TA-1130

ISO

Set using ISO screws

General Export Model

GEP Model

NEP Model

SONY®

SERVICE MANUAL

TABLE OF CONTENTS

SECTION 1
TECHNICAL DESCRIPTION

1-1. TECHNICAL SPECIFICATIONS

Technical specifications for the TA-1130 are given in Table 1-1.

TABLE 1-1. SPECIFICATIONS

Power Amplifier Section

Dynamic power output:	230 watts (4 ohms), both channels operating
(IHF constant power supply method)	200 watts (8 ohms), both channels operating
Continuous RMS power:	70 watts (4 ohms) per channel, both channels operating 65 watts (8 ohms) per channel, both channel operating
20 Hz to 20 kHz power output:	50 watts (8 ohms) both channels operating
Power bandwidth:	7 Hz to 30 kHz, IHF
Harmonic distortion: (20 Hz ~ 20 kHz)	Less than 0.1% at 1 kHz at rated output Less than 0.05% at 1 watt output
IM distortion: (60 Hz: 7 kHz = 4 : 1)	Less than 0.1% at rated output Less than 0.05% at 1 watt output
Frequency response:	10 Hz to 200 kHz ($\pm^{0}_{2}$ dB) at 1 watt output
Signal-to-noise ratio:	Greater than 110 dB (shorted input, weighting network A)
Residual noise:	Less than 0.008μW
Input sensitivity and impedance:	1V for rated output, 90 k ohms (POWER AMP INPUT)

Preamplifier Section

Frequency response:	PHONO 1, 2	RIAA curve ±0.5 dB
	TAPE	10Hz to 100kHz
	REC/PB	10Hz to 100kHz
	AUX1,2,3	10Hz to 100kHz
	TUNER	10Hz to 100kHz
Input sensitivity and impedance:	PHONO 1, 2	1.2 mV, 47 k
	TUNER	130 mV, 100 k
	TAPE	130 mV, 100 k
	REC/PB	130 mV, 100 k
	AUX 1,2,3	130 mV, 100 k
Signal output and impedance:	REC OUT	150 mV, 10 k
	REC/PB out	30 mV, 82 k
	PRE OUT	1 V, 5 k
Signal-to-noise ratio:	PHONO 1, 2	greater than 70 dB (weighting network A)
	TAPE: REC/PB: AUX 1,2,3:	greater than 90 dB (weighting network A)
Tone controls:	BASS	±10dB at 100 Hz (10 steps by 2 dB each)
	TREBLE	±10 dB at 10 kHz (10 steps by 2 dB each)
Filters:	HIGH	6 dB/oct, above 7 kHz
	LOW	6 dB/oct, below 100 Hz
Loudness control:	+8 dB at 50 Hz, +3 dB at 10 kHz (with 30 dB attenuation)	
Harmonic distortion:	Less than 0.1% at 1 kHz at rated output	
IM distortion: (60 Hz : 7 kHz = 4 : 1)	Less than 0.1% at rated output	

General

Power consumption:	Approx. 280 watts (GEP and General Export Model) Approx. 210 watts (NEP Model)
Power requirement:	100, 117, 220 or 240 volts, 50/60 Hz ac
Dimensions:	400 mm (width) × 149 mm (height) × 327 mm (depth) 15¾"(width) × 5⅞"(height) × 12⅞"(depth)
Net weight:	13 kg (28 lb 11 oz)
Shipping weight:	14.9 kg (32 lb 14 oz)

1-2. DETAILED CIRCUIT ANALYSIS

The following describes the function or operation of all stages and controls. The text sequence follows signal paths. Stages are listed by transistor reference designation at the left margin; major components are also listed in a similar manner. Refer to the block diagram on page 8 and the schematic diagram on pages 25 to 28.

Stage/Control	*Function*
Preamplifier Section	
Equalizer amplifier Q101, Q102	This direct-coupled two-stage amplifier (FET-NPN) amplifies the small signal provided by the phono cartridge to the level required at the input of the following tone-control amplifier. An FET has an high input impedance and generates less noise than conventional silicon transistors. Therefore, FETs are employed in the preamplifier stages. The FETs used in the preamplifier stages are selected according to their Idss rank, and care should be taken to use replacement FETs with the exact same Idss rank. Idss rank is indicated by the identification number, as illustrated in Fig. 1-1.

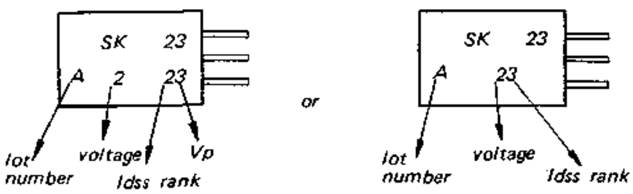


Fig. 1-1 Example of Idss rank

Stage/Control	*Function*
Bias circuit R110, R109 R102	Dc bias voltage for Q101 is extracted from R110 in the emitter circuit of Q102 and fed back to the gate of Q101 through R109 and R102. This dc negative feedback technique provides stable operation.
Equalization circuit R111, R112, R113, R104 C107, C108, C109	RIAA equalization is achieved by the negative-feedback loop containing R111, R112, R113, R104, C107, C108 and C109. Be sure to use replacement components with the exact same values. R115 (215) in the output circuit prevents interaction between left and right channel equalization when the MODE switch is set to L+R.
MONITOR switch S3	Selects the signals from TAPE, AUX or equalizer outputs.
MODE switch S4	Selects the desired mode of operation. This switch may also be used for test purposes. The relation between the positions of the MODE switch and outputs of the set are summarized in the table below.
VOLUME control RV302	The equalized phono signals and signals applied to the other input terminals are fed to the VOLUME control through the MONITOR and MODE switches. The level of the signal applied to the following tone-control amplifier is determined by the setting of RV302.

TABLE 1-2.

OUTPUTS / MODE SELECTOR SWITCH POSITION	SPEAKER OUT; LEFT	SPEAKER OUT; RIGHT	HEAD-PHONE OUT; LEFT	HEAD-PHONE OUT; RIGHT	REC OUT; LEFT	REC OUT; RIGHT	PRE-AMP OUT; LEFT	PRE-AMP OUT; RIGHT
REVERSE	R	L	R	L	L	R	R	L
STEREO	L	R	L	R	L	R	L	R
L + R	L + R	L + R	L + R	L + R	L + R	L + R	L + R	L + R
LEFT	L	L	L	L	L	L	L	R
RIGHT	R	R	R	R	R	R	L	R

Stage/Control	Function
LOUDNESS switch S5	This switch and R301, R302, C301 and C302 compensate for the characteristics of the human ear which vary according to the loudness of the sound being heard. When this switch is set to ON, and the VOLUME control is set for 30 dB attenuation, the overall frequency response is increased 8 dB at 50 Hz and 3 dB at 10 kHz with reference to the level at 1 kHz.
Tone-control amplifier Q301, Q302, Q303	This three-stage amplifier has basically flat response, but it operates as a negative-feedback type tone-control circuit. The input signals are amplified by Q301 and Q302, and then applied to Q303 (source follower). The output generated at the source circuit of Q303 is fed back to the source circuit of Q301 through the treble and bass tone-control network.
BASS control switch S6-1F, S6-1R	Decreases the amount of negative feedback voltage by switching the resistors connected to S6-1F in steps for increasing the low-frequency components of the signal. Conventional RC filter network techniques are applied to obtain proper response at low frequencies by switching the resistors connected to S6-1R in steps.
TREBLE control switch S7-1R, S7-1F	Decreases the amount of negative feedback voltage by switching the resistors connected to S7-1R in steps when increasing the high-frequency components. The conventional RC filter network techniques are applied to obtain proper response at high frequencies by switching the resistors connected to S7-1F in steps. This has a range of ±10 dB at 10 kHz.
HIGH FILTER switch S8	The high-cutoff filter (R344 and C314) eliminates unwanted high-frequency components (6 dB/oct above 7 kHz) from the input signal when this switch is ON.
LOW FILTER switch S9	Cuts out unwanted low frequency components from the input signal (6 dB/oct below 100 Hz) in the ON position.
Muting circuit for preamplifier Q921, Q922 (Q923)	This muting circuit prevents the loud "pop" (due to initial current flow) or click noises produced by switch controls just after turning the power switch to ON. These transients might damage a delicate high-fidelity speaker system. The base of Q922 (Q923) is connected to the collector circuit of Q921 through R998 (R999), while the base of Q921 is connected to an RC network
R994, C991	(R994, C991) with a long time constant. When you first turn ON the power switch, Q921 remains off due to the long time constant of the associated bias circuit, while Q922 (Q923) is forward biased by R996. As a result, Q922 (Q923) is ON, shorting the preamplifier's output to ground. Thus the preamplifier's output is effectively muted. As Q921 is gradually turned ON due to the slowly-increasing base current flow, Q921 conducts and cuts off Q922, removing the muting.
NORMAL/ SEPARATE switch S10	In NORMAL, the output of the preamplifier is fed to the power amplifier's input through S10. In SEPARATE, the output of the preamplifier is disconnected from the power amplifier's input terminal, allowing you to use the sections separately.

Power Amplifier Section

Stage/Control	Function
Preamplifier Q701, Q702	Q701 and Q702 form a paraphase amplifier, but signal out-

Stage/Control	Function
	put is extracted from the collector circuit of Q701. This circuit has a various advantages in direct coupling systems. One is high stability despite temperature variations and another is high input impedance without reducing the amplifier's gain. The ac output appears across load resistor R712 (R812) in the collector circuit. An emitter decoupling circuit is formed by the emitter-base resistance of Q702, C702 and R710 in the base circuit of Q702. An emitter circuit formed by the emitter-base resistance of Q702, C702 and R710 is essentially a frequency-selective ac bypass to reduce the amplifier's gain at very low frequencies. Common emitter-resistor R711 keeps the dc current flow constant in Q701 and Q702, thus increasing the dc stability.
Dc balance adj. R702	The stabilized positive and negative power supply voltages are picked off by R908 and R907, R909 and R908, and applied to R702 or R802, R702 provides a stabilized bias voltage for transistor Q701 to set the output terminal voltage at zero dc.
Thermal compensation and noise suppressor D701	As all the stages are directly coupled, dc stability is required. The negative temperature coefficient of D701 provides thermal compensation for the following driver stage. It also acts as a noise suppressor to reduce the popping noise caused by unbalanced current flow in the following stages when the power switch is turned off.
Driver Q704	Though this stage is a conventional flat amplifier, it determines the output voltage swings because the following stages are basically emitter-followers. The ac load resistor for this stage is R714.
Dc bias adj. (idling current) Q705, R715	Q705 is biased into conduction and operates as a small resistance providing the necessary forward bias on the two cascaded emitter-followers. R715 controls the base bias of Q705, determining its emitter-collector impedance and thereby controls the dc bias voltage for the following complementary circuit.
Thermal compensator for dc bias D702 (D802)	The negative temperature coefficient of diodes D702 and (D802) provides thermal compensation for the complementary and power-transistor circuits. D702 is attached to the power transistor's heat sink to detect temperature increases in the power transistors.
Complementary circuit Q710, Q711	These transistors operate as emitter-followers to provide the current swings demanded of the output stages and also provide the necessary phase inversion. Phase inversion is performed by using PNP and NPN type transistors.
Power transistors Q712, Q713	The output transistors Q712 and Q713 are connected directly to a power supply of about ±50 V. Q712 supplies power to the load during the positive half cycle and Q713 operates during the negative half cycle. As all the stages are directly coupled and designed to obtain zero potential at the output terminal, the large coupling capacitor at the output which may cause power loss or distortion at low frequencies is eliminated.
Protection circuit	Two kinds of protection circuits are employed in this power amplifier. One is a power-transistor protection circuit and the

Stage/Control	*Function*
	other is a speaker-system protection circuit.
Power-transistor protection circuit	To protect overloaded power transistors from destruction, a new protection circuit is employed. In the event of a short circuit at the output terminals, the protection circuit holds down the current in the power transistor and also limits the input drive signals. Fig. 1-2 shows a partial schematic diagram detailing this protection circuit. With reference to this diagram, the protection circuit operates as follows: (Since the protection circuit is identical for positive-going half cycles and negative-going half cycles, only the positive-going half cycle operation is described here.) Q707 limits the positive-going half cycle of the drive voltage applied to the base of Q710 when power consumption at the Q712 collector exceeds the safety margin. Since power dissipation at the collector can be considered a function of collector voltage and current, the trigger signal for Q707 is taken from the collector and emitter. Base voltage is partly determined by the ratio of resistor R720 to the series resistance consisting of R724, R728, R736 and RL (load). Base voltage is also determined by the current flow in R736 and the collector voltage of Q712. During normal operation, Q707 is cut off. When excessive current flows in the power transistor or power dissipation at the collector of the power transistor exceeds the specified value, Q707 turns ON and limits the input drive voltage to the power transistor. Limiting operation is also actuated by the condition of the load. The base voltage of Q707 is determined by resistances R726, R722, R728, R736 and RL (load). D706 prevents reverse voltage from being applied during the negative going half cycle. Q707 turns ON limiting the input drive voltage to the power transistor when the load resistance decreases to some extent.

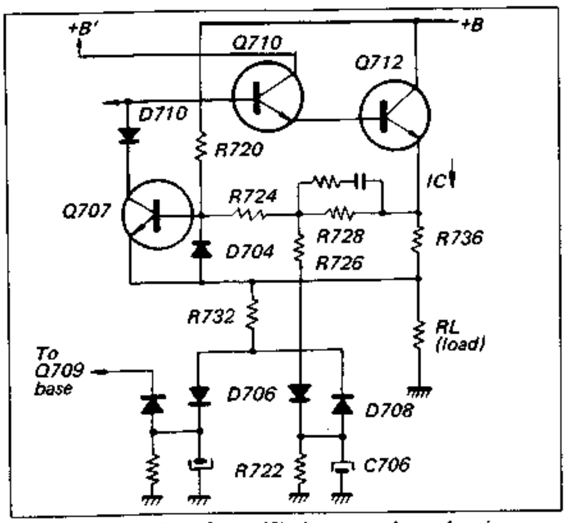


Fig. 1-2 Simplified protection circuit

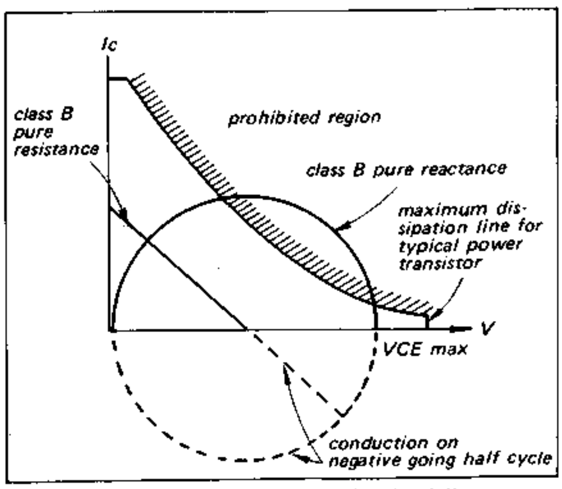


Fig. 1-3 Resistive and reactive load lines for class B output stage showing breakdown risk

Stage/Control	Function
	Under reactive load conditions in class B amplifiers, maximum current will flow when the voltage across the power transistor is maximum. This is the worst case for secondary breakdown. See Fig. 1-3. Since all speakers have reactive properties, the protection circuit must take care of this problem. Fig. 1-3 shows the operating load lines for one half of a class B output stage under conditions of equal load impedance; in one case the load is purely reactive, a load case which would result in transistor failure. Through a complex network of resistors and transistors, D708, C706 and R732 change the base voltage of Q707 according to the reactive voltage induced in the load to provide proper protection. Diode D706 detects reactive voltage at the output terminal and charges C706. This voltage changes the bias on Q707 to compensate for the reactive voltage. D704 protects Q707 from breakdown between base and emitter due to detected reactive voltage across C706.

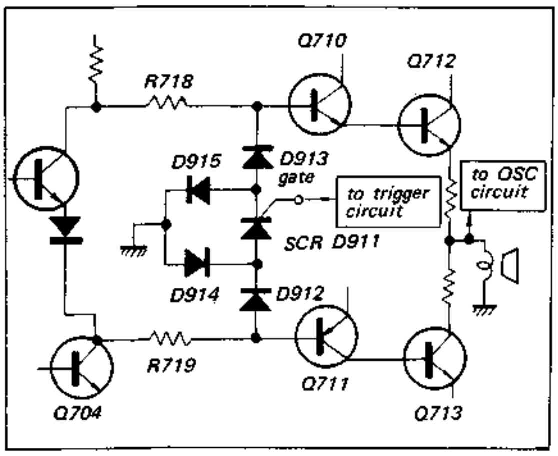
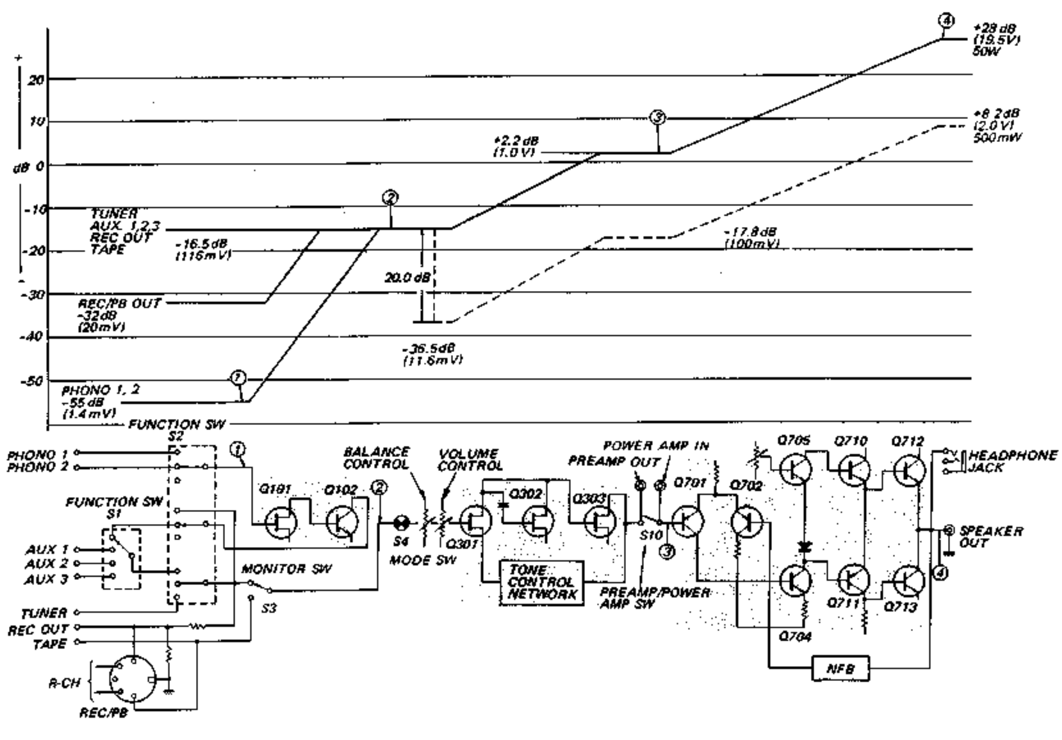


Fig. 1-4 Speaker protection circuit

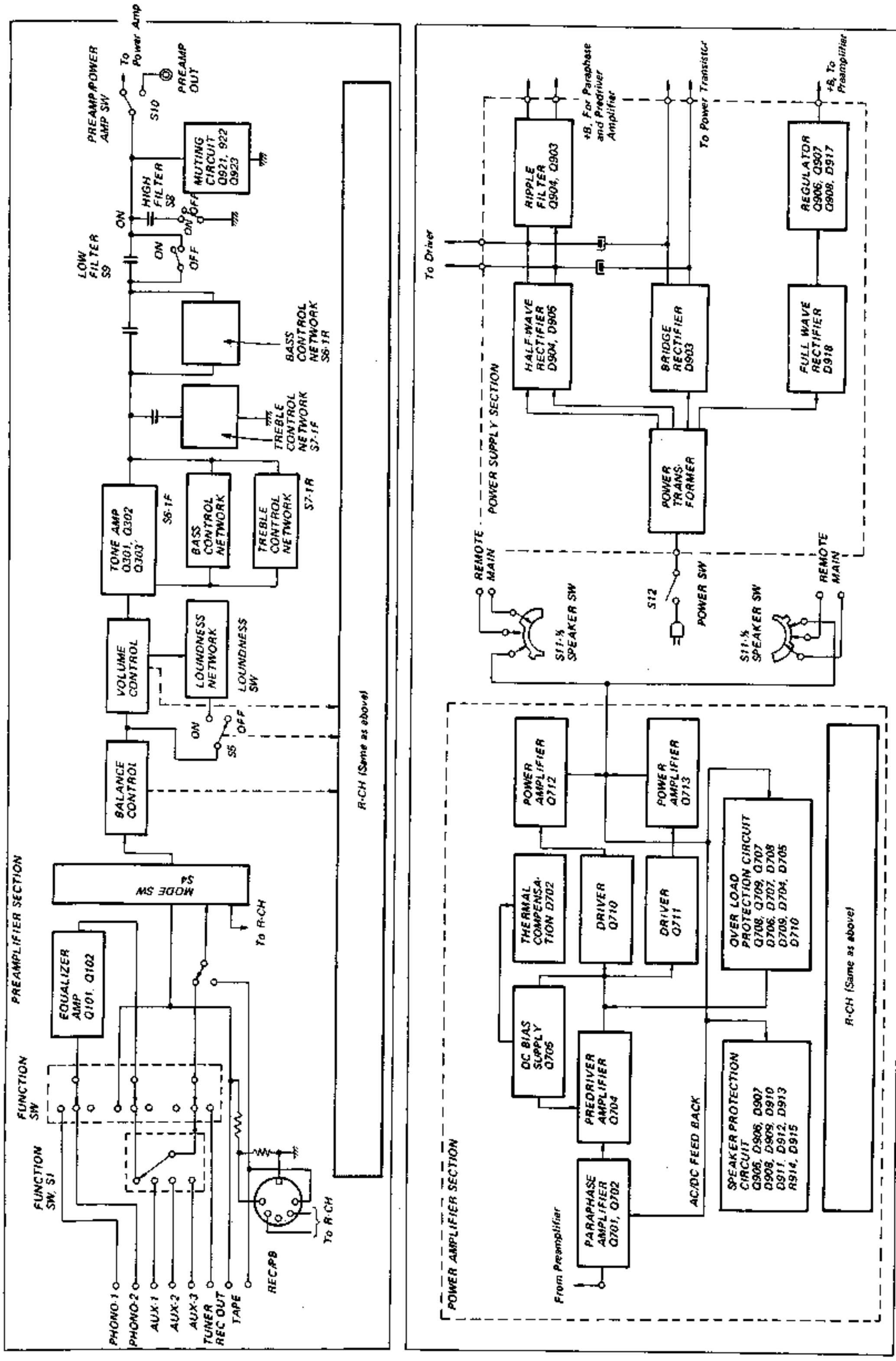
Stage/Control	Function
Speaker protection circuit	In a direct-coupled power amplifier, some faults in the early-stage transistors appears as a large unbalanced dc voltage across output terminal. This might damage a delicate speaker system. Therefore, the TA-1130 incorporates a speaker protection circuit which operates as follows (refer to Fig. 1-4): The output signal is extracted from the output terminal through a low-pass filter (R931 or R932, C931 and C932) and fed to the bridge rectifier (D906 ~ D909). Because of this filter, the voltage applied to the bridge rectifier is only the very-low frequency or dc component caused by transistor faults. When the rectified dc voltage becomes large enough, it starts the Hartley oscillator (Q905 and T osc). The oscillator's output is rectified by D910 and thus provides trigger voltage for SCR D911. When the trigger voltage is applied to the gate of the SCR, the SCR turns on and shorts the base voltage of Q710 to ground through D912, the SCR, and D915. The base voltage of Q711 is also shorted to ground through D914, the SCR, and D913. This stops any current flow in the output stage and thus protects the speaker system. Note that the direction of diodes D912, SCR D911 and D913 also ensure speaker protection even if one of the power transistors is damaged by accident, by forcing the other power transistor into secondary breakdown.

Stage/Control	*Function*
Power-Supply Section	
Rectifier D903	A full-wave bridge rectifier and center-tapped transformer provides positive and negative dc power supplies for the power amplifier.
Rectifier D904, D905	A pair of half-wave rectifiers (D904 and D905) and filter capacitors (C916 and C924) supply additional dc voltage in series with the bridge-rectifier output for the complementary stages.
Ripple filter Q903, R912, R913, C914, Q904, R915, R916, C922	These components reduce the ripple voltages in the dc power supply for preamplifier and driver stages of the power amplifier section to an extremely-low value. Q903 and Q904 serve as an electronic filter to supply well-filtered dc of about ± 53V to preamplifier stages in the power amplifier.
Regulated power supply Q906, Q907, Q908	Dc output from rectifier D918 is filtered by C944 and applied to series regulator Q906. Transistor Q908 compares a sample of the output voltage picked off across R956 with reference voltage supplied by voltage stabilizer D917. A change in output voltage is detected at the base of Q908 and therefore alters collector voltage. Since the collector of Q908 is directly coupled to the base of Q907, the change in output voltage alters the conduction of Q907 and Q906 by the amount necessary to maintain the output voltage constant. An increase in output voltage causes an increase in the impedance (decrease in conduction) of Q906, and vice versa. The dc output voltage supplied to the preamplifier section is therefore, extremely stable.

1-3. LEVEL DIAGRAM



1-4. BLOCK DIAGRAM



SECTION 2
DISASSEMBLY AND REPLACEMENT PROCEDURES

WARNING

Unplug the ac power cord before starting any disassembly or replacement procedures.

2-1. TOOLS REQUIRED

The following tools are required to perform disassembly and replacement procedures on the TA-1130.

1. Screwdriver, Phillips-head
2. Screwdriver, 3 mm (1/8") blade
3. Pliers, long-nose
4. Diagonal cutters
5. Wrench, adjustable
6. Tweezers
7. Electric drill
8. Drill bits
9. Prick punch
10. Hammer, ball-peen
11. Soldering iron, 40 to 50 watts
12. Solder, rosin core
13. Cement solvent
14. Cement, contact
15. Silicone grease

2-2. HARDWARE IDENTIFICATION GUIDE

The following chart will help you to decipher the hardware codes given in this service manual.

Note: All screws in the TA-1130 are manufactured to the specifications of the International Organization for Standardization (ISO). This means that the new and old screws are not interchangeable because ISO screws have a different number of threads per mm compared to the old ones. The ISO screws have an identification mark on their heads as shown in Fig. 2-1.

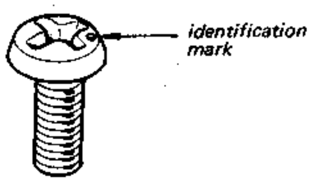


Fig. 2-1 ISO screw

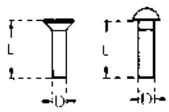
— Hardware Nomenclature —

P	Pan Head Screw
PS	Pan Head Screw with Spring Washer
K	Flat Countersunk Head Screw
B	Binding Head Screw
RK	Oval Countersunk Head Screw
T	Truss Head Screw
R	Round Head Screw
F	Flat Fillister Head Screw
SC	Set Screw
E	Retaining Ring (E Washer)

W – Washer
SW – Spring Washer
LW – Lock Washer
N – Nut

– Example –

⊕ P 3×10
- ⊕ — Type of Slot
- P — Type of Head
- 3 — Diameter in mm (D)
- 10 — Length in mm (L)



2-3. TOP COVER AND FRONT PANEL REMOVAL

1. Remove the two machine screws at each side of the case, and lift off the top cover.
2. Remove all control knobs and levers. The knobs can be removed by loosening the slotted set screws and pulling the knobs straight out. The levers are simply pulled off.
3. Remove the three screws (+PSW 4×6) behind the top edge of the front subchassis as shown in Fig. 2-2.
4. Remove the three self-tapping screws (+B 3×6) at the front bottom of the chassis as shown in Fig. 2-3. This frees the front panel.

2-4. FRONT SUBCHASSIS REMOVAL

The front subchassis is the vertical member on which all the controls, switches, and pilot lamp are attached.

1. Remove the top cover and front panel as described in Procedure 2-3.
2. Remove the two screws (⊕B 3×6) at each side of the chassis (see Fig. 2-5) and four self-tapping screws (⊕B 3×6) at the front bottom of the chassis as shown in Fig. 2-3. This frees front subchassis as shown in Fig. 2-4.

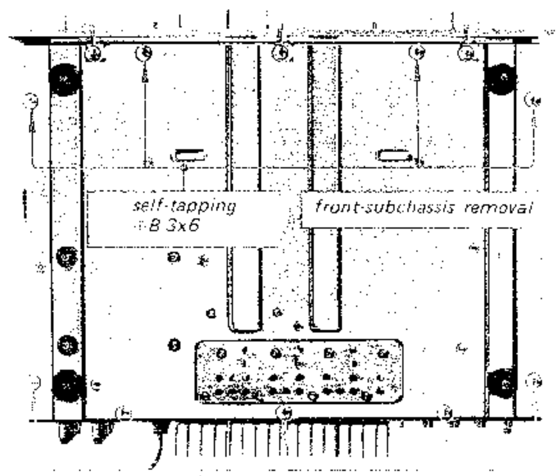


Fig. 2-5 Bottom view

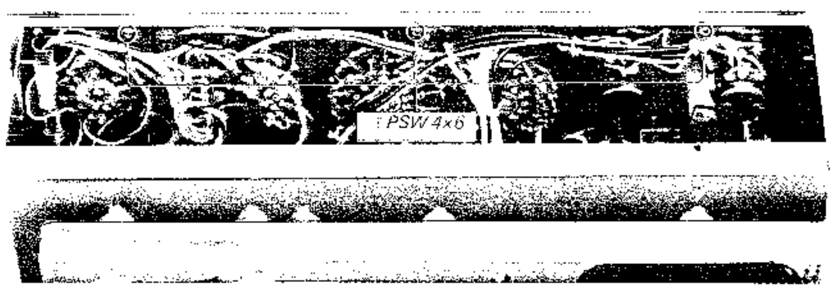


Fig. 2-2 Front-panel removal

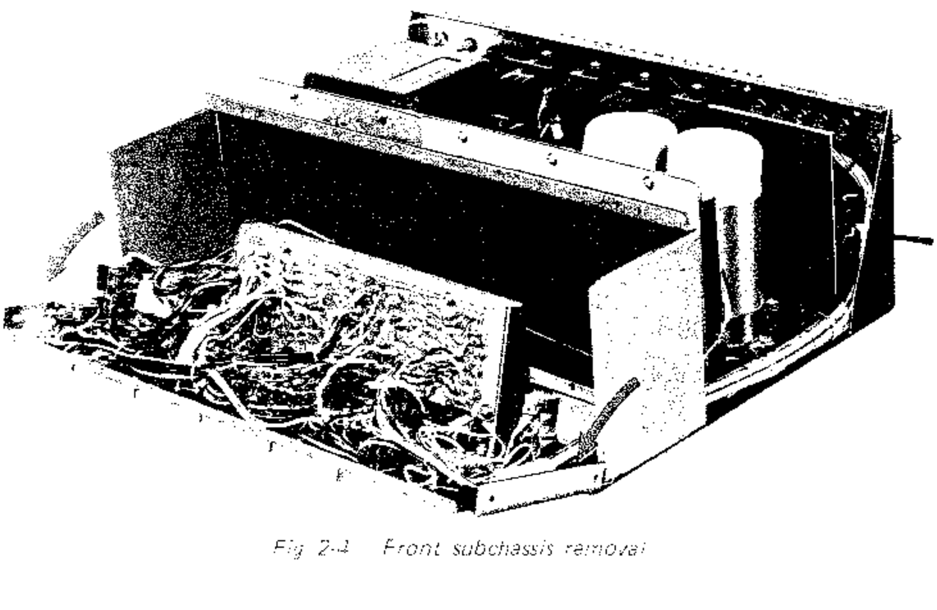


Fig. 2-4 Front subchassis removal

2-5. CONTROL AND SWITCH REPLACEMENT

Prepare for replacing any of the controls or switches by removing the front subchassis as described in Procedure 2-4.

POWER, LOW FILTER, HIGH FILTER, LOUDNESS, MONITOR and FUNCTION (2) Switches

1. Remove the two screws (⊕PS 3×5) securing switches to the front subchassis as shown in Fig. 2-5.
2. Unsolder the lead wires from the defective switch, and then install the replacement switch.

SPEAKER, MODE, FUNCTION (1) Switches and VOLUME, BALANCE, BASS and TREBLE Controls

1. Remove the hex nuts that secure the switches or controls to the front subchassis as shown in Fig. 2-5.
2. Unsolder the lead wires from the defective switch or control, and then install the new one.

HEADPHONE, AUX-3 Jacks

1. Remove the two screws (⊕B 3×6) securing the jack escutcheon to the front subchassis.
2. Unsolder the lead wires from the defective jack, and then install the new one.

2-6. REAR PANEL REMOVAL

1. Remove the top cover as described in Procedure 2-3.
2. Remove the four screws (⊕B 3×6) at each side of the chassis (see Fig. 2-6) and five self-tapping screws (⊕B 3×6) at the rear bottom of the chassis as shown in Fig. 2-7.
3. Remove the power amplifier board, and then unsolder the lead wires coming from the NORMAL SEPARATE switch.
4. Remove the ground lug terminal by loosening the screw securing the electrolytic capacitor (C923) bracket to the chassis as shown in Fig. 2-5.
5. Unhook the flexible conduit from the clamp located inside the rear panel, and then cut the strings tying the lead wires to the rear jacks together. [illegible]

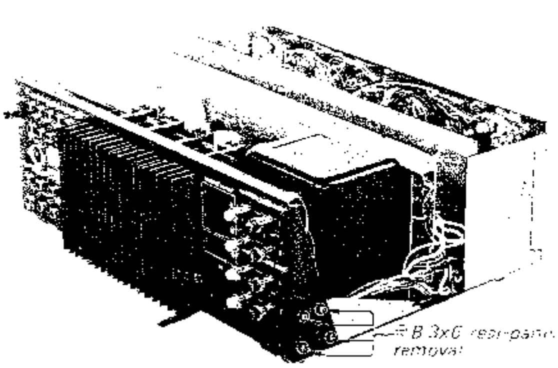


Fig. 2-6 Rear panel removal

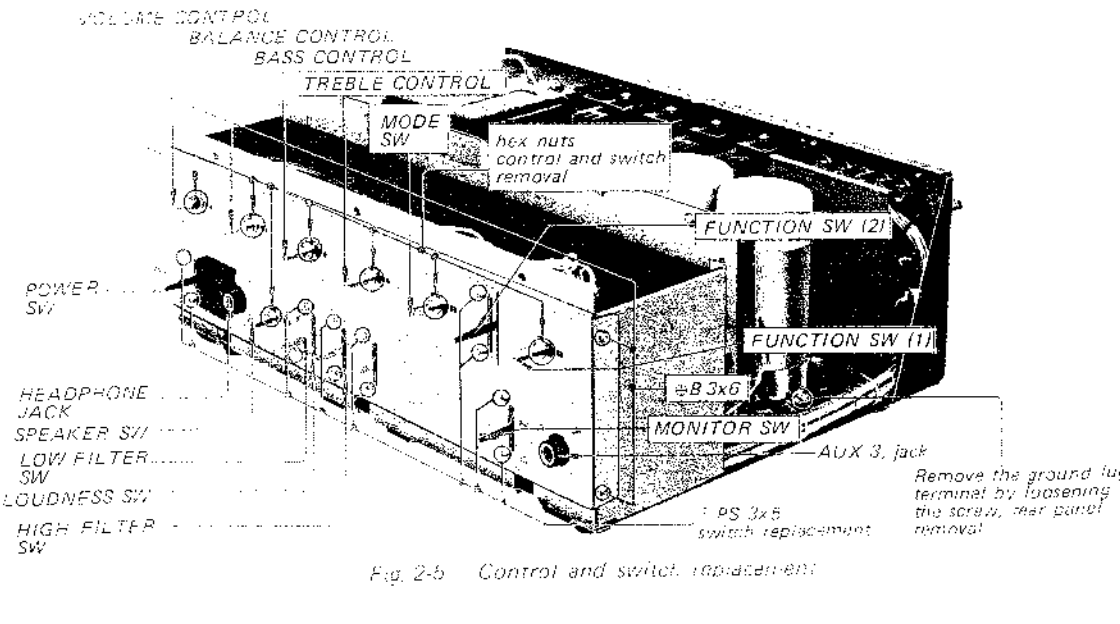


Fig. 2-5 Control and switch replacement

2-7. POWER TRANSISTOR REPLACEMENT

1. Remove the top cover as described in Procedure 2-3.
2. Remove the four self-tapping screws (⊕ B 3x8) securing the top heat-sink bracket as shown in Fig. 2-7.
3. Remove the four self-tapping screws (⊕ B 3x8) securing the pair of heat sinks to the chassis as shown in Fig. 2-8.
4. Carefully draw back the pair of heat sinks, and then remove the two screws (⊕ B 3x14) and nuts securing the power transistor to the heat sink. See Fig. 2-9.
5. Cut the emitter and base leads of the defective power transistor with a diagonal cutter. This prevents mica washer damage when removing the defective power transistor.
6. When replacing the power transistor, apply a coating of a heat-transferring grease to both sides of the insulating mica washer. Any excess grease squeezed out when the mounting bolts are tightened should be wiped off with a clean cloth. This prevents it from accumulating conductive dust particles that might eventually cause a short.

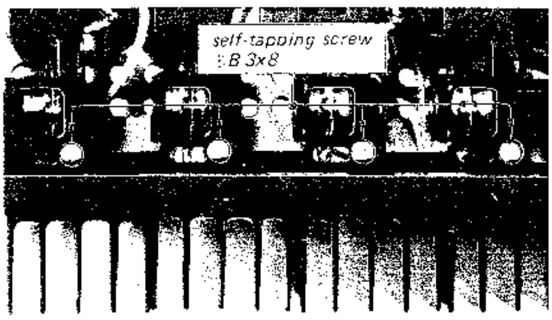


Fig. 2-7 Top heat sink removal

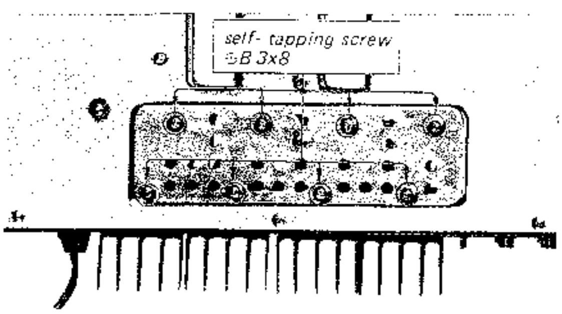


Fig. 2-8 Heat sink removal

2-8. REPLACEMENT OF COMPONENTS SECURED TO THE REAR PANEL BY RIVETS

1. Remove the rear panel as described in Procedure 2-6.
2. Bore out the rivets using a drill bit slightly larger in diameter than the rivet. See Fig. 2-10.
3. Punch out the remainder of the rivet with a nail set or prick punch.
4. Remove the defective component, and then install a new one.
5. Secure the new component with a suitable screw and nut, or a repair rivet screw (part number 3-701-402).

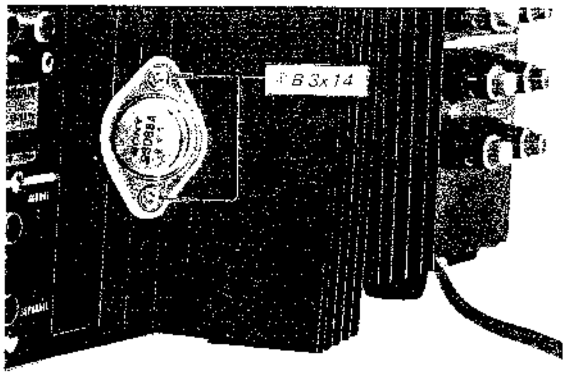


Fig. 2-9 Power transistor removal

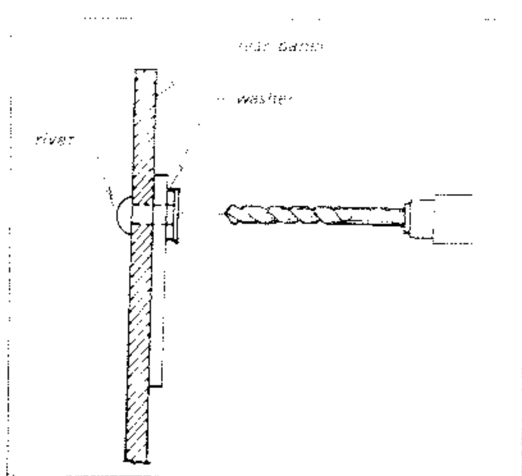
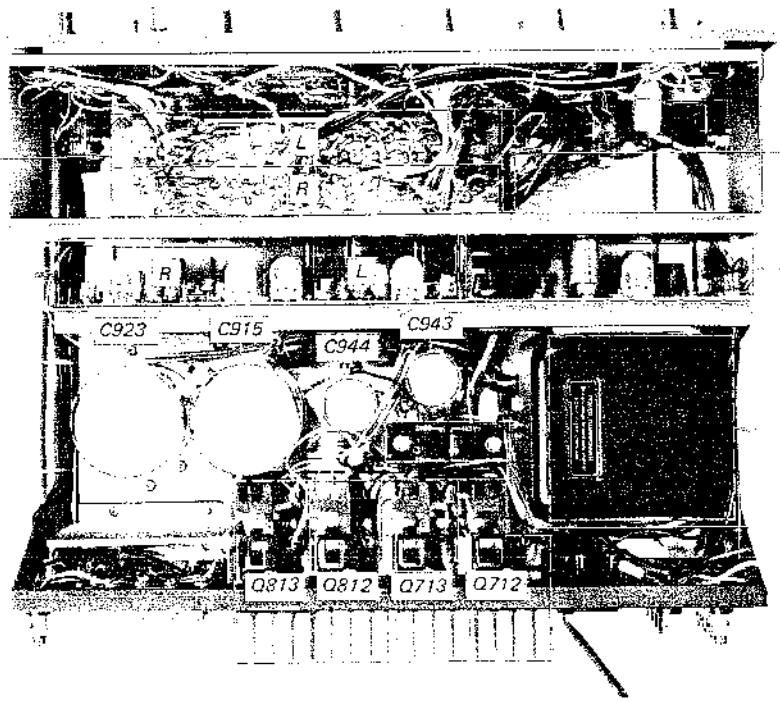


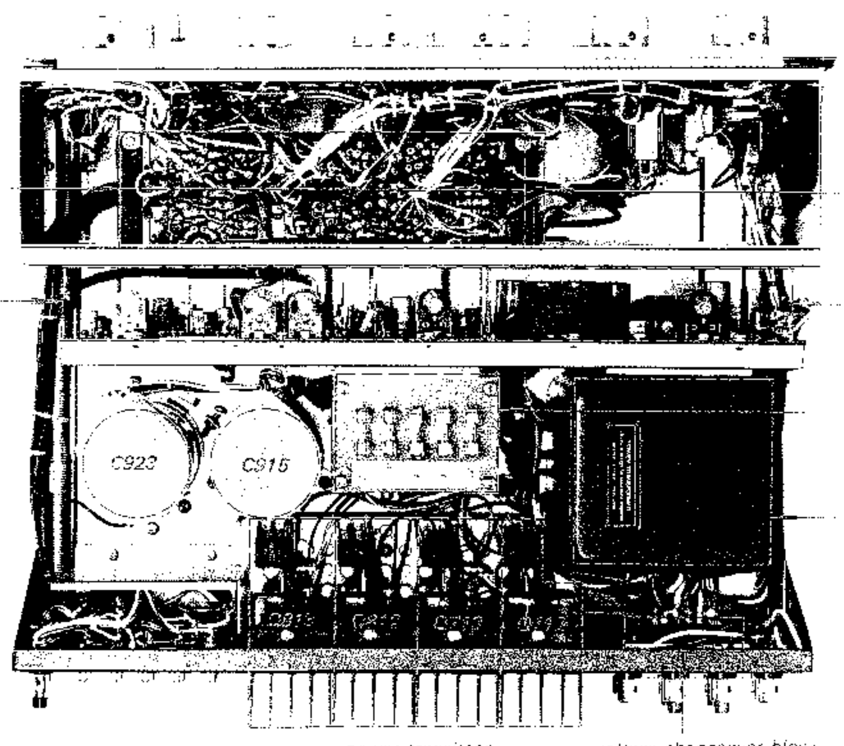
Fig. 2-10 Rivet removal

2-9. CHASSIS LAYOUT

General Export Model



GEP and NEP Model



SECTION 3
ADJUSTMENTS

3-1. POWER SUPPLY VOLTAGE ADJUSTMENT FOR PREAMPLIFIER SECTION

Test Equipment Required

1. Dc voltmeter:
   Capable of measuring 40V dc or more.
2. Screwdriver with 3 mm (1/8") blade
3. Variable transformer

Preparation

1. Remove the top cover as described in Procedure 2-3.
   Connect the dc voltmeter to the test point as shown in Fig. 3-1.

Procedure

1. Set the variable transformer for minimum output.
2. Turn the POWER switch to ON and then increase the line voltage up to the rated value.
3. Adjust semifixed resistor R956 (see Fig. 3-1) to obtain a 40V reading on the meter.

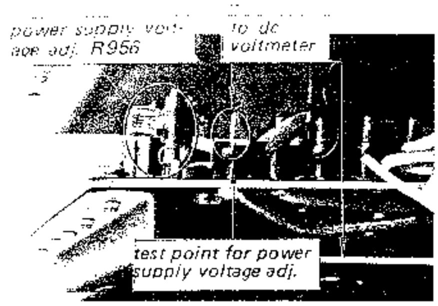


Fig. 3-1 Dc voltmeter connection and parts location

3-2 POWER AMPLIFIER ADJUSTMENTS

Note: There are two adjustments to be made in the power amplifier. One is dc-bias adjustment and the other is dc-balance adjustment. These adjustments should be alternately repeated two or three times after replacing any of the power transistors until the best operation is obtained.

Dc-bias Adjustment

Serious deficiencies in performance, such as thermal runaway of power transistors, will result if this adjustment is improperly set.

CAUTION

To avoid accidental power transistor damage, increase the ac line voltage gradually, using a variable transformer, while alternately measuring the voltage across test points and the hot side of the speaker binding post (emitter resistors R736 and R836 of the power transistors, as shown in Fig. 3-2. Check to see that the reading does not exceed 25 mV. If it does, turn off the power as soon as possible, then check and repair the trouble in the power amplifier board.

Test Equipment Required

1. Dc millivoltmeter.
   Capable of measuring [illegible] less
2. Variable transformer
3. Screwdriver with 3 mm (1/8") blade

Preparation

1. Remove the top cover as described in Procedure 2-3.
2. [illegible] point and the hot side of the speaker binding post (L-CH) (emitter resistor R736 of power transistor Q712) as shown in Fig. 3-2.
   When measuring the R-CH [illegible] the dc millivoltmeter lead should be connected to the R-CH hot side of the speaker binding post also.

Procedure

1. Apply a drop of cement solvent to the semifixed resistors on the power amplifier board, and then set the semifixed resistors (see Fig. 3-2) on the power amplifier board as follows:
   R715 (L-CH, dc-bias) .... fully clockwise
   R815 (R-CH, dc-bias) .... fully counterclockwise
   R702, R802 (dc-balance) .... mid position
2. Set the variable transformer for minimum output.
3. Turn the POWER switch to ON, and then increase the line voltage up to the rated value.
4. Adjust R715 and R815 to obtain a 25 mV reading on the meter and then perform the dc-balance adjustment.

Dc-Balance Adjustment

Excessive harmonic distortion at high levels or speaker system damage will result if this adjustment is improperly set.

Test Equipment Required

1. Dc null meter or dc millivoltmeter.
2. Screwdriver with 3mm (1/8") blade.

Preparation

1. Set the SPEAKER switch to MAIN.
2. Connect the dc null meter or dc millivoltmeter to the MAIN speaker output terminal.

Procedure

1. Turn the POWER switch to ON, and then adjust R702 (R802) to obtain a 0 V reading on the meter.
2. After 10 minutes warm-up, alternately repeat this and the dc-bias adjustment two or three times.
3. After completing the adjustments, apply a drop of lock paint to R715 and R702 (R815 and R802).

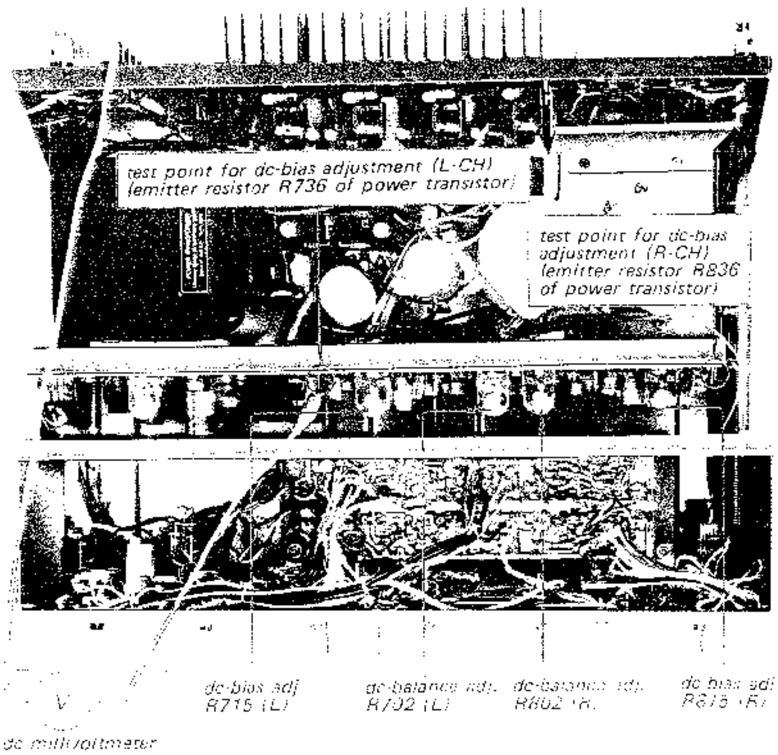


Fig. 2-2 Test points and adjustments

SECTION 4
REPACKING

The TA-1130's original shipping carton and packing materials are the ideal containers for shipping the unit. However to secure the maximum protection, the TA-1130 must be repacked in these materials precisely as before. The proper repacking procedures are shown in Fig. 4-1.

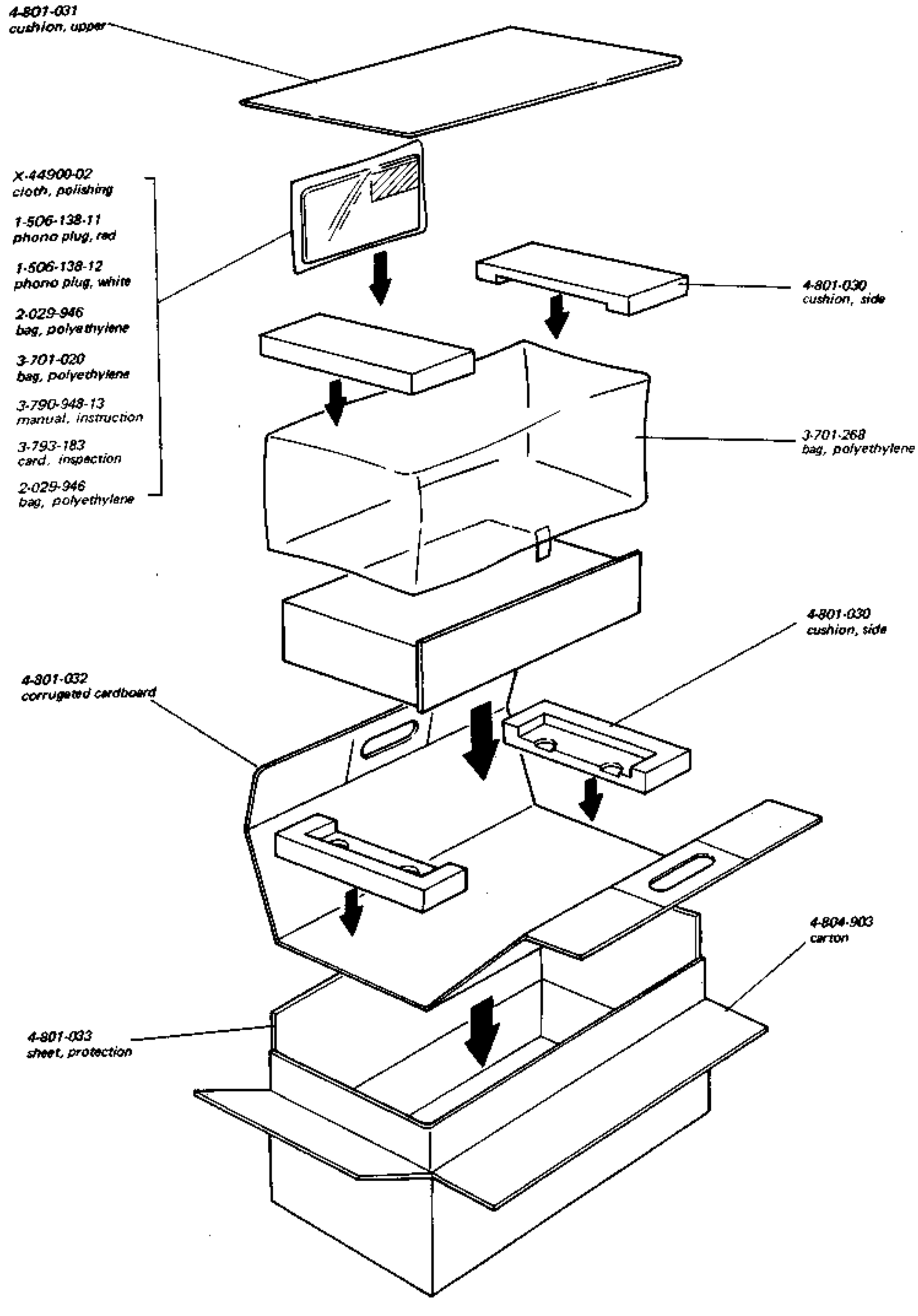
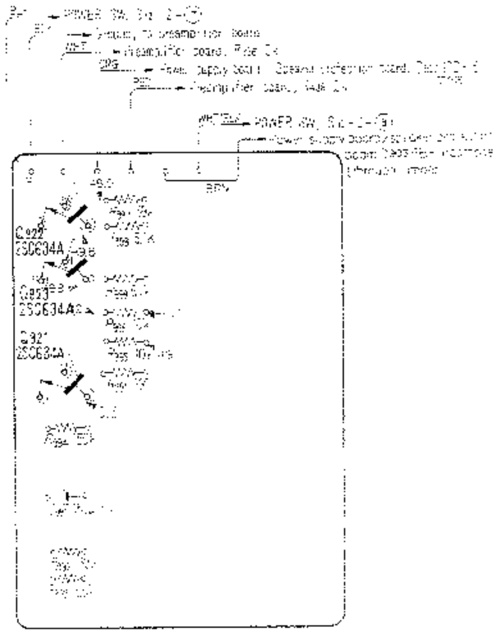


Fig. 4-1 Repacking

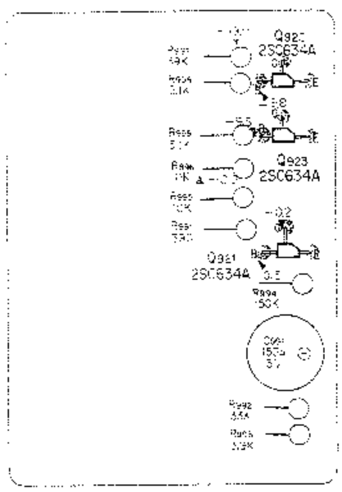
SECTION 5
DIAGRAMS

5-1. MOUNTING DIAGRAM – Muting Board –

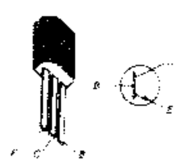
– *Conductor Side* –



– *Component Side* –

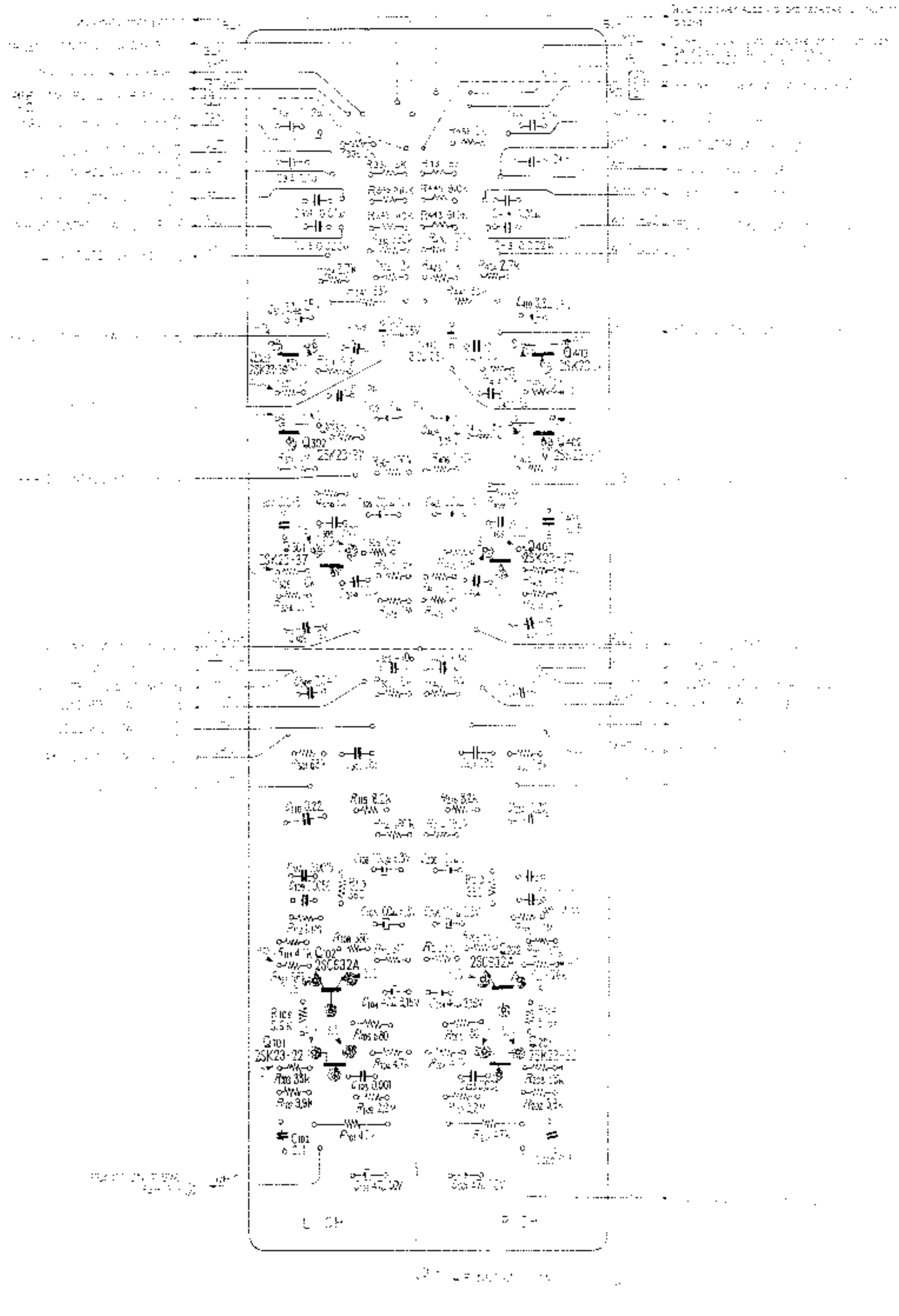


2SC634A



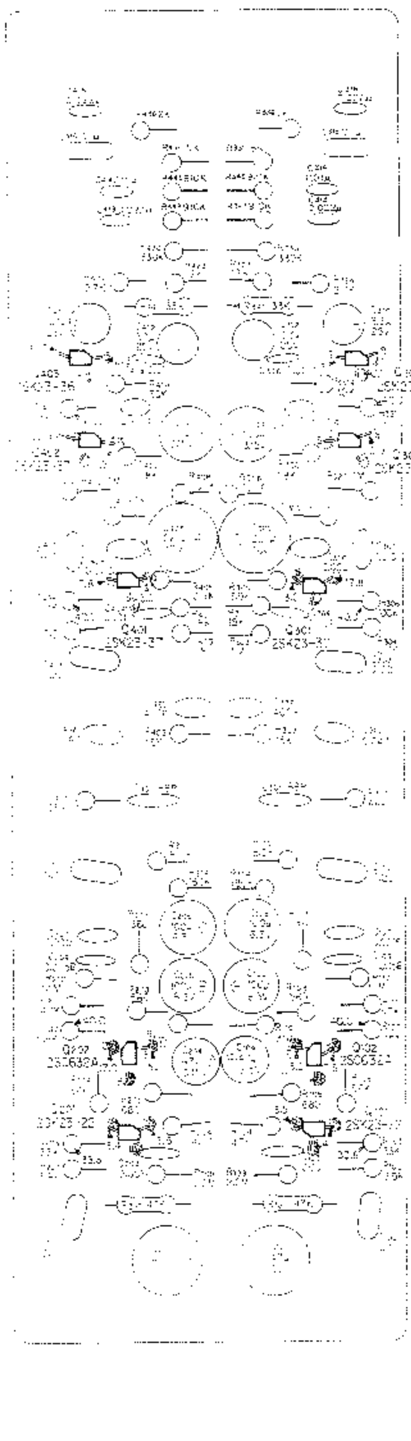
5-2. MOUNTING DIAGRAM – Preamplifier Board –

– Conductor Side –

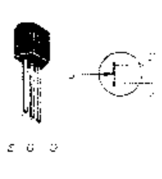


5-2. MOUNTING DIAGRAM – Preamplifier Board –

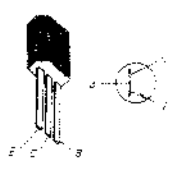
· *Component Side*



2SK23



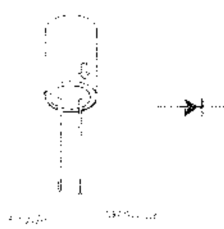
2SC632A



5-3. MOUNTING DIAGRAM – Power Amplifier Board –

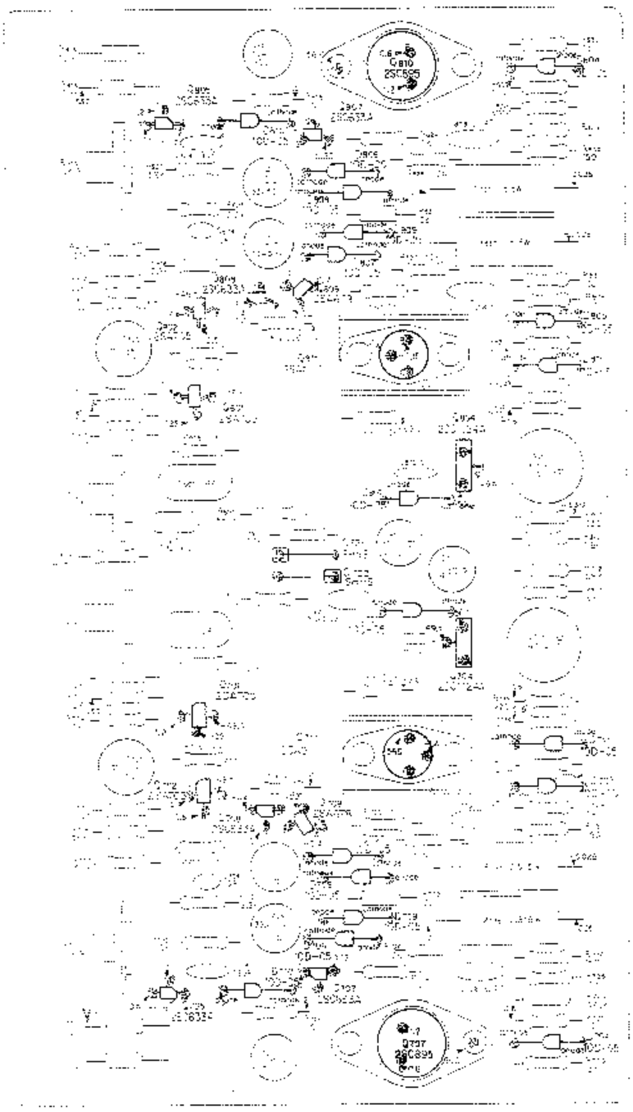
– Conductor Side –

SV-31

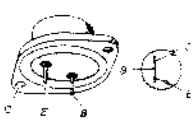


5-3. MOUNTING DIAGRAM – Power Amplifier Board –

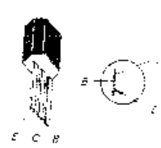
– Component Side –



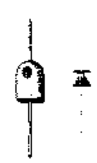
2SC895



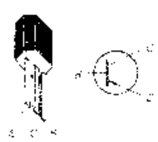
2SA678



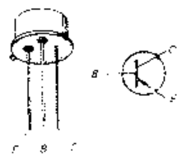
SH 1S



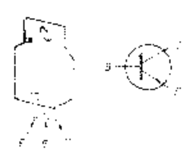
2SA705



2SA527



2SC1124A



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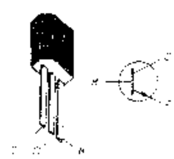
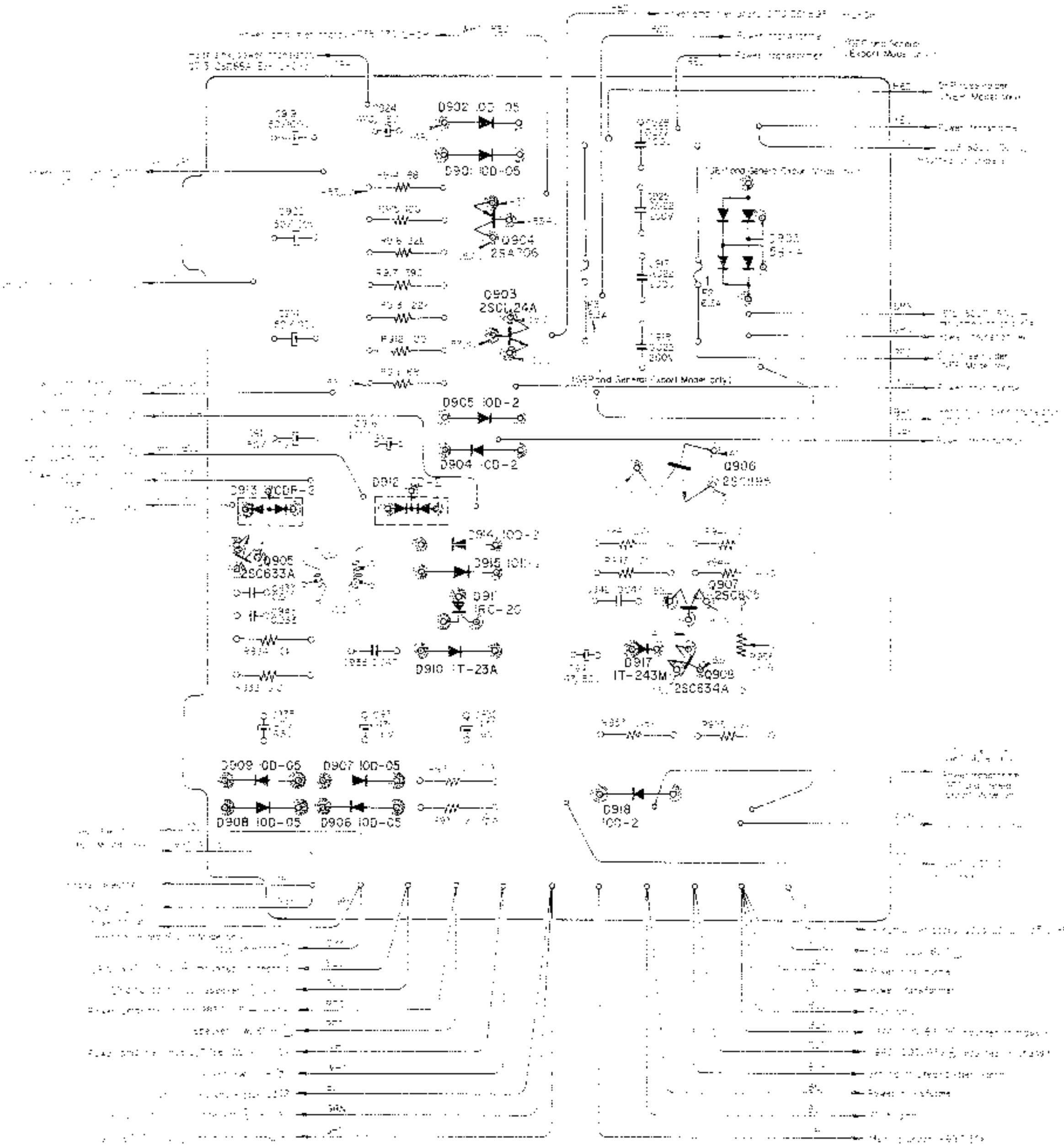


10D-05

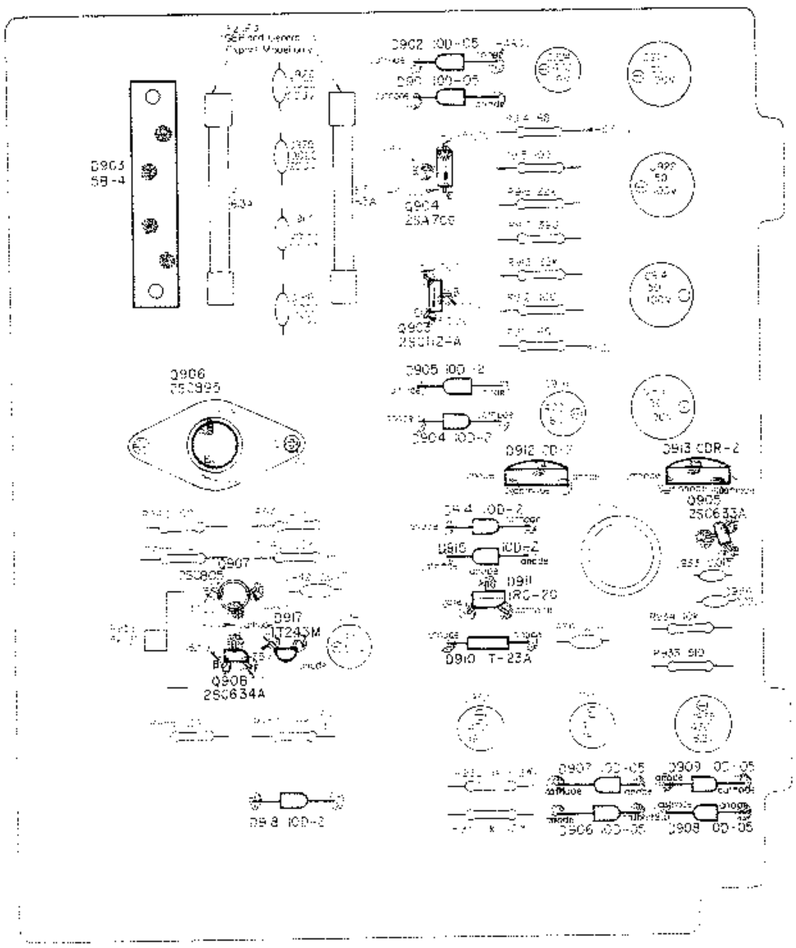
5-4. MOUNTING DIAGRAM – Power Supply/Speaker Protection Board –

– Conductor Side –

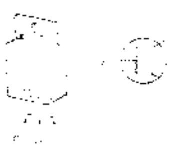


5-4. MOUNTING DIAGRAM – Power Supply/Speaker Protection Board –

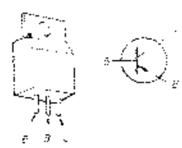
– Component Side



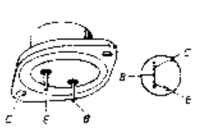
2SC1124



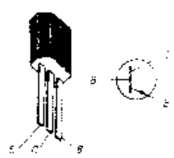
2SA706



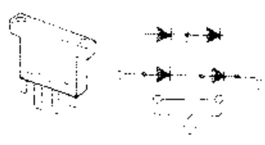
2SC395



2SC633A
2SC634A



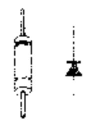
SB-4



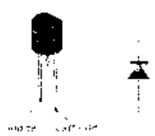
1RC 20

1T23A

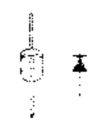
10D-05



1T243M



10D-2

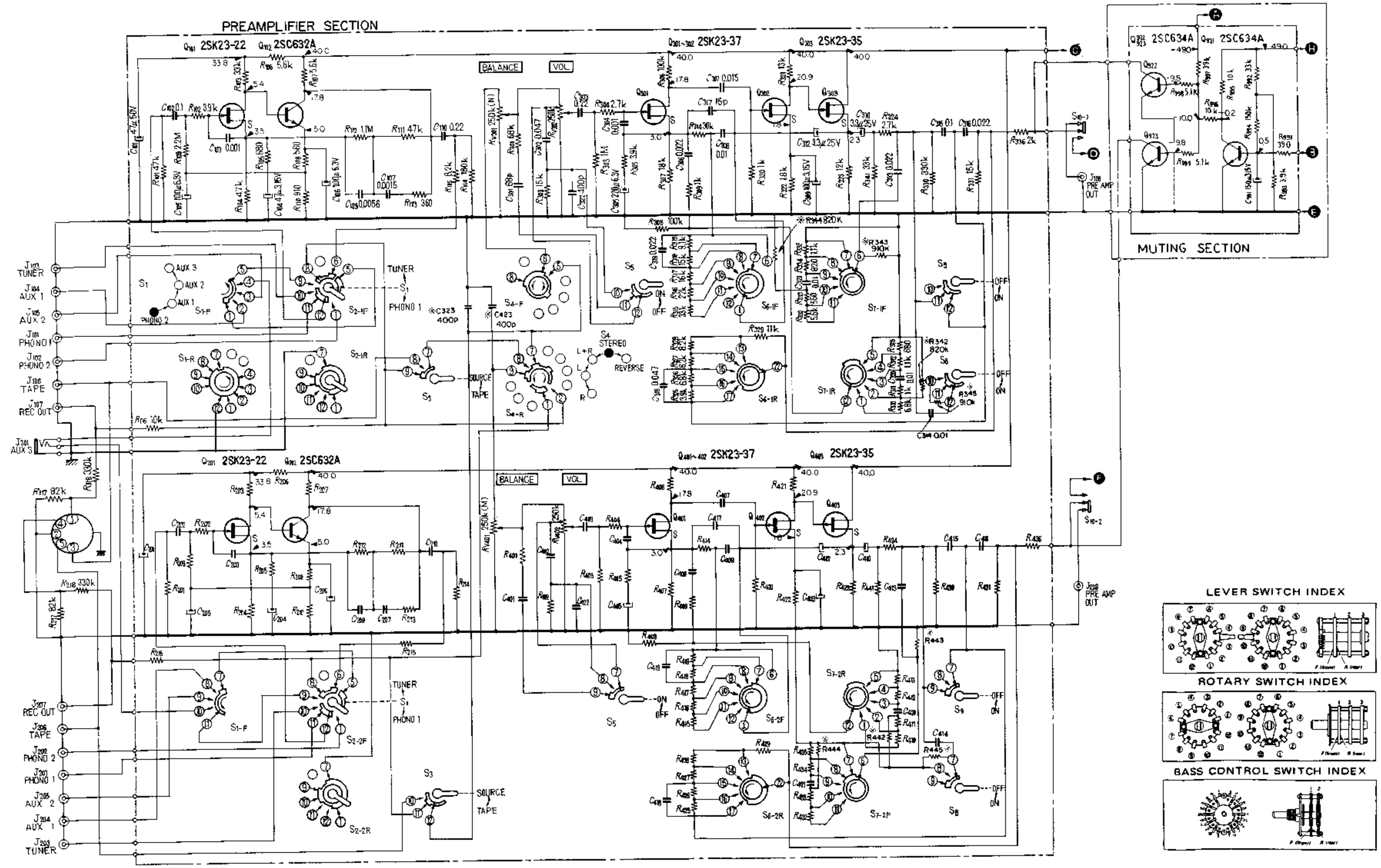


CDR-2

CD-2

MEMO

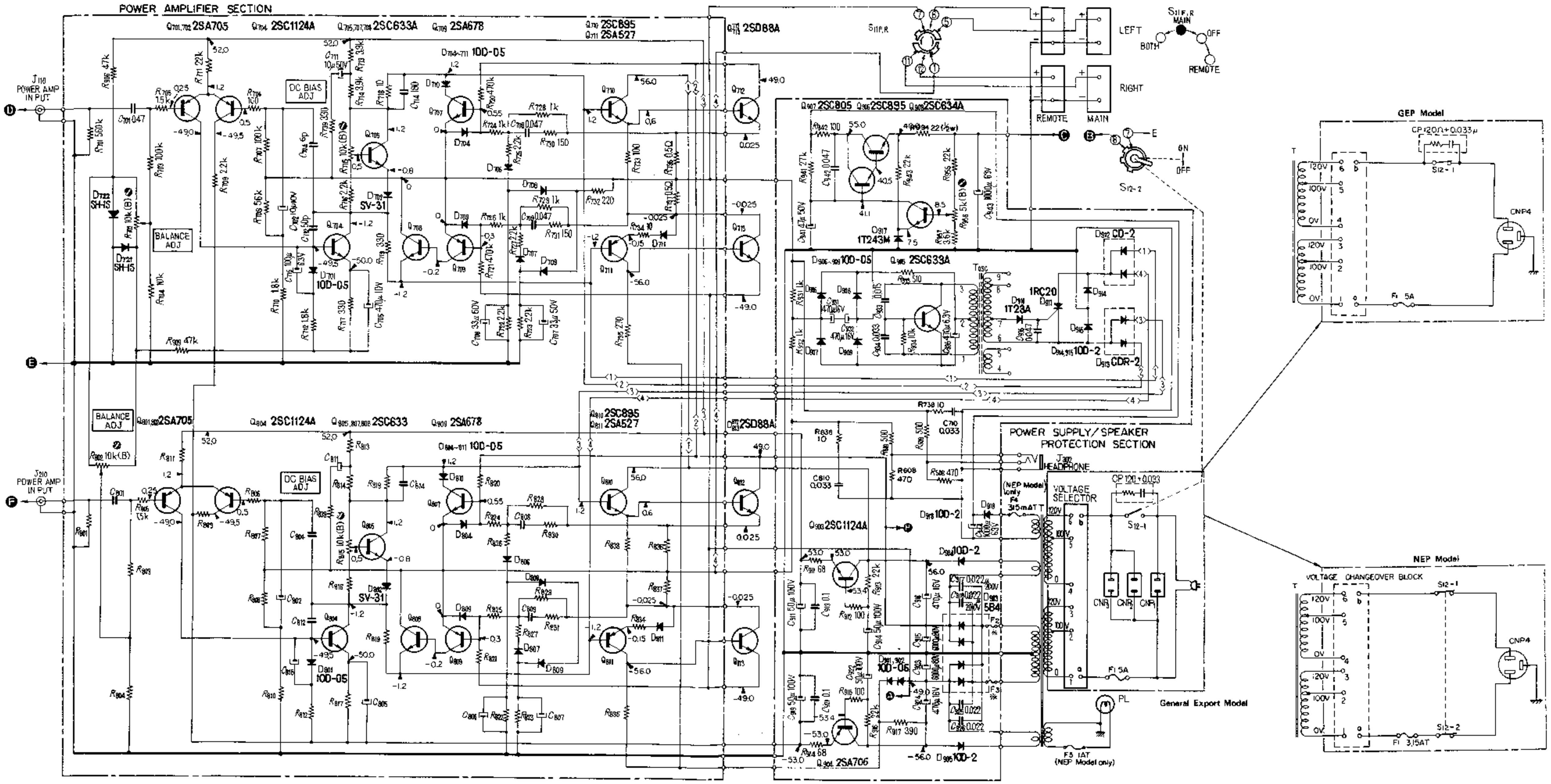
5-5. SCHEMATIC DIAGRAM – Preamplifier Section –



Ref. No.	Description	Position
S1	FUNCTION (1) SW (PHONO 2 - AUX 1 - AUX 2 - AUX 3)	PHONO 2
S2	FUNCTION (2) SW (PHONO 1 - FUNCTION (1) - TUNER)	PHONO 1
S3	MONITOR SW (SOURCE - TAPE)	SOURCE
S4	MODE SW (REVERSE - STEREO - L+R - LEFT - RIGHT)	STEREO
S5	LOUDNESS SW	ON
S6	BASS CONTROL SW	-10 dB
S7	TREBLE CONTROL SW	-10 dB
S8	HIGH FILTER SW	OFF
S9	LOW FILTER SW	OFF
S10	PREAMP/POWER AMP SW (SEPARATE - NORMAL)	SEPARATE

Note:
All resistance values are in ohms. k = 1,000, M = 1,000 k
All capacitance values are in μF except as indicated with p, which means μμF
All voltages represent an average value and should hold within ±20%.
All voltages are dc measured with a VOM which has an input impedance of 20 k ohms/volt. No signal in.

5-6. SCHEMATIC DIAGRAM – Power Amplifier Section –



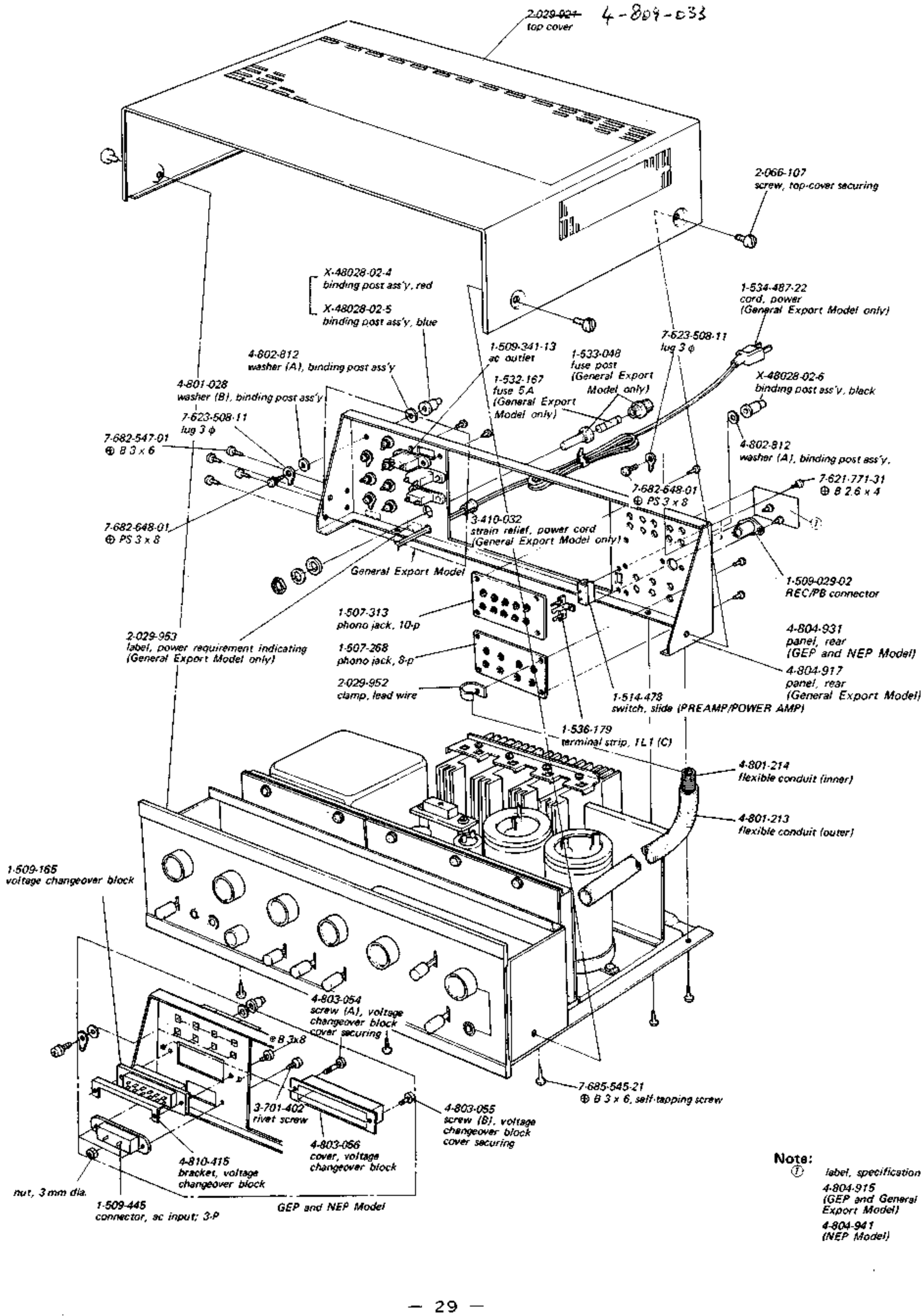
※ F2, F3
GEP and General Export Model; 6.3A
NEP Model; 6.3AT

Ref. No.	Description	Position
S11	SPEAKER SW (REMOTE - OFF - MAIN - BOTH)	MAIN
S12	POWER SW (OFF - ON)	ON

Note:

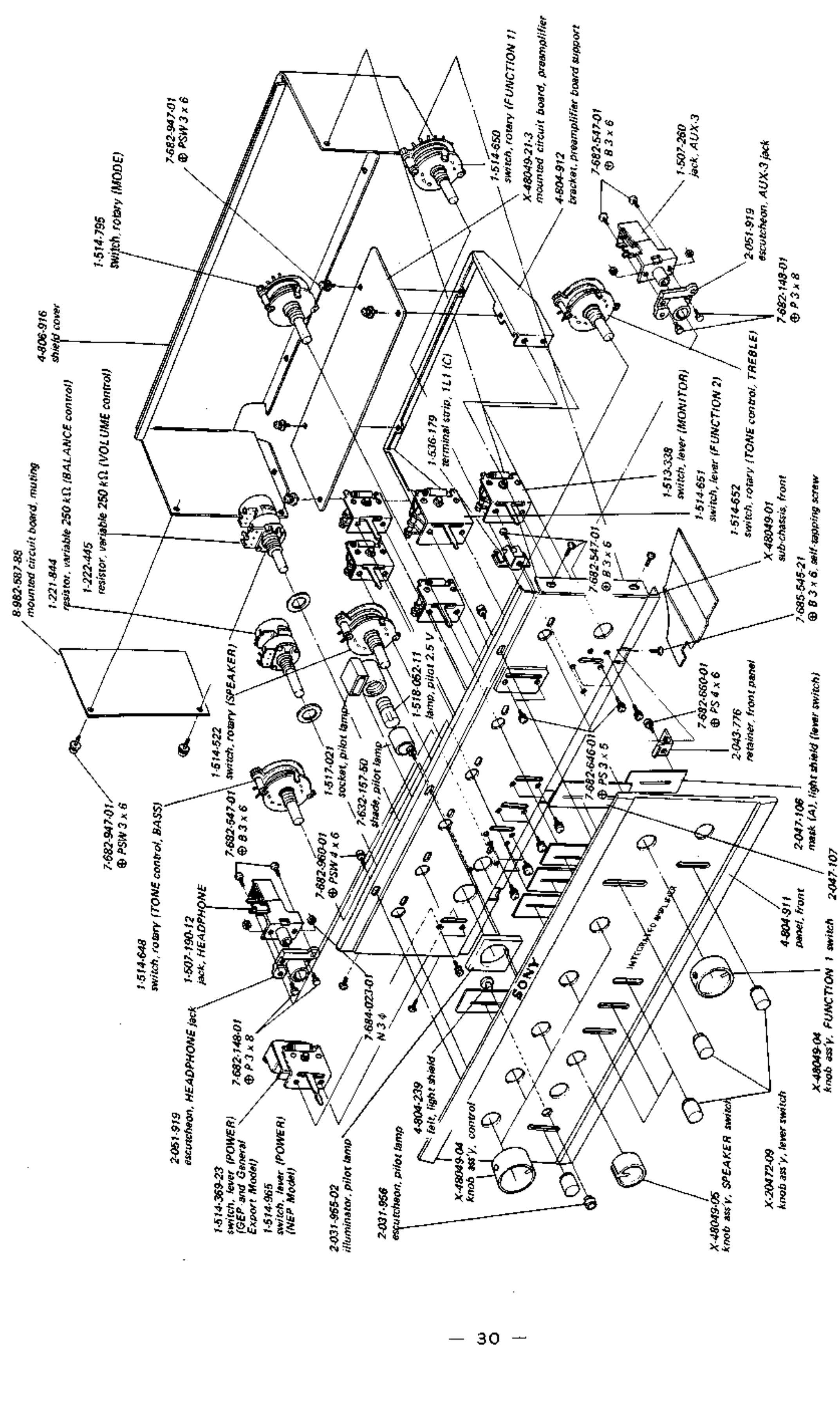
All resistance values are in ohms. k = 1,000, M = 1,000k
All capacitance values are in μF except as indicated with p, which means μμF.
All voltages represent an average value and should hold within ±20%.
All voltages are dc measured with a VOM which has an input impedance of 20k ohms/volt. No signal in.

SECTION 6
EXPLODED VIEW

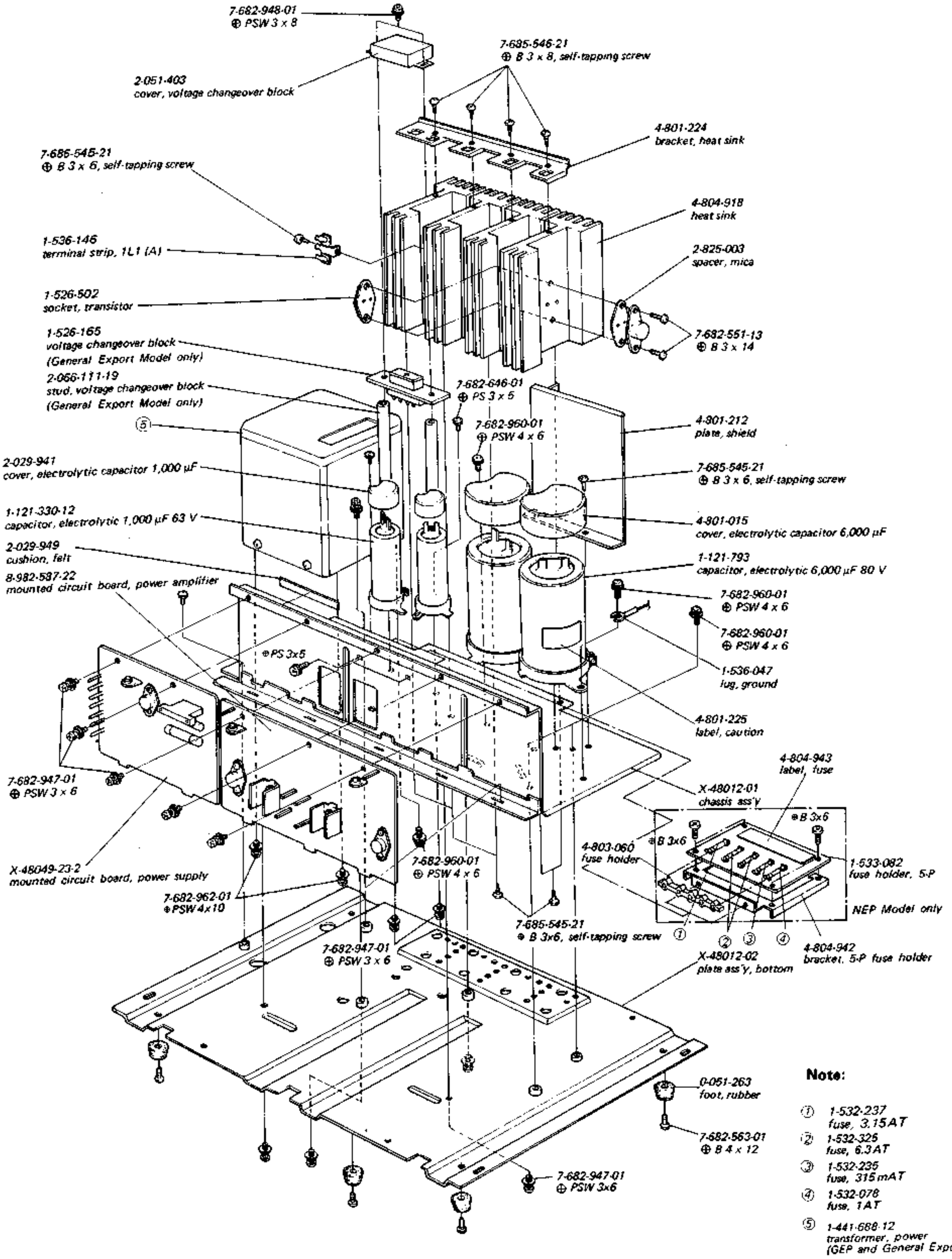


Note:
① label, specification
4-804-915
(GEP and General Export Model)
4-804-941
(NEP Model)

A-1130



7-682-947-01 ⊕ PSW 3 x 6
1-514-795 switch, rotary (MODE)
4-806-916 shield cover
8-982-587-88 mounted circuit board, muting
1-221-844 resistor, variable 250 kΩ (BALANCE control)
1-222-445 resistor, variable 250 kΩ (VOLUME control)
1-514-650 switch, rotary (FUNCTION 1)
X-48049-21-3 mounted circuit board, preamplifier
4-804-912 bracket, preamplifier board support
7-682-547-01 ⊕ B 3 x 6
1-507-260 jack, AUX-3
2-051-919 escutcheon, AUX-3 jack
7-682-148-01 ⊕ P 3 x 8
1-536-179 terminal strip, 1L1 (C)
1-513-338 switch, lever (MONITOR)
1-514-651 switch, lever (FUNCTION 2)
1-514-652 switch, rotary (TONE control, TREBLE)
X-48049-01 sub-chassis, front
7-682-547-01 ⊕ B 3 x 6
7-685-545-21 ⊕ B 3 x 6, self-tapping screw
7-682-660-01 ⊕ PS 4 x 6
2-043-776 retainer, front panel
7-682-646-01 ⊕ PS 3 x 5
2-047-106 mask (A), light shield (lever switch)
2-047-107 mask (B), light shield (FUNCTION 2 switch)
4-804-911 panel, front
X-48049-04 knob ass'y, FUNCTION 1 switch
X-20472-09 knob ass'y, lever switch
X-48049-05 knob ass'y, SPEAKER switch
X-48049-04 knob ass'y, control
4-804-239 felt, light shield
2-031-956 escutcheon, pilot lamp
2-031-965-02 illuminator, pilot lamp
7-684-023-01 N 3 4
1-514-369-23 switch, lever (POWER) (GEP and General Export Model)
1-514-965 switch, lever (POWER) (NEP Model)
2-051-919 escutcheon, HEADPHONE jack
7-682-148-01 ⊕ P 3 x 8
1-514-648 switch, rotary (TONE control, BASS)
1-507-190-12 jack, HEADPHONE
7-682-947-01 ⊕ PSW 3 x 6
7-682-547-01 ⊕ B 3 x 6
7-682-960-01 ⊕ PSW 4 x 6
1-514-522 switch, rotary (SPEAKER)
1-517-021 socket, pilot lamp
7-632-157-50 shade, pilot lamp
1-518-052-11 lamp, pilot 2.5 V
SONY



Note:

① 1-532-237 fuse, 3.15AT
② 1-532-325 fuse, 6.3AT
③ 1-532-235 fuse, 315mAT
④ 1-532-078 fuse, 1AT
⑤ 1-441-688-12 transformer, power (GEP and General Export Model)
1-441-830-11 transformer, power (NEP Model)

SECTION 7
ELECTRICAL PARTS LIST

MOUNTED CIRCUIT BOARDS

Ref. No.	*Part No.*	*Description*
	X-48049-21-3	preamplifier circuit board
	8-982-587-22	power amplifier circuit board
	X-48049-23-2	power supply circuit board
	8-982-587-88	muting circuit board

SEMICONDUCTORS

Ref. No.	*Part No.*	*Description*
D701 (D801)		diode, 10D-05
D702 (D802)		varistor, SV-31
D704 (D804)		diode, 10D-05
D705 (D805)		diode, 10D-05
D706 (D806)		diode, 10D-05
D707 (D807)		diode, 10D-05
D708 (D808)		diode, 10D-05
D709 (D809)		diode, 10D-05
D710 (D810)		diode, 10D-05
D711 (D811)		diode, 10D-2
D721		diode, SH-1S
D722		diode, SH-1S
D901		diode, 10D-05
D902		diode, 10D-05
D903		diode, 5B4
D904		diode, 10D-2
D905		diode, 10D-2
D906		diode, 10D-05
D907		diode, 10D-05
D908		diode, 10D-05
D909		diode, 10D-05
D910		diode, 1T23A
D911		SCR, 1RC20
D912		diode, CD-2
D913		diode, CDR-2
D914		diode, 10D-2
D915		diode, 10D-2
D917		diode, 1T243M
D918		diode, 10D-2
Q101 (Q201)		FET, 2SK23-22
Q102 (Q202)		transistor, 2SC632A
Q301 (Q401)		FET, 2SK23-37
Q302 (Q402)		FET, 2SK23-37
Q303 (Q403)		FET, 2SK23-35
Q701 (Q801)		transistor, 2SA705
Q702 (Q802)		transistor, 2SA705
Q704 (Q804)		transistor, 2SC1124A
Q705 (Q805)		transistor, 2SC633A
Q707 (Q807)		transistor, 2SC633A
Q708 (Q808)		transistor, 2SC633A
Q709 (Q809)		transistor, 2SA678
Q710 (Q810)		transistor, 2SC895
Q711 (Q811)		transistor, 2SA527
Q712 (Q812)		transistor, 2SD88A
Q713 (Q813)		transistor, 2SD88A
Q903		transistor, 2SC1124A
Q904		transistor, 2SA706
Q905		transistor, 2SC633A
Q906		transistor, 2SC895
Q907		transistor, 2SC805
Q908		transistor, 2SC634A
Q921		transistor, 2SC634A
Q922		transistor, 2SC634A
Q923		transistor, 2SC634A

TRANSFORMERS

Ref. No.	*Part No.*	*Description*
T osc	1-433-132-27	transformer, osc.
T	1-441-688-12	transformer, power (GEP and General Export Model)
	1-441-830-11	transformer, power (NEP Model)

CAPACITORS

All capacitance values are in μF except as indicated with p, which means $\mu\mu$F.

Ref. No.	*Part No.*	Value	Tolerance	Voltage	Type
C101 (C201)	1-121-411	47	$\pm^{100}_{10}$%	50 V	electrolytic
C102 (C202)	1-105-685-12	0.1	±10%	50 V	mylar
C103 (C203)	1-105-661-12	0.001	±10%	50 V	mylar
C104 (C204)	1-121-406	47	$\pm^{100}_{10}$%	3.15 V	electrolytic
C105 (C205)	1-121-413	100	$\pm^{100}_{10}$%	6.3 V	electrolytic
C106 (C206)	1-121-413	100	$\pm^{100}_{10}$%	6.3 V	electrolytic
C107 (C207)	1-106-005-12	0.0015	±5%	50 V	mylar
C108 (C208)		– discarded –			
C109 (C209)	1-106-019-12	0.0056	±5%	50 V	mylar

Ref. No.	Part No.	Description			
C110 (C210)	1-105-689-12	0.22	±10%	50V	mylar
C301 (C401)	1-101-888	68p	±5%	50V	ceramic
C302 (C402)	1-106-041-12	0.047	±5%	50V	mylar
C303 (C403)	1-105-689-12	0.22	±10%	50V	mylar
C304 (C404)	1-105-661-12	0.001	±10%	50V	mylar
C305 (C405)	1-121-420	220	$\pm^{100}_{10}\%$	10V	electrolytic
C306 (C406)	1-106-033-12	0.022	±5%	50V	mylar
C307 (C407)	1-105-675-12	0.015	±10%	50V	mylar
C308 (C408)	1-106-025-12	0.01	±5%	50V	mylar
C309 (C409)	1-121-413	100	$\pm^{100}_{10}\%$	6.3V	electrolytic
C310 (C410)	1-121-392	3.3	$\pm^{150}_{10}\%$	25V	electrolytic
C312 (C412)	1-121-392	3.3	$\pm^{150}_{10}\%$	25V	electrolytic
C313 (C413)	1-106-033-12	0.022	±5%	50V	mylar
C314 (C414)	1-105-673-12	0.01	±10%	50V	mylar
C315 (C415)	1-105-685-12	0.1	±10%	50V	mylar
C316 (C416)	1-106-033-12	0.022	±5%	50V	mylar
C317 (C417)	1-101-861	15p	±5%	50V	ceramic
C318 (C418)	1-106-041-12	0.047	±5%	50V	mylar
C319 (C419)	1-106-033-12	0.022	±5%	50V	mylar
C320 (C420)	1-106-025-12	0.01	±5%	50V	mylar
C321 (C421)	1-106-025-12	0.01	±5%	50V	mylar
C322 (C422)	1-101-099	400p	±20%	50V	ceramic
C323 (C423)	1-101-099	400p	±20%	50V	ceramic
C701 (C801)	1-105-693-12	0.47	±10%	50V	mylar
C702 (C802)	1-121-469	10	$\pm^{100}_{10}\%$	10V	electrolytic
C704 (C804)	1-102-943	6p	±0.5pF	50V	ceramic
C705 (C805)	1-121-425	470	$\pm^{100}_{10}\%$	10V	electrolytic
C706 (C806)	1-121-405	33	$\pm^{100}_{10}\%$	50V	electrolytic
C707 (C807)	1-121-405	33	$\pm^{100}_{10}\%$	50V	electrolytic
C708 (C808)	1-105-681-12	0.047	±10%	50V	mylar
C709 (C809)	1-105-681-12	0.047	±10%	50V	mylar
C710 (C810)	1-105-679-12	0.033	±10%	50V	mylar
C711 (C811)	1-121-738	10	$\pm^{100}_{10}\%$	50V	electrolytic
C712 (C812)	1-107-002	50p	±10%	500V	silvered mica
C714 (C814)	1-107-091	180p	±5%	50V	silvered mica
C715 (C815)	1-121-413	100	$\pm^{100}_{10}\%$	6.3V	electrolytic
C911	1-121-559	50	$\pm^{100}_{10}\%$	100V	electrolytic
C913 (C921)	1-105-725-12	0.1	±10%	100V	mylar
C914	1-121-559	50	$\pm^{100}_{10}\%$	100V	electrolytic
C915	1-121-793	6,000	$\pm^{100}_{10}\%$	80V	electrolytic
C916	1-121-426	470	$\pm^{100}_{10}\%$	16V	electrolytic
C917	1-105-917-12	0.022	±20%	200V	mylar
C918	1-105-917-12	0.022	±20%	200V	mylar
C919	1-121-559	50	$\pm^{100}_{10}\%$	100V	electrolytic
C922	1-121-559	50	$\pm^{100}_{10}\%$	100V	electrolytic
C923	1-121-793	6,000	$\pm^{100}_{10}\%$	80V	electrolytic
C924	1-121-426	470	$\pm^{100}_{10}\%$	16V	electrolytic
C925	1-105-917-12	0.022	±20%	200V	mylar
C926	1-105-917-12	0.022	±20%	200V	mylar
C931	1-121-426	470	$\pm^{100}_{10}\%$	16V	electrolytic
C932	1-121-426	470	$\pm^{100}_{10}\%$	16V	electrolytic
C933	1-105-675-12	0.015	±10%	50V	mylar
C934	1-105-679-12	0.033	±10%	50V	mylar
C935	1-121-425	470	$\pm^{100}_{10}\%$	10V	electrolytic
C936	1-105-681-12	0.047	±10%	50V	mylar
C941	1-121-411	47	$\pm^{100}_{10}\%$	50V	electrolytic
C942	1-105-721-12	0.047	±10%	100V	mylar
C943	1-121-330	1,000	$\pm^{100}_{10}\%$	63V	electrolytic
C944	1-121-330	1,000	$\pm^{100}_{10}\%$	63V	electrolytic
C991	1-121-741	150	±20%	3.15V	electrolytic

RESISTORS

All resistance values are in ohms, ±5%, ¼ watts and carbon type unless otherwise indicated.

Ref. No.	Part No.	Description
R101 (R201)	1-244-713	47k
R102 (R202)	1-242-687	3.9k
R103 (R203)	1-242-709	33k
R104 (R204)	1-242-689	4.7k
R105 (R205)	1-242-669	680
R106 (R206)	1-242-691	5.6k
R107 (R207)	1-242-691	5.6k
R108 (R208)	1-242-667	560
R109 (R209)	1-210-051	2.2M
R110 (R210)	1-242-672	910
R111 (R211)	1-242-713	47k
R112 (R212)	1-210-124	1.1M
R113 (R213)	1-242-662	360
R114 (R214)	1-242-727	180k
R115 (R215)	1-242-695	8.2k
R116 (R216)	1-244-697	10k
R117 (R217)	1-244-719	82k
R118 (R218)	1-244-733	330k
R301 (R401)	1-242-717	68k
R302 (R402)	1-242-701	15k
R303 (R403)	1-242-745	1M

Ref. No.	Part No.	Description			
R304 (R404)	1-242-683	2.7k			
R305 (R405)	1-242-687	3.9k			
R306 (R406)	1-242-721	100k			
R307 (R407)	1-242-703	18k			
R308 (R408)	1-242-721	100k			
R309 (R409)	1-242-673	1k			
R310 (R410)	1-244-493	6.8k		1/8 W	
R311 (R411)	1-244-473	1k		1/8 W	
R312 (R412)	1-244-474	1.1k		1/8 W	
R313 (R413)	1-244-469	680		1/8 W	
R314 (R414)	1-242-708	30k			
R315 (R415)	1-244-509	33k		1/8 W	
R316 (R416)	1-244-505	22k		1/8 W	
R317 (R417)	1-244-502	16k		1/8 W	
R318 (R418)	1-244-501	15k		1/8 W	
R319 (R419)	1-244-496	9.1k		1/8 W	
R320 (R420)	1-242-745	1M			
R321 (R421)	1-242-700	13k			
R322 (R422)	1-242-679	1.8k			
R323 (R423)	1-242-699	12k			
R324 (R424)	1-242-683	2.7k			
R325 (R425)	1-244-487	3.9k		1/8 W	
R326 (R426)	1-244-493	6.8k		1/8 W	
R327 (R427)	1-244-492	6.2k		1/8 W	
R328 (R428)	1-244-495	8.2k		1/8 W	
R329 (R429)	1-244-498	11k		1/8 W	
R330 (R430)	1-242-733	330k			
R331 (R431)	1-242-701	15k			
R332 (R432)	1-244-491	5.6k		1/8 W	
R333 (R433)	1-244-467	560		1/8 W	
R334 (R434)	1-244-471	820		1/8 W	
R335 (R436)	1-244-474	1.1k		1/8 W	
R336 (R436)	1-242-680	2k			
R341 (R441)	1-244-709	33k			
R342 (R442)	1-244-543	820k			
R343 (R443)	1-242-744	910k			
R344 (R444)	1-244-543	820k			
R345 (R445)	1-242-744	910k			
R508 (R608)	1-202-565	10	±10%	1/2 W	composition
R509 (R609)	1-207-167	500	±10%	1.5 W	wire-wound
R701 (R801)	1-244-739	560k			
R702 (R802)	1-221-967	10k (B), semi-fixed			
R703 (R803)	1-244-721	100k			
R704 (R804)	1-244-697	10k			
R705 (R805)	1-244-677	1.5k			
R706 (R806)	1-244-649	100			
R707 (R807)	1-244-721	100k			
R708 (R808)	1-244-715	56k			
R709 (R809)	1-244-681	2.2k			
R710 (R810)	1-244-679	1.8k			
R711 (R811)	1-244-705	22k			
R712 (R812)	1-244-679	1.8k			
R713 (R813)	1-202-587	3.9k	±10%	1/2 W	composition
R714 (R814)	1-202-587	3.9k	±10%	1/2 W	composition
R715 (R815)	1-221-967	10k (B), semi-fixed			
R716 (R816)	1-244-681	2.2k			
R717 (R817)	1-244-661	330			
R718 (R818)	1-244-625	10			
R719 (R819)	1-244-661	330			
R720 (R820)	1-244-737	470k			
R721 (R821)	1-244-737	470k			
R722 (R822)	1-244-681	2.2k			
R723 (R823)	1-244-681	2.2k			
R724 (R824)	1-244-673	1k			
R725 (R825)	1-244-673	1k			
R726 (R826)	1-244-681	2.2k			
R727 (R827)	1-244-681	2.2k			
R728 (R828)	1-244-673	1k			
R729 (R829)	1-244-673	1k			
R730 (R830)	1-244-653	150			
R731 (R831)	1-244-653	150			
R732 (R832)	1-202-557	220	±10%	1/2 W	composition
R733 (R833)	1-244-649	100			
R734 (R834)	1-244-625	10			
R735 (R835)	1-244-659	270			
R736 (R836)	1-205-803	0.5	±10%	5 W	wire-wound
R737 (R837)	1-205-803	0.5	±10%	5 W	wire-wound
R738 (R838)	1-202-525	10	±10%	1/2 W	composition
R739 (R839)	1-244-661	330			
R906 (R909)	1-244-713	47k			
R911	1-244-645	68			
R912	1-244-649	100			
R913	1-244-705	22k			
R914	1-244-645	68			
R915	1-244-649	100			
R916	1-244-705	22k			
R917	1-244-663	390			

Ref. No.	Part No.	Description
R931	1-202-573	1k
R932	1-202-573	1k
R933	1-244-666	510
R934	1-244-697	10k
R941	1-244-707	27k
R942	1-202-549	100 ±10% ½W composition
R943	1-244-705	22k
R944	1-202-533	22 ±10% ½W composition
R955	1-244-705	22k
R956	1-221-996	5k (B), semi-fixed
R957	1-244-686	3.6k
R991	1-242-663	390
R992	1-242-709	33k
R993	1-242-687	3.9k
R994	1-242-725	150k
R995	1-202-597	10k ±10% ½W composition
R996	1-242-697	10k
R997	1-242-711	39k
R998	1-242-690	5.1k
R999	1-242-690	5.1k
RV301 (RV401)	1-221-844	250k, variable (BALANCE control)
RV302 (RV402)	1-222-445	250k, variable (VOLUME control)
		SWITCHES
S1	1-514-650	switch, rotary (FUNCTION 1)
S2	1-514-651	switch, lever/rotary (FUNCTION 2)
S3	1-513-338	switch, lever/rotary (MONITOR)
S4	1-514-795	switch, rotary (MODE)
S5	1-513-338	switch, lever/rotary (LOUDNESS)
S6	1-514-648	switch, rotary (TONE control, BASS)
S7	1-514-652	switch rotary (TONE control, TREBLE)
S8	1-513-338	switch, lever/rotary (HIGH FILTER)
S9	1-513-338	switch, lever/rotary (LOW FILTER)
S10	1-514-478	switch, slide (PRE AMP/POWER AMP)
S11	1-514-522	switch, rotary (SPEAKER)
S12	1-514-369-23	switch, lever/rotary (POWER) (GEP and General Export Model)
	1-514-965	switch, lever/rotary (POWER) (NEP Model)
		MISCELLANEOUS
	1-507-190-12	jack, HEADPHONE
	1-507-260	jack, AUX-3
	1-507-268	phono jack, 8-P
	1-507-313	phono jack, 10-P
	1-509-029	REC/PB connector
	1-509-341-13	ac outlet (General Export Model only)
	1-509-445	ac input connector, 3-P (GEP and NEP Model only)
	1-517-021	socket, pilot lamp
	1-518-052	lamp, pilot
	1-526-165	voltage changeover block
	1-526-502	socket, transistor
	1-532-325	fuse, 6.3AT (F2, F3) (NEP Model only)
	1-532-256	fuse, 6.3A (F2, F3) (GEP and General Export Model only)
	1-532-237	fuse, 3.15AT (F1) (NEP Model only)
	1-532-167	fuse, 5A (F1) (General Export Model only)
	1-532-255	fuse, 5A (F1) (GEP Model only)
	1-532-078	fuse, 1AT (F4) (NEP Model only)
	1-532-235	fuse, 315 mAT (F5) (NEP Model only)
	1-533-082	fuse holder, 5-P (NEP Model only)
	1-533-048	fuse post (General Export Model only)
	1-536-047	pin, connecting
	1-536-146	terminal strip, 1L1 (A)
	1-536-179	terminal strip, 1L1 (C)
	1-536-189	terminal strip, 1L1 (GEP Model only)
CP	1-231-057	encapsulated component, 120Ω + 0.033μF (General Export Model only)
	1-534-487-22	cord, power (General Export Model only)
	1-506-108	pin, connecting