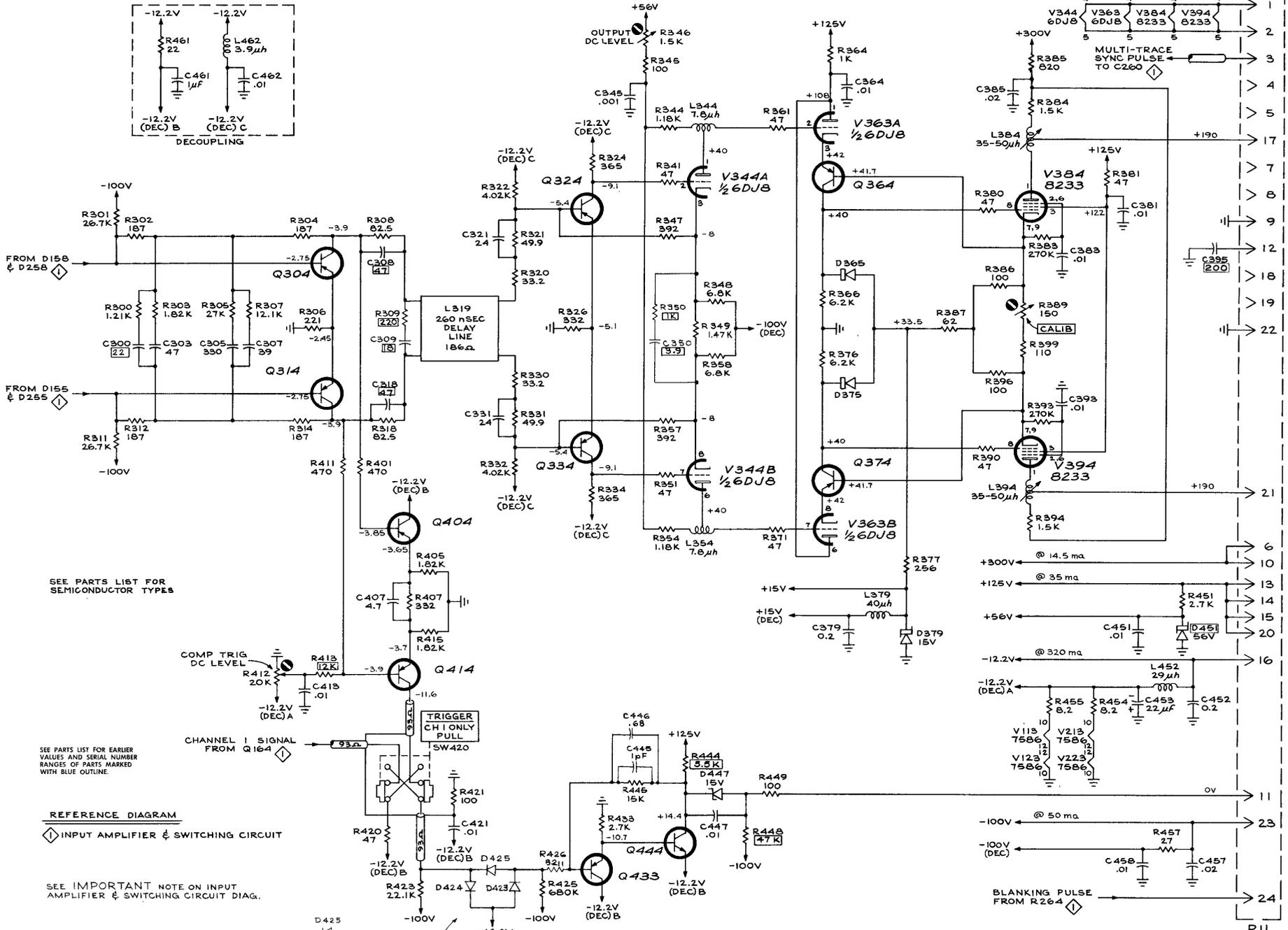
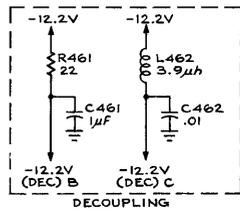
The trigger output amplifier is a low input impedance amplifier having a transimpedance of 15 k ($\Delta 3$ volt output $\div \Delta 2$ milliamp input). D425 prevents Q444 from saturating by limiting the positive input signal. D424 provides a path to the -12.2 supply when D425 limits the positive input signal. Diode D423 limits the negative voltage excursion of the input and prevents overshoot when a large trigger signal is present.

The Zener diode D447 drops the voltage level of the trigger amplifier output signal about 15 volts so that the output to pin 11 of the interconnecting plug is nominally zero volts with a no-signal trace positioned to crt center.



TYPE 3A6 PLUG-IN

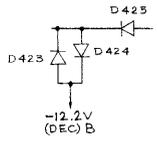
INPUT AMPLIFIER & SWITCHING CIRCUIT



SEE PARTS LIST FOR SEMICONDUCTOR TYPES

REFERENCE DIAGRAM
 ◆ INPUT AMPLIFIER & SWITCHING CIRCUIT

SEE IMPORTANT NOTE ON INPUT AMPLIFIER & SWITCHING CIRCUIT DIAG.



EFF S/N 6300

TYPE 3A6 PLUG-IN

OUTPUT AMPLIFIER 269

P11