

TA-3200F

US Model

(Serial No. 810,001 and later)

E Model

(Serial No. 510,001 and later)

Canadian Model

(Serial No. 710,001 and later)



STEREO POWER AMPLIFIER

SPECIFICATIONS

Dynamic power output: (IHF)	320 watts (8 ohms) 500 watts (4 ohms)	Inputs: Sensitivity 1.4 volts (for rated output) Impedance: 75 k ohms Two pairs of inputs equipped with level controls.
Continuous RMS power output: (rated output) (Less than 0.1 % THD)	At 1 kHz 140/140 watts (8 ohms) 200/200 watts (4 ohms) Per channel operating 110 + 110 watts (8 ohms) 130 + 130 watts (4 ohms) Both channels driven simultaneously At 20 Hz-20 kHz 100 + 100 watts/8 ohms Both channels driven simultaneously	Outputs: Accepts 4-16 ohm speakers. Equipped with two pairs of speaker outputs.
Power bandwidth: (IHF)	5 Hz-35 kHz	Power requirements: 120 volts ac (USA and Canada Model) 100, 120, 220 or 240 volts ac (General Export Model)
Harmonic distortion: (20 Hz-20 kHz)	Less than 0.1 % at rated output Less than 0.05 % at 1 watt output	Power consumption: 280 watts (USA Model) 610 watts (IEC standards) 600 VA (Canada Model)
IM distortion:	Less than 0.1 % at rated output Less than 0.03 % at 1 watt output	AC outlets: Switched 1, Unswitched 1 Total 300 watts
Frequency response:	5 Hz-200 kHz - ⁰ ₂ dB (at 1 watt output, NORMAL/TEST switch set at TEST) NORMAL setting cuts low frequencies below 30 Hz 6 dB/octave.	Dimensions: 400 (w) x 149 (h) x 323 (d) mm 15 ³ / ₄ (w) x 5 ⁷ / ₈ (h) x 12 ³ / ₄ (d) inches
S/N ratio:	110 dB, short-circuited	Net weight: 14.0 kg (30 lb 10 oz)
Residual noise:	Less than 0.003 μ watt/8 ohms	Shipping weight: 16.7 kg (36 lb 14 oz)

E Model = General Export Model

SONY
(6)
SERVICE MANUAL

SECTION 1

TECHNICAL DESCRIPTION

1-1. CIRCUIT DESCRIPTION DIGEST

The following describes the newly adopted circuit that might help you in repair work. Refer to the schematic diagram on page 11.

(1) Low Filter Switch S2

C101 and R102 form a low-cut filter 6 dB/oct below 30 Hz for eliminating extremely low frequencies when the LOW FILTER switch is set to NORMAL.

(2) Preamplifier (Q101, Q102, Q103, Q104)

This is a modified paraphase amplifier but output signal is extracted from the emitter circuit of Q102. Note that Q101 and Q102 are in a Darlington configuration and Q104 acts as a constant current source. These circuits have various advantages in a direct-coupling system. One is high stability despite temperature variation and another is high input impedance without reducing the amplifier gain. The ac output appears across R108 in the emitter circuit of Q102 while the decoupling circuit is formed by the emitter-base resistance of Q103, C104 and R109. C104 and R109 form a frequency-selective ac bypass to reduce amplifier gain at very low frequencies. Q104 keeps the dc current flow constant in Q101, Q102 and Q103, thus increasing the dc stability.

Noise Suppressor

D101 connected to Q104 reduces the popping noise due to unbalanced current flow in the following stages when the power switch is turned off.

Dc Balance

R105 provides a stabilized bias voltage for

transistor Q101 to set the output terminal voltage at zero dc. This also enables TA-3200F to provide same but opposite poled output to the load.

(3) Pre-Driver Q106

Though this stage is a conventional flat amplifier it determines the output voltage swings because the following stages are basically emitter-followers. The ac load resistor for this stage is R112 (4.7 k).

Dc Bias Adj.

Q105 is biased into conduction and operates as a small resistance providing the necessary forward bias on the two cascaded emitter followers. R116 controls the base bias of Q105, determining its emitter-collector impedance and thereby controls the dc bias voltage for the following circuit. D102 provides thermal compensation for the following complementary and power transistor circuits. D102 is attached to the power transistor heat sink to detect temperature increase in the power transistors.

(4) Protection Circuit

Two kinds of protection circuits are used in this power amplifier. One is a power transistor protection and the other is a speaker protection circuits.

Power Transistor Protection

Referring to Fig. 1-1, the protection circuit operates as follows: (Since the protection circuit is identical for positive-and negative-half cycles, only the positive half cycle operation is described.) During normal operation, Q107 and Q114 are cut off (the load impedance is 2 ohms or more) and have no effect upon power tran-

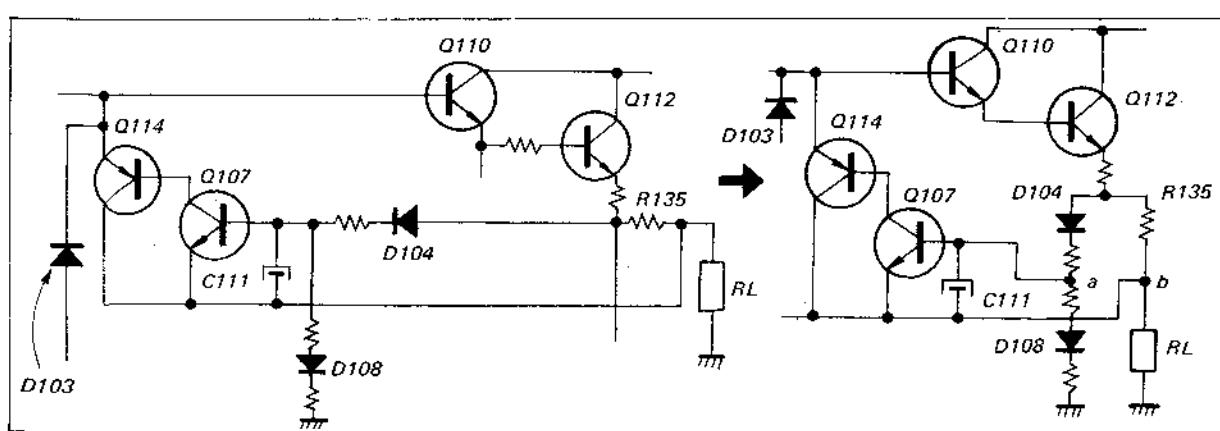


Fig. 1-1. Simplified power transistor protection circuit

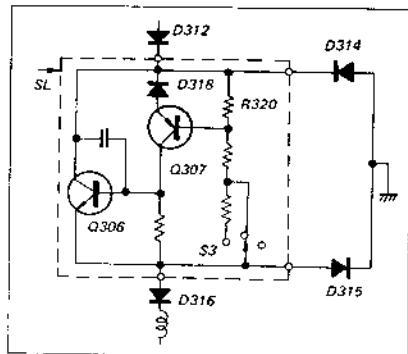


Fig. 1-5. Detail of limiter switch SL

1-2. BLOCK DIAGRAM

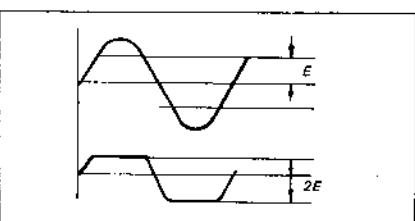
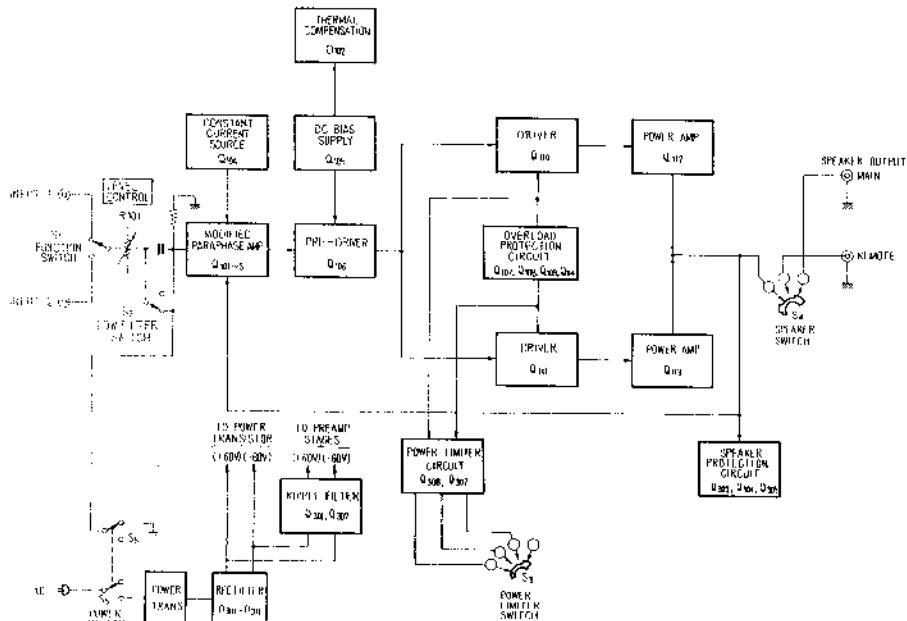


Fig. 1-6. Peak limiting operation

sistor operation because the voltage at point "a" is designed negative referred to point "b". When excessive current flows, that is the load impedance decreases extremely low value (less than 2 ohms or short), the voltage at point "a" becomes positive referred to point "b" thereby turning on Q107 and Q114. This effectively limits the input drive voltage to the power transistor and holds the current flow in the power transistor to 2A. D103 protects Q114 from break down between base and emitter during negative-half cycle when output is shorted.

Additional Power Transistor Protection Circuit

Referring to Fig. 1-2, D110, D111 form an additional power transistor protection circuit.

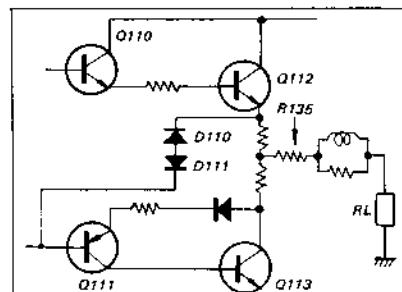


Fig. 1-2. Additional power transistor circuit

When the output terminal is shorted, zener diode D110 shorts the excessive negative half cycle drive voltage to ground through R135 and D111, limiting the drive voltage, thereby restricts excessive current flow in the power transistor Q113. D111 prevents D110 from turning on during the positive half cycle when supplying relatively high output power to the load.

Speaker Protection

In a direct-coupled power amplifier, some faults in a prior transistor cause a large unbalanced dc voltage at output terminal. This may damage a delicate speaker system. Therefore, the TA-3200F incorporates a speaker protection circuit which operates as follows: Referring to Fig. 1-3, the dc or very-low frequency component caused by transistor faults appears at output terminal and applied to the base of Q303 or Q304 through a lowpass filter (R317 or R316 and C316). Therefore Q304 or Q303 turns on corresponding to the polarity of input signal applied and short the base of Q110 (Q210)

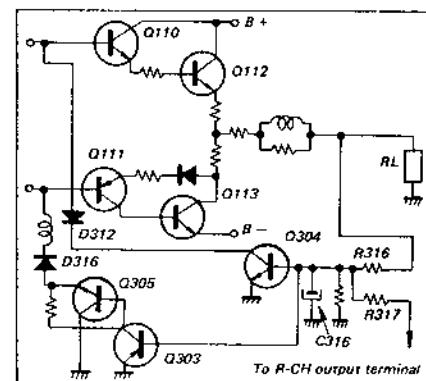


Fig. 1-3. Speaker protection circuit

or Q111 (Q211) to ground. This holds the output terminal to about 2 V dc and thus protecting the speaker system. Note that Q304 turns on due to positive input while Q303, Q305 operate due to negative input.

(S) **Power Limiter Circuit**

This determines the output power corresponding to the value selected by Power Limiter Switch S3. Referring to Fig. 1-4, this operates as a peak limiter of drive voltage as follows: When the instantaneous value of the positive drive voltage exceeds some specified value, switch SL closes and diode D312 and D315

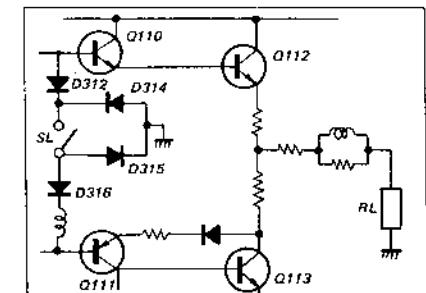


Fig. 1-4. Simplified power limiter circuit

conduct shorting the drive voltage to ground. In negative voltage case, D314 and D316 short the drive voltage. Switch SL is formed by Q306, Q307 and D318 as shown in Fig. 1-5 and operates as follows: When S3 is set to "½" or "¼", Q306 turns on only when voltage across R320 exceeds zener voltage of D318. Typical peak limiting operation is shown in Fig. 1-6.

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SECTION 2

DISASSEMBLY AND REPLACEMENT

2-6. REPLACEMENT OF COMPONENTS SECURED TO THE REAR PANEL BY RIVETS

1. Remove the rear panel as described in Procedure 2-4.
2. Bore out the rivets using a drill bit slightly larger in diameter than the rivet. See Fig. 2-4.
3. Punch out the remainder of the rivet with a nail set or prick punch.
4. Remove the defective component and then install a new one.
5. Secure the new component with a suitable screw and nut or a repair rivet screw (part number 3-701-402-00).

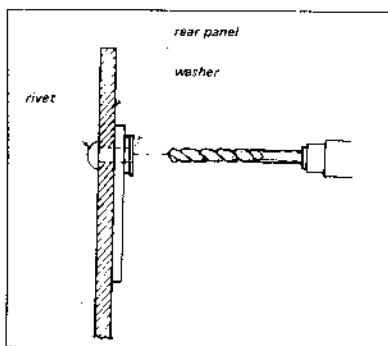
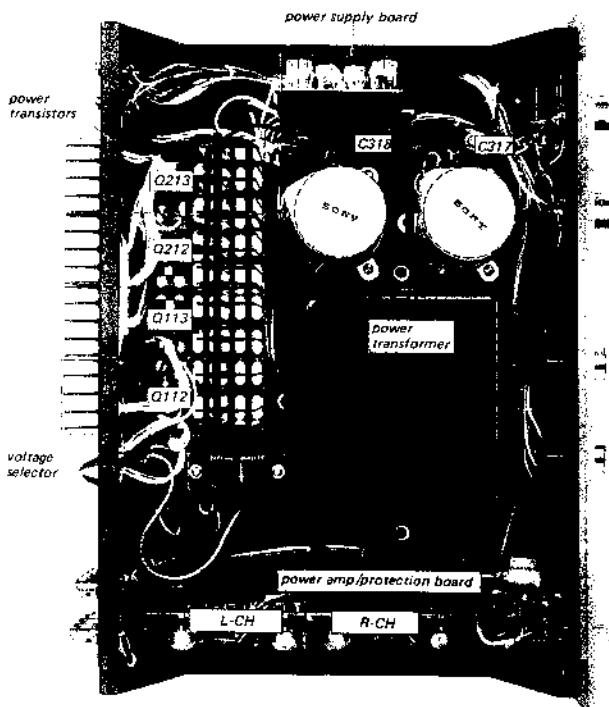


Fig. 2-4. Rivet removal

2-7. CHASSIS LAYOUT



Note: All screws in this service manual are Phillips type (cross recess type) unless otherwise indicated.

2-1. FRONT PANEL REMOVAL

1. Remove the two screws at both sides of the top cover. This frees the top cover.
2. Take out all the knobs, then remove the three screws at front top and bottom of the chassis as shown in Figs. 2-1 and 2-2. This frees the front panel.



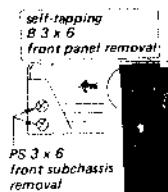
Fig. 2-1. Front panel removal

2-2. FRONT SUBCHASSIS REMOVAL

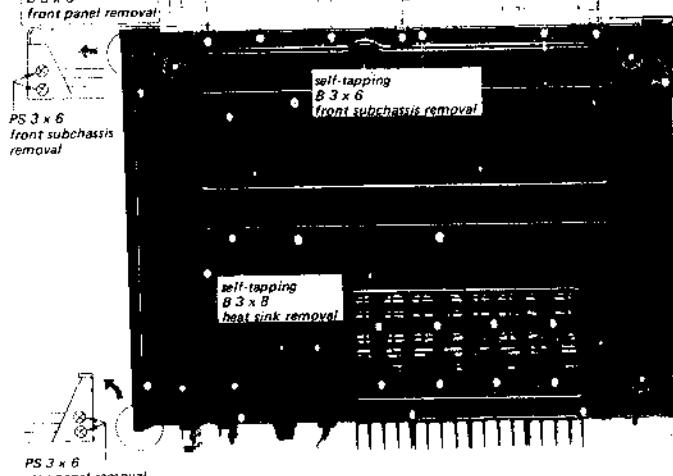
1. Remove the six screws from the bottom and two screws at both sides of the chassis as shown in Fig. 2-2. This frees the front subchassis.

2-3. CONTROL AND SWITCH REPLACEMENT

1. Remove the front panel and front subchassis as described in Procedures 2-1 and 2-2.
2. Remove the screws or nuts securing each component to the front subchassis as shown in Fig. 2-3.



PS 3 x 6
front panel removal



PS 3 x 6
front subchassis removal

PS 3 x 6

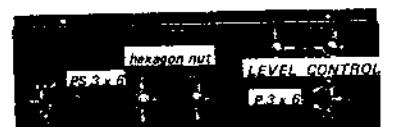


self-tapping
B 3 x 6
heat sink removal

self-tapping
B 3 x 6
rear panel removal

PS 3 x 6

Fig. 2-2. Bottom view



POWER SW SPEAKER SW POWER LIMITER SW FUNCTION SW

Fig. 2-3. Switch and control replacement

2-4. REAR PANEL REMOVAL

1. Remove the five screws at rear bottom and two screws at both sides of the chassis as shown in Fig. 2-2. This frees the rear panel.

2-5. POWER TRANSISTOR REPLACEMENT

1. Remove the heat sink on which the defective power transistor is mounted by taking out the screws as required shown in Fig. 2-2.
2. Always remove the pair of heat sinks when replacing or checking the power transistors mounted on one of them as the signal harness restricts the heat sink movement.
3. When replacing the power transistor, apply a coating of heat-transferring silicone grease to both sides of the mica washer. Any excess grease, squeezed out when the mounting screws are tightened, should be wiped off with a clean cloth to prevent the accumulation of conductive dust particles that might eventually cause a short.

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SECTION 4 REPACKING

The TA-3200F original shipping carton and packing materials are the ideal containers for shipping the unit. However to secure the maximum protection,

the TA-3200F must be repacked in these materials precisely as before. The proper repacking procedures are shown in Fig. 4-1.

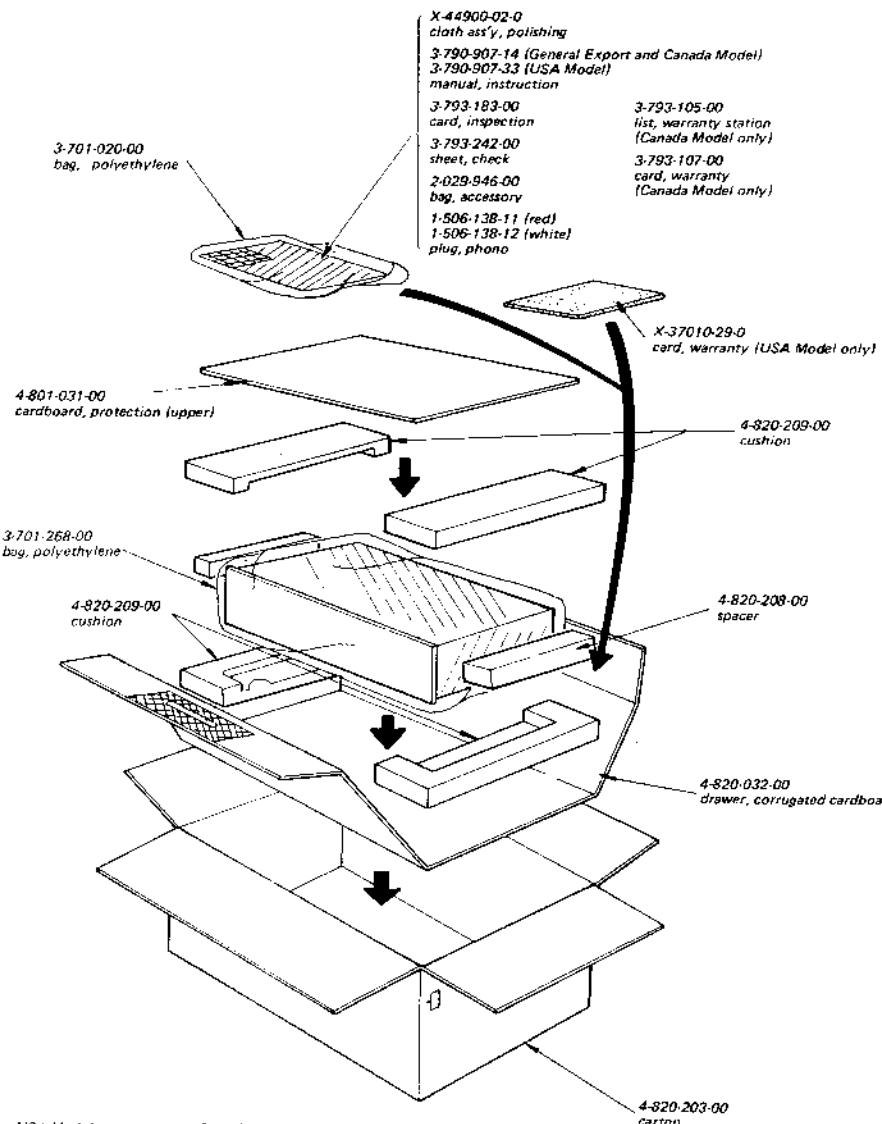


Fig. 4-1. Repacking

Note: USA Model Serial No. 810,001 and later
 General Export Model Serial No. 510,001 and later
 Canada Model Serial No. 710,001 and later

SECTION 3 ADJUSTMENTS

Note: There are two adjustments in the power amplifier, a dc-bias adjustment and a dc-balance adjustment. These adjustment should be alternately repeated two or three times after replacing any of the transistors in the power amplifier until the best operation is obtained.

3-1. DC BIAS ADJUSTMENT

Serious deficiencies in performance, such as break down or thermal runaway of power transistors, will result if this adjustment is improperly made.

CAUTION

To avoid accidental power transistor damage, increase the ac line voltage gradually (using a variable transformer) while measuring the voltage across the test points as shown in Fig. 3-1. Check to see that the reading does not exceed 26 mV. If it does, turn off the power immediately, then check and repair the trouble in the circuit board.

Test Equipment Required

1. Dc millivoltmeter
2. Variable transformer

Procedure

1. Connect the dc millivoltmeter across the test points on the circuit board, as shown in Fig. 3-1.

2. Set the adjustable resistors (screwdriver-adjust potentiometers) as follows:
 R116 (L-CH, dc bias) fully counterclockwise
 R216 (R-CH, dc bias) fully counterclockwise
 R105, R205 (dc balance) . . . midposition

3. Turn on the POWER switch, then increase the line voltage up to the rated value.
4. Adjust R116, R216 to obtain a 25 mV reading on the meter, and then make the dc balance adjustment.

3-2. DC BALANCE ADJUSTMENT

Harmonic distortion at high levels will result if this adjustment is improperly made.

Test Equipment Required

1. Dc null meter or dc millivoltmeter
2. Screwdriver, with 3 mm ($\frac{1}{8}$ ") blade

Procedure

1. Connect the dc null-meter or millivoltmeter to the speaker output terminal.
2. Turn the POWER switch to ON, and then adjust R105 (R205) to obtain a 0V reading on the meter.
3. After 10 minutes warm-up, alternately repeat this and the dc bias adjustment two or three times.

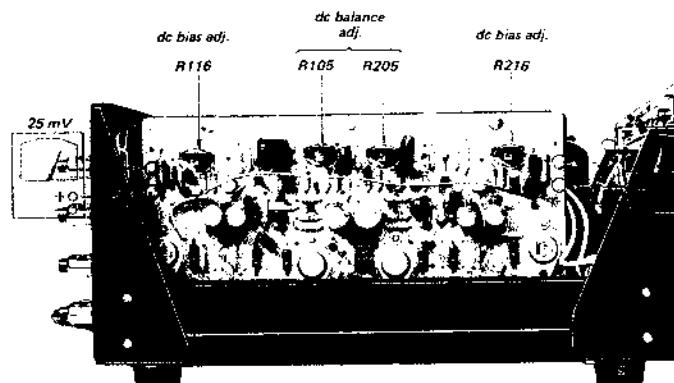
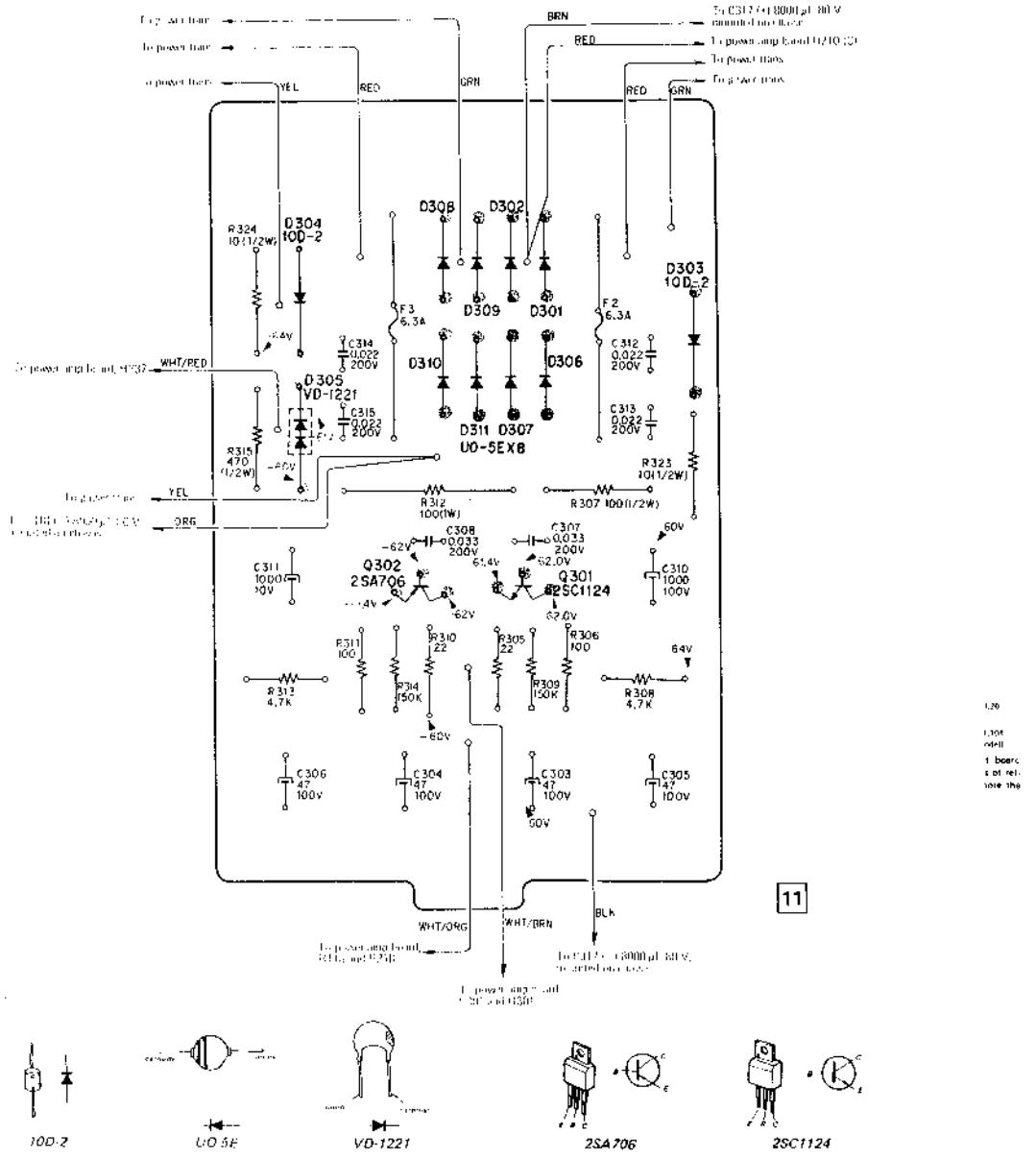


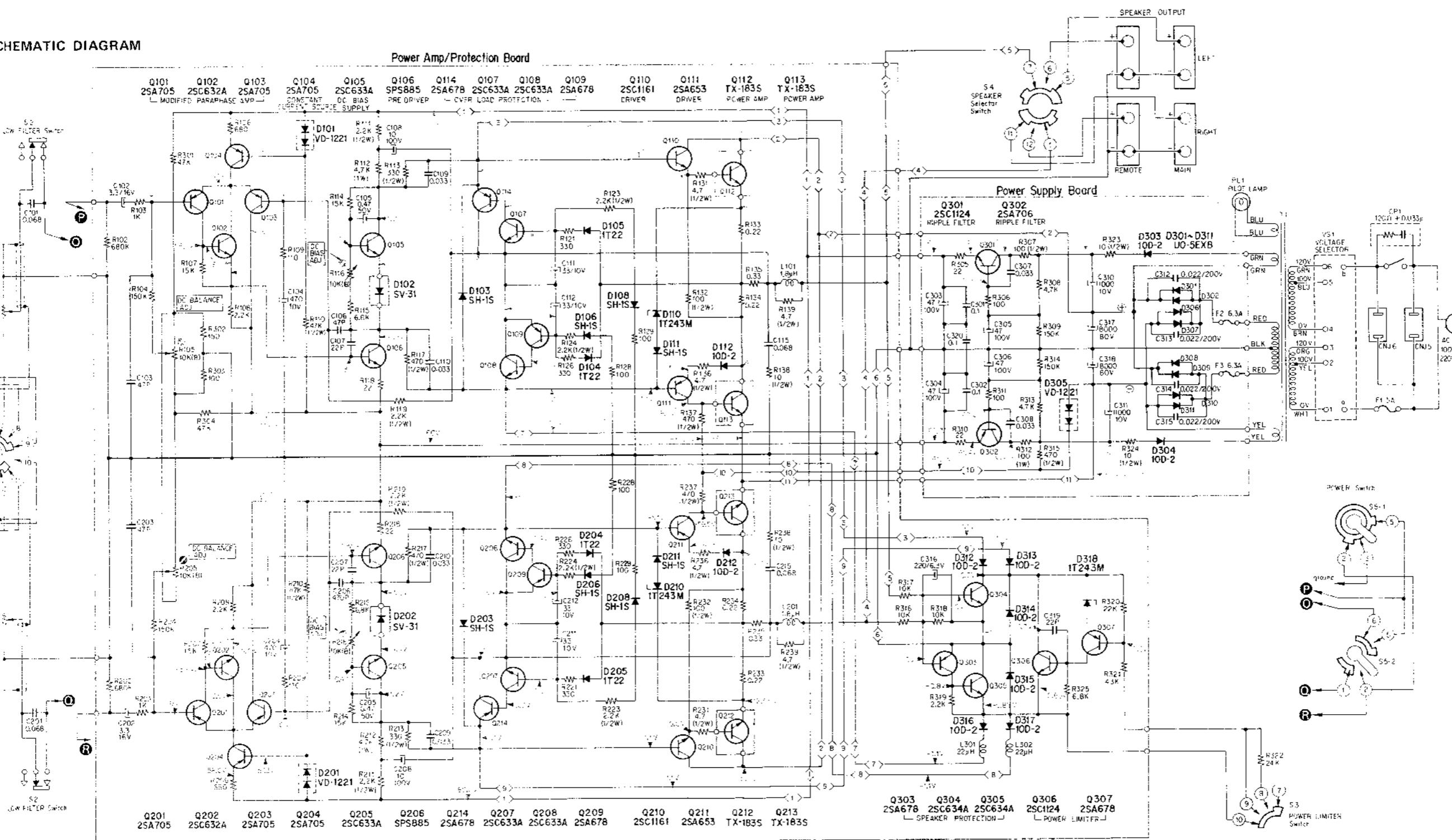
Fig. 3-1. Connection point of dc millivoltmeter and adjustment parts location

SECTION 5 DIAGRAMS

5-1. MOUNTING DIAGRAM – Power Supply Board –

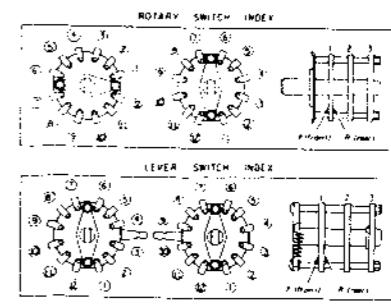


5.3. SCHEMATIC DIAGRAM



<u>Ref. No.</u>	<u>Description</u>	<u>Position</u>
S1	FUNCTION SW (1-2)	1
S2	LOW FILTER SW (TEST-NORMAL)	TEST
S3	POWER LIMITER SW (FULL-1/4)	FULL
S4	SPEAKER SW (MAIN-REMOTE)	MAIN
S5	POWER SW	OFF

Note: All resistance values are in ohms. $k = 1,000$.
 $M = 1,000 \text{ k}$.
All capacitance values are in μF except as indicated with p, which means $\mu\mu\text{F}$.
All voltages are dc measured with a VOM having 20 k ohms/volt input impedance. No signal in.
Voltage variations may be noted due to normal production tolerances.

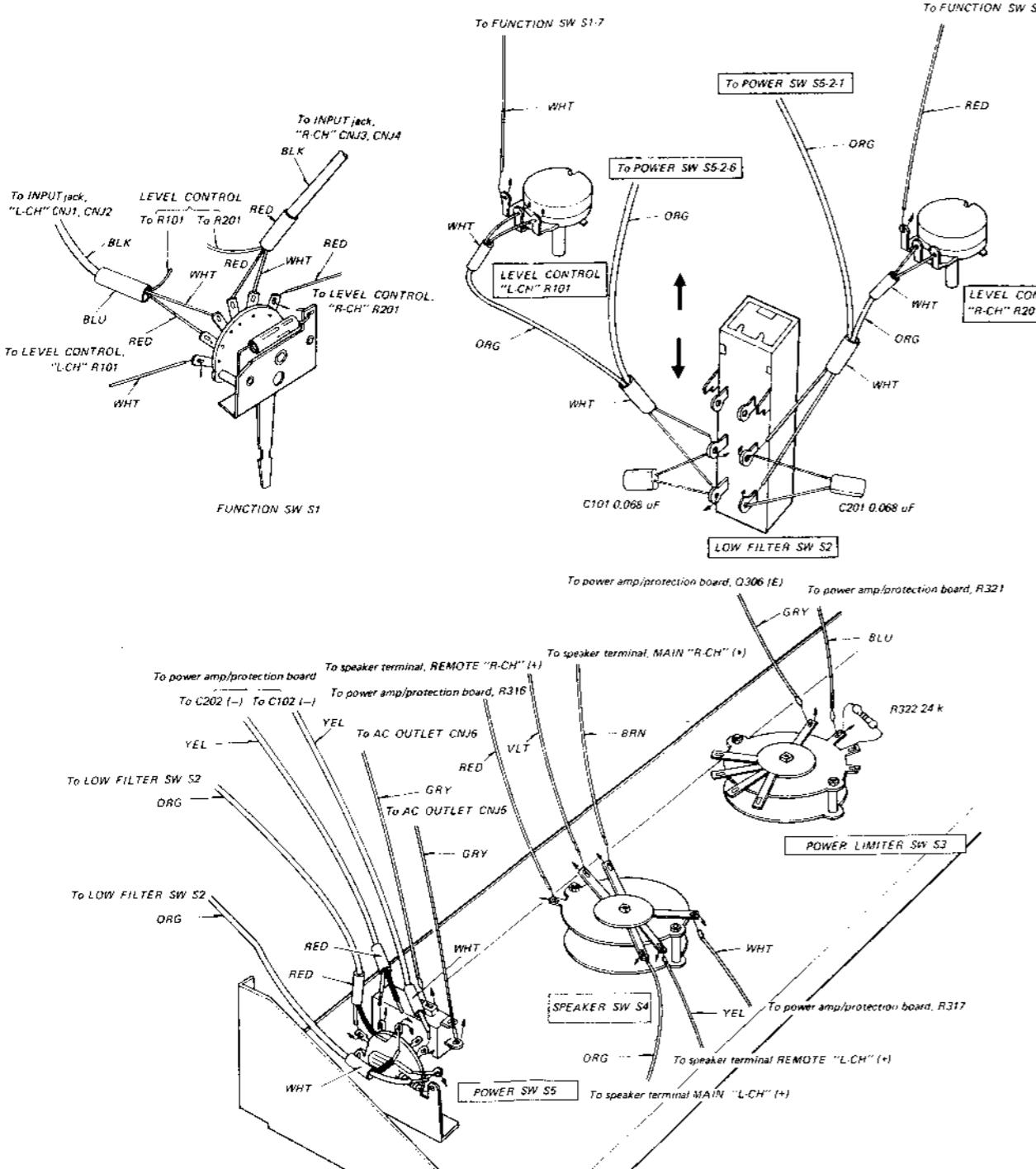


SECTION 6 EXPLODED VIEWS

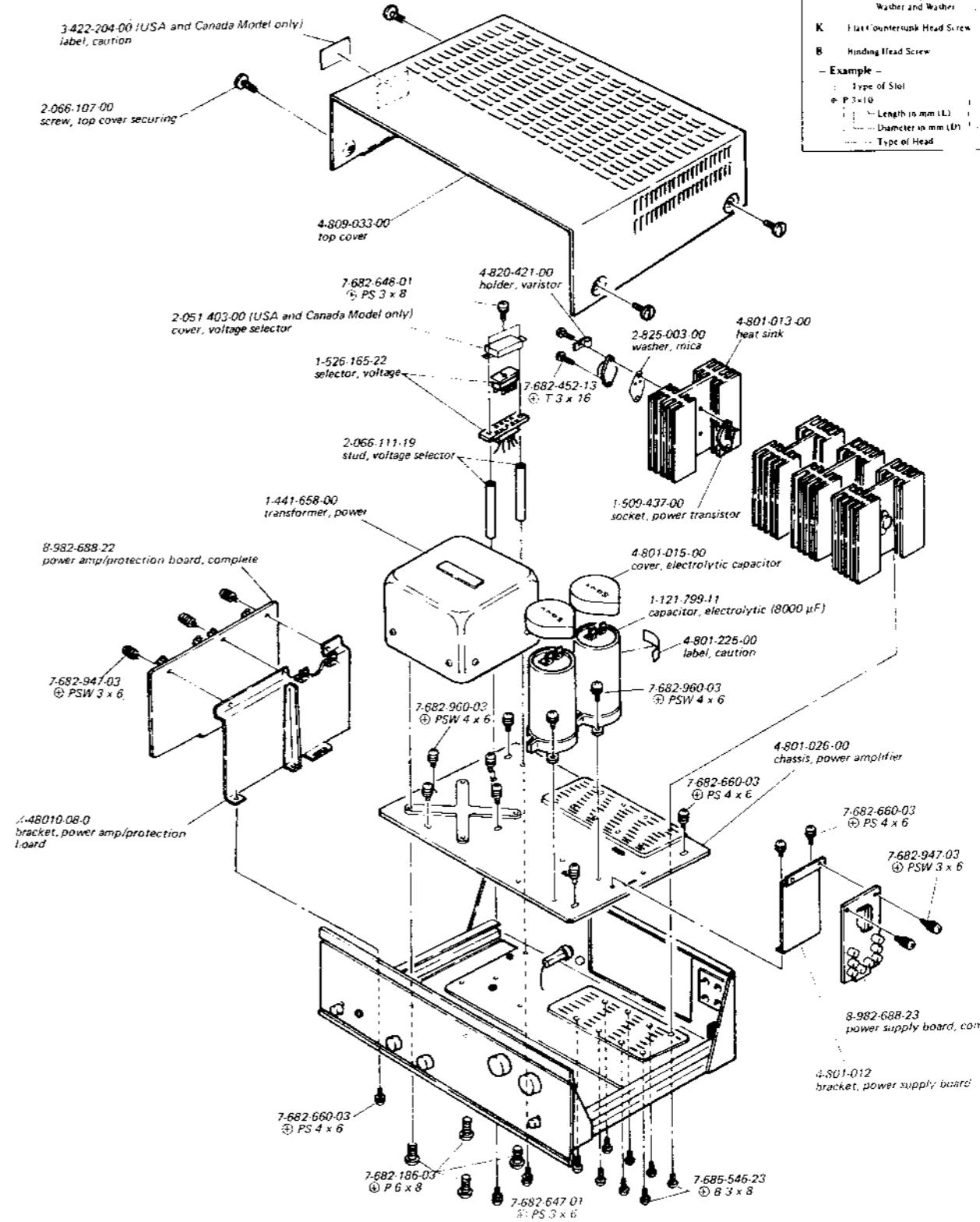
Note:
 USA Model Serial No. 810,001 and later
 General Export Model Serial No. 510,001 and later
 Canada Model Serial No. 710,001 and later

5-4. WIRING DIAGRAM

— Front Panel —

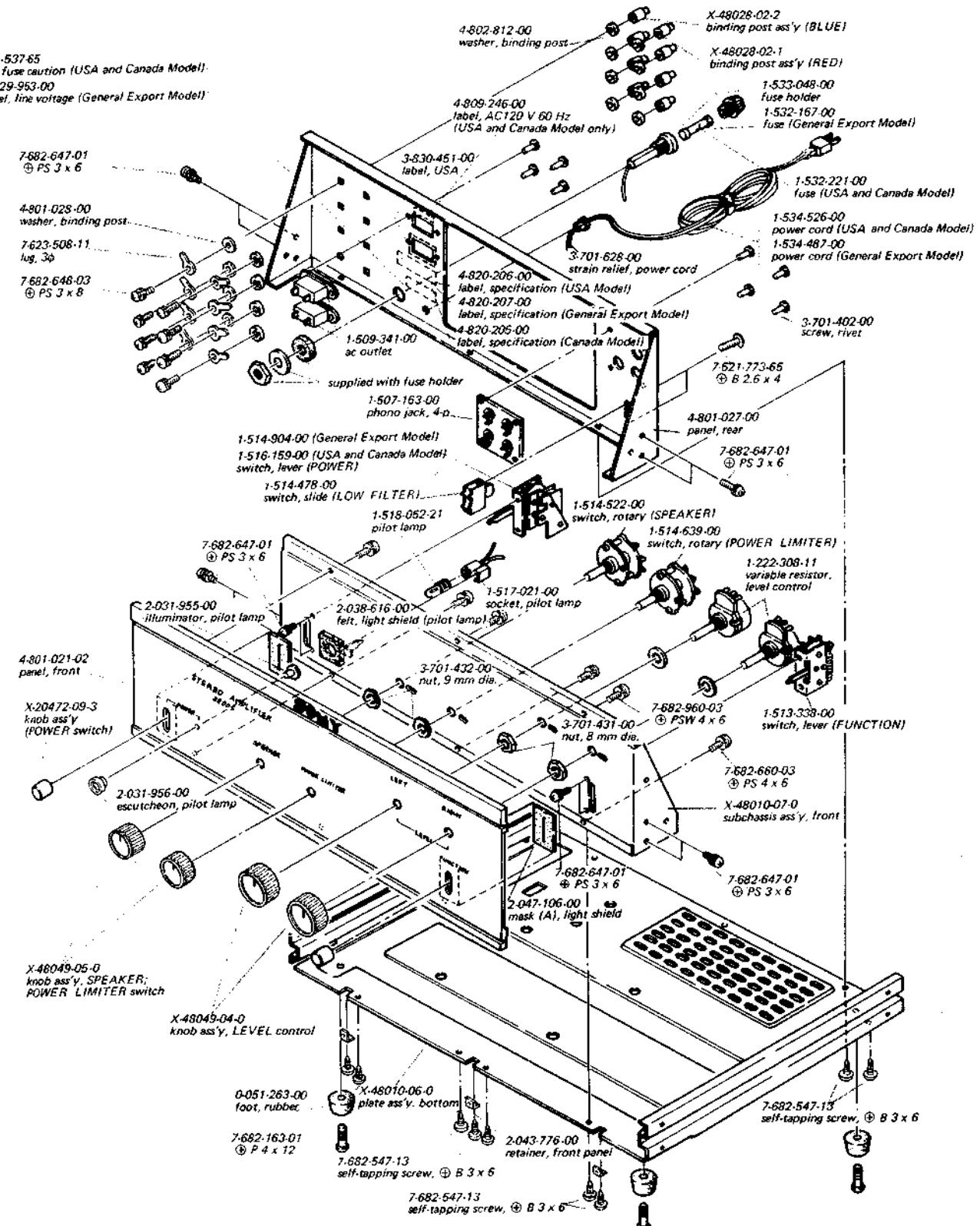


(1)



Hardware Nomenclature	
P	Pan Head Screw
PS	Pan Head Screw with Spring Washer
PSW	Pan Head Screw with Spring Washer and Washer
K	Flat Countersunk Head Screw
B	Holding Head Screw
— Example —	
— Type of Slot	— Length in mm (L)
— P 3x10	— Diamet in mm (D)
— — —	— Type of Head

(2)





SECTION 7
ELECTRICAL PARTS LIST

Note:

USA Model Serial No. 810,001 and later
 General Export Model Serial No. 510,001 and later
 Canada Model Serial No. 710,001 and later

<u>Ref. No.</u>	<u>Part No.</u>	<u>Description</u>	<u>Ref. No.</u>	<u>Part No.</u>	<u>Description</u>	<u>Ref. No.</u>	<u>Part No.</u>	<u>Description</u>	<u>Ref. No.</u>	<u>Part No.</u>	<u>Description</u>
COMPLETE CIRCUIT BOARDS											
B-982-688-22	power amp/protection board		Q301	transistor	2SC1124	C319	I-102-967-11	22 p $\pm 10\%$ 50 V ceramic	R308	I-244-689-11	4.7 k
8-982-688-23	power supply board		Q302	transistor	2SA706	C320	I-105-685-12	0.1 $\pm 10\%$ 50 V mylar	R309	I-244-725-11	150 k
SEMICONDUCTORS			Q303	transistor	2SA678	RESISTORS					
D101(D201)	diode	VDI221	Q304	transistor	2SC634A	R101(R201) I-222-308-11	150 k (B), variable (LEVEL control)	R310	I-244-633-11	22	
D102(D202)	diode	SV-31	Q305	transistor	2SC634A	R102(R202) I-244-741-11	680 k	R311	I-244-649-11	100	
D103(D203)	diode	SH-1S	Q306	transistor	2SC1124	R103(R203) I-244-673-11	1 k	R312	I-206-081-11	100	
D104(D204)	diode	SH-1S	Q307	transistor	2SA678	R104(R204) I-244-725-11	150 k	R313	I-244-689-11	4.7 k	
D105(D205)	diode	SH-1S	TRANSFORMER & INDUCTORS			R105(R205) I-221-967-11	10 k (B), adjustable (dc balance)	R314	I-244-725-11	150 k	
D106(D206)	diode	SH-1S	T1	I-441-658-00	transformer, power	R106(R206) I-244-669-11	680	R315	I-202-565-11	470	
D107(D207)	diode	SH-1S	CAPACITORS			R107(R207) I-244-701-11	15 k	R316	I-244-697-11	10 k	
D108(D208)	diode	SH-1S	All capacitors are in μ F except as indicated with p, which means $\mu\mu$ F.			R108(R208) I-244-681-11	2.2 k	R317	I-244-697-11	10 k	
D109(D209)	diode	SH-1S				R109(R209) I-244-650-11	110	R318	I-242-697-11	10 k	
D110(D210)	diode	1T243M				R110(R210) I-202-613-31	47 k $\frac{1}{2}$ W carbon	R319	I-242-681-11	2.2 k	
D111(D211)	diode	SH-1S				R111(R211) I-244-881-11	2.2 k $\frac{1}{2}$ W carbon	R320	I-242-705-11	22 k	
D112(D212)	diode	10D-2				R112(R212) I-206-101-11	4.7 k 1 W metal-oxide	R321	I-242-712-11	43 k	
D301	diode	UO-5E	C101(C201) I-105-683-12	0.068 $\pm 10\%$ 50 V mylar	R113(R213) I-202-564-11	330 $\frac{1}{2}$ W composition	R322	I-244-706-11	24 k		
D302	diode	UO-5E	C102(C202) I-131-197-11	3.3	R114(R214) I-244-701-11	15 k	R325	I-242-693-11	6.8 k		
D303	diode	10D-2	C103(C203) I-101-881-11	47 p $\pm 10\%$ 50 V ceramic	R115(R215) I-244-693-11	6.8 k	SWITCHES				
D304	diode	10D-2	C104(C204) I-121-425-11	470	R116(R216) I-221-967-11	10 k (B), adjustable (dc bias)	S1	I-513-338-00	lever (FUNCTION)		
D305	diode	VD-1221	C105(C205) I-121-726-11	0.47	R117(R217) I-202-565-11	470 $\frac{1}{2}$ W composition	S2	I-514-478-00	slide (LOW FILTER)		
D306	diode	UO-5E	C106(C206) I-101-881-11	47 p $\pm 10\%$ 50 V ceramic	R118(R218) I-244-633-11	22	S3	I-514-639-00	rotary (POWER LIMITER)		
D307	diode	UO-5E	C107(C207) I-102-967-11	22 p $\pm 10\%$ 50 V ceramic	R119(R219) I-244-881-11	2.2 k $\frac{1}{2}$ W carbon	S4	I-514-522-00	rotary (SPEAKER)		
D308	diode	UO-5E	C108(C208) I-123-080-11	10	R120(R220) -----	-----	S5	I-514-904-00	lever/rotary (POWER) (General Export Model)		
D309	diode	UO-5E	C109(C209) I-105-679-12	0.033 $\pm 10\%$ 50 V mylar	R121(R221) -----	-----	I-516-159-00	lever/rotary (POWER) (USA and Canada Model)			
D310	diode	UO-5E	C110(C210) I-105-679-12	0.033 $\pm 10\%$ 50 V mylar	R122(R222) -----	-----	MISCELLANEOUS				
D311	diode	UO-5E	C111(C211) I-121-402-11	33	R123(R223) I-202-581-11	2.2 k $\frac{1}{2}$ W composition	CPI	I-231-057-00	encapsulated component, 120 Ω + 0.033 μ F		
D312	diode	10D-2	C112(C212) I-121-402-11	33	R124(R224) I-202-581-11	2.2 k $\frac{1}{2}$ W composition	CNJ1,2,3,4	I-507-163-00	jack, phono, 4-p		
D313	diode	10D-2	C113(C213) -----	-----	R125(R225) -----	-----	CNJ5,6	I-509-341-00	outlet, ac		
D314	diode	10D-2	C114(C214) -----	-----	R128(R228) I-244-649-11	100	F1	I-532-167-00	fuse, 5 A (General Export Model)		
D315	diode	10D-2	C115(C215) I-105-683-12	0.068 $\pm 10\%$ 50 V mylar	R129(R229) I-244-649-11	100	F2,3	I-532-221-00	fuse, 5 A (USA and Canada Model)		
D316	diode	10D-2	C301	I-105-725-12	0.1 $\pm 10\%$ 100 V mylar	R130(R230) -----	-----	I-532-227-00	fuse, 6.3 A (USA and Canada Model)		
D317	diode	10D-2	C302	I-105-725-12	0.1 $\pm 10\%$ 100 V mylar	R131(R231) I-202-517-11	4.7 $\frac{1}{2}$ W composition	I-532-256-00	fuse, 6.3 A (General Export Model)		
D318	diode	1T243M	C303	I-123-083-11	47	R132(R232) I-202-549-11	100 $\frac{1}{2}$ W composition	PLI	I-518-052-21	lamp, pilot 2.5 V	
Q101(Q201)	transistor	2SA705	C304	I-123-083-11	47	R133(R233) I-217-156-11	0.22 5 W metal	VSI	I-526-165-22	selector, voltage	
Q102(Q202)	transistor	2SC632A	C305	I-123-083-11	47	R134(R234) I-217-156-11	0.22 5 W metal	I-506-346-00	connector		
Q103(Q203)	transistor	2SA705	C306	I-123-083-11	47	R135(R235) I-217-157-11	0.33 5 W metal	I-535-055-00	connector		
Q104(Q204)	transistor	2SA705	C307	I-105-679-12	0.033 $\pm 10\%$ 50 V mylar	R136(R236) I-202-517-11	4.7 $\frac{1}{2}$ W composition	I-509-437-00	socket, power transistor		
Q105(Q205)	transistor	2SG633A	C308	I-105-679-12	0.033 $\pm 10\%$ 50 V mylar	R137(R237) I-202-565-11	470 $\frac{1}{2}$ W composition	I-517-021-00	socket, pilot lamp		
Q106(Q206)	transistor	SPS885	C309	-----	-----	R138(R238) I-202-525-11	10 $\frac{1}{2}$ W composition	I-533-048-00	holder, fuse		
Q107(Q207)	transistor	2SC633A	C310	I-121-736-11	1.000	R139(R239) I-202-517-11	4.7 $\frac{1}{2}$ W composition	I-534-487-00	cord, power (General Export Model)		
Q108(Q208)	transistor	2SG633A	C311	I-121-736-11	1.000	R301	I-244-713-11	47 k	I-534-526-00	cord, power (USA and Canada Model)	
Q109(Q209)	transistor	2SA678	C312	I-105-757-12	0.022 $\pm 10\%$ 200 V mylar	R302	I-244-653-11	150	I-536-353-00	terminal post, U-shaped	
Q110(Q210)	transistor	2SC1161	C313	I-105-757-12	0.022 $\pm 10\%$ 200 V mylar	R303	I-244-649-11	100	I-536-354-00	terminal post	
Q111(Q211)	transistor	2SA653	C314	I-105-757-12	0.022 $\pm 10\%$ 200 V mylar	R304	I-244-713-11	47 k			
Q112(Q212)	transistor	TX183S	C315	I-105-757-12	0.022 $\pm 10\%$ 200 V mylar	R305	I-244-633-11	22			
Q113(Q213)	transistor	TX183S	C316	I-123-419-11	220	R306	I-244-649-11	100			
Q114(Q214)	transistor	2SA678	C317	I-121-799-11	8,000	R307	I-211-614-11	100 $\frac{1}{2}$ W carbon			
			C318	I-121-799-11	8,000						