

General Export Model









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SECTION 1 TECHNICAL DESCRIPTION

1-1. TECHNICAL SPECIFICATIONS

Rated output:

2.6 W, per channel, both channels

operating, 8 ohms

Technical specifications for the HST-399 are listed

in Table 1.

Power bandwidth: 45 Hz to 15 kHz, 8 ohms, 1HF

Table 1. HST-399 TECHNICAL SPECIFICATIONS

Harmonic distortion:

Less than 5% at 1 kHz at rated

output

Fm Tuner Section

87.5 to 108 MHz

 $3.0 \,\mu\text{V} \, (\text{S/N} = 30 \,\text{dB})$

Input sensitivity:

PHONO: 500 mV, 2.8 M ohms

TAPE:

300 mV, 60 k ohms

MIC: $0.8 \,\mathrm{mV}$

REC/PB: 300 mV, 60 k ohms

Sensitivity:

Intermediate frequency:

Frequency range:

10,7 MHz

Signal-to-noise

ratio:

PHONO:

greater than 55 dB greater than 60 dB

TAPE: REC/PB

BASS:

80 mV

Cassette Section

REC/PB (output): 40 mV, 88 k ohms

(input): greater than 60 dB

TREBLE: ±8 dB at 10 kHz

weighting network "B"

±10 dB at 100 Hz

Signal-to-noise ratio:

Selectivity:

60 dB

20 dB, IHF

Image rejection:

20 dB

I-f rejection:

50 dB

300 ohms balanced with ac line

antenna

Fm stereo separation:

Antenna:

Greater than 30 dB at 400 Hz

Harmonic

distortion:

Mono 2.0% at 400 Hz 100% mod.

SCA suppression:

19 kHz, 38 kHz

suppression:

46 dB

50 dB

Tape speed: Stereo 2.0% at 400 Hz 100% mod.

Frequency

response:

50 Hz to 10 kHz (-15 dB)

4.8 cm/sec (11/s inch/sec)

Recording bias

Tone controls:

REC out:

frequency:

85 kHz

Flutter and wow:

less than 0.5%

Frequency range:

530 to 1,605 kHz

A-m Tuner Section

455 kHz

Input:

Power

MIC (0.8 mV)

General

Approx. 20W

Intermediate frequency:

Sensitivity:

48 dB/m, built-in antenna

Signal-to-noise

ratio:

50 dB

Image rejection:

38 dB at 1,400 kHz

I-f rejection:

20 dB at 1,000 kHz

Harmonic

distortion:

2.0%

Audio Amplifier Section Net weight:

Music power:

10W, both channels operating,

8 ohms 5% THD

Power

requirements:

consumption:

100, 117, 220, 240 V, 50/60 Hz

Dimensions:

21" (width) × 5" (height)

 $\times 11^{7/16}''$ (depth)

534 mm (width) × 126 mm (height) × 290 mm (depth)

13 lb 14 oz (6.3 kg)

Shipping weight:

17 lb (7.7 kg)



1-2. BLOCK DIAGRAM

A block diagram of the HST-399 is provided for your understanding of the overall operation.

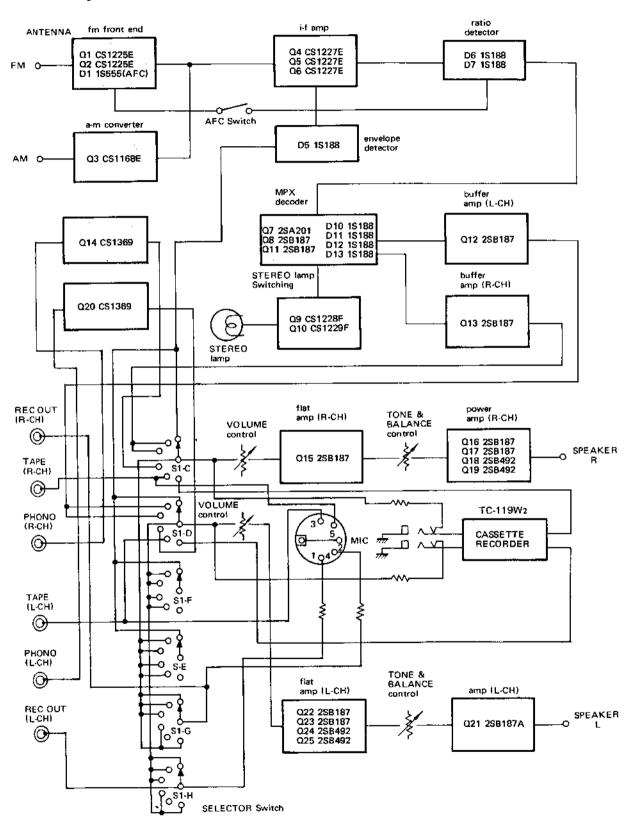


Fig. 1-1 Block diagram



1-3. CIRCUIT ANALYSIS

The following describes the functions of all stages and controls. The text sequence follows signal paths. Stages are listed by transistor reference designation at the left margin; major components are also listed in a similar manner. Refer to the block diagram on page 2 and the schematic diagram on page 35 and 36.

Fm Front End

Stage/Control

Function

ATT switch S4 (DX-LOCAL selector)

This selects the input network according to the signal strength for clear fm reception. In the DX position, input signals are directly fed to the fm front end. In the LOCAL position, excessively strong signals that may saturate the rf amplifier in the fm front end and cause distortion are attenuated in the resistive network.

Fm rf amplifier Ol A common-base circuit is ideally suited for stable amplification. The output signals of this stage are developed across the tuned circuit at the collector of Q1, and fed to the subsequent converter stage through coupling capacitor C6.

Fm frequency converter Q2 This common-base configuration serves as both mixer and localoscillator. The nonlinear baseemitter characteristic of Q2 is employed to function as a mixer. Transistor O2 and the major components such as C8, C10, C11, CT-F2, CV-F2 and L3 form a modified Colpitts oscillator, that provides the injection voltage for heterodyne operation. Tuned transformer FM IFT-A develops the 10.7 MHz i-f output and provides low-impedance link coupling to the i-f amplifier chain.

Afc circuit D2

The afc circuit maintains a stable local-oscillator frequency. Fre-

Stage/Control

Function

quency drift is detected as a do voltage change at the discriminator and fed to variable capacitance diode D2 through AFC switch S2. The barrier capacitance of D2 changes according to the dc voltage applied across it. Since the series circuit composed of D2 and C12 is connected in parallel with the tank circuit of the local oscillator, it operates as a tuning capacitor, compensating for frequency drift. In the ON position of \$2, relatively weak stations will not be received because strong adjacent stations will take over the afc.

I-f Amplifier Section

A-m frequency converter O3

When the FUNCTION switch is set to AM, transistor Q3 operates as an a-m frequency converter to produce 455-kHz if output. This circuit employs a Hartley oscillator with feedback applied to the base of Q3 from the tap on a-m oscillator coil L2, through the antenna coil L1, to generate injection voltage for heterodyning with incoming a-m signals.

I-f transformer A-M IFT-F I-f transformer A-M IFT-F develops the i-f signal and provides a path to ground through bypass capacitor C21 for the other heterodyne products.

Fm/a-m i-f amplifier Q4,5 The fm and a-m i-f strips use the same amplifier, tuned to both 10.7 MHz and 455 kHz. Switching is not necessary because of the wide difference in the intermediate frequencies.

A-m agc circuit Two kinds of age circuits are employed in this section, one is conventional reverse age and the other is delayed age.

Reverse age works as follows:

Stage/Control

Function

Reverse ago D5

The negative dc output voltage which is proportional to the input signal strength is picked off at the a-m detector (D5). It is filtered by R147, C29 and then fed back to the base of i-f amplifier Q4 through the secondary winding of A-M IFT-F and FM IFT-A. As a result, the bias current in Q4 decreases, reducing its gain.

Delayed ago D3, R12, R15 Delayed agc is also used to control the i-f amplifier's gain, especially when a relatively strong signal is The basic concept of received. this age circuit is that the tuned amplifier's gain is greatly affected by the "Q" of the tank circuit. In this circuit, D3 acts as a shunting resistance which reduces effective "Q" of the tank circuit of A-M IFT-F to decrease amplifier's gain. Normally, voltage drops across R12 and R15 place a reverse bias on D3, so it presents a large value of resistance. When a strong signal is received, the collector current in O4 is reduced by means of reverse bias agc. This in turn eliminates the reverse bias on D3, forcing it to conduct. As a result, the tank circuit of A-M IFT-F is shunted by the low forward resistance of D3. This drastically reduces the effective "Q" of the tank circuit.

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Fm i-f amplifier Amplifies the 10.7-MHz signals to the level required to drive the ratio detector.

Ratio detector D6, D7 FM IFT-D FM IFT-E

Discriminator transformers FM IFT-D and FM IFT-E, and diodes D6 and D7 form a balanced ratio detector that transforms the frequency-modulated signal into an audio signal which appears across C36.

Envelope detector **D**5

Diode D5 acts as an envelope detector for a-m signals.

A bypass capacitor (C30) removes the 455-kHz component in the detected signals. Audio output is, on the other hand, furnished to Stage/Control

Function

both audio amplifier chains.

Multiplex Decoder Section

SCA trap MT-D, C113 The composite stereo signal passes through the parallel trap consisting of MT-D and C113. This trap removes the unwanted SCA signals to provide a clean composite stereo signal.

07

Buffer amplifier This stage serves two functions. It extracts the 19-kHz pilot signal by means of a tuned circuit at its collector and provides a low-impedance source of composite stereo signal (without the pilot carrier) at its emitter. A parallel resonant circuit in the emitter circuit eliminates the 19-kHz pilot signal in the composite stereo signal.

19-kHz amplifier Q8

Amplifies the 19-kHz drive voltage for the frequency doubler (D8 and

Frequency doubler D8, D9

Signals developed at the collector of Q8 are transformer-coupled to full-wave rectifier D8 and D9. The output of this rectifier is not filtered, resulting in two negative pulses for each input cycle. Thus the 19-kHz pilot-carrier frequency is effectively doubled by D8 and However, the waveform is not sinusoidal at the base of Ol 1.

38-kHz amplifier 011

The 38-kHz pulses produced by D8 and D9 are amplified by Q11. The tank circuit at the collector of Q11 is tuned to 38 kHz to restore these pulses to a sinusoidal switching signal. This signal is transformer-coupled to the bridge-type demodulator to supply the sampling drive.

STEREO lamp circuit Q9, Q10

The STEREO indicator lamp lights when an fm stereo signal is reæived. The output voltage of the frequency doubler is supplied to the base of Q9, which is normally cur off. The circuit operates as fd lows: When a composite stereo signal is Stage/Control

D12, D13

Function

applied to the multiplex decoder, the negative 38-kHz pulses produced

by the frequency doubler force

O9 into conduction. This, in turn,

makes Q10 conduct, thus lighting

Stage/Control

Function

Audio Amplifier Section

Since the audio amplifier section contains two identical amplifier chains, only the right channel will be described. Component reference designations for the left channel are given in parentheses.

The demodulator circuit employs Multiplex. four diodes in a balanced-bridge demodulator arrangement. This system has the D10, D11,

the STEREO lamp,

advantage of cancelling residual rf components (38-kHz signal, some

19-kHz signal, and higher-order harmonics of these frequencies). "L" and "R" components are developed at each side of the bridge as the result of demodulation, when the receiver is operated in the In the monaural stereo mode. mode, the emitter circuit of Q11 is opened, cutting off the 38 kHz

stereo signal is applied to the demodulator. Diodes D10~D13 are forward

carrier. Thus, only the composite

biased to avoid nonlinear distortion.

capacitors provide De-emphasis These C58, C62 roll-off at high-audio frequencies necessary to compensate for preemphasis at the transmitter.

38-kHz filter This filter eliminates the 38-kHz carrier, thereby preventing carrier leak.

"L" and "R" audio signals are Buffer amplified to the level required to amplifier Q12, Q13 drive the following audio preampli-

The network that connects the Channel emitters of Q12 and Q13, provides separation a form of negative feedback beadj. VR5 tween left and right channels. Any residual inverted "L" signals in the "R" channel are cancelled out by the "L" signal from the "L" The same is true of channel. residual "R" signals in the "L" channel. VR5 is therefore set for

maximum channel separation.

This stage employs the common-Preamplifier Q14 (Q20) collector configuration (emitter follower). This has the advantage of high-input impedance and low-

output impedance.

VOLUME control VR1 C100, C101, R132 (C103, C102, R133)

The signal level applied to the flat amplifier is determined by the set-Loudness circuit ting of VR1. In addition, the loudness circuit compensates for the characteristics of the human ear, whose tonal response varies according to the loudness of the sound being heard. High- and lowfrequency components are increased in inverse proportion to the VOLUME control setting.

Flat These stages amplify the low-level amplifiers signal provided by preamplifier Q14 Q15, Q16 and cassette recorder (or tape re-(Q21, Q22) corder connected to the TAPE or

REC/PB jack) to the level required at the input of the power amplifier.

BASS control This control has a range of ±10 dB VR3 at 100 Hz.

TREBLE This control has a range of ±8 dB at control VR4 10 kHz.

BALANCE This control optimizes stereo recontrol VR2 production by attenuating either channel's signal level.

Driver Q17 Transistor Q17 provides enough (Q23) signal to drive the power transistors.

Driver Transformer T1 provides equal but transformer oppositely-phased output to drive T1 (T2) the push-pull power-output stage.

Power These power transistors operate as amplifier emitter followers in the single-Q18, Q19 ended push-pull configuration, and (Q24, Q25) deliver power to the speakers.



SECTION 2 DISASSEMBLY AND REPLACEMENT PROCEDURES

WARNING

Unplug the ac power cord before starting any disassembly or replacement procedures.

2-1. TOOLS REQUIRED

The following tools are required for performing disassembly and replacement procedures on the HST-399.

Jacknut driver
Screwdriver, Phillips head
Diagonal cutters
Contact cement
Cement solvent
Soldering iron, 40-150 watt
Solder, rosin core
Tape, electrical
Tape, adhesive
Wrench, 6-inch adjustable
Pliers, long-nose
Silicone grease

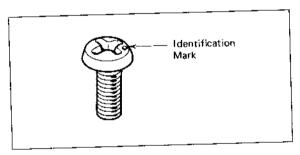
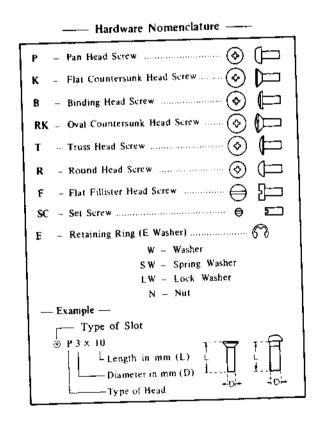


Fig. 2-1 ISO screw

2-2. HARDWARE IDENTIFICATION GUIDE

The following chart will help you to decipher the hardware codes given in this service manual.

NOTE: Some screws in the HST-399 are manufactured to the specifications of International Organization for Standardization (ISO). This means that the new and old screws are not interchangeable because ISO screws have a different number of threads per mm compared to the old ones. The ISO screws have an identification mark on their heads as shown in Fig. 2-1.



2-3. RECEIVER UNIT REMOVAL

- Remove all control knobs by pulling them off.
- Remove the nut securing the HEADPHONE jack with a jacknut driver.
- 3. Remove the six screws at the rear hardboard; two of them (+P 2.6×6) secure the ATT switch, and the four others (wood screw +R 3.1×10) secure the hardboard to the wooden case. See Fig. 2-2.
- 4. Remove the seven screws (+P 3x20) at the bottom of the wooden case. See Fig. 2-2.
- Disconnect 7 pin plug and two-pairs of Phono plug connecting between receiver unit and cassette deck.
- Carefully draw the receiver unit out of the wooden case. Care should be taken so as not to damage the tuning-dial system.

24. FRONT-END BOARD REMOVAL

- 1. Remove the receiver unit as described in Procedure 2-3.
- Turn the tuning shaft to place the dial-pointer in the center of the dial-scale back-plate. Then loosen one of the set screws on the tuning-capacitor drive-drum.
- Turn the tuning shaft once more to set the pointer at the right side of the back-plate.
 Loosen the remaining set screw on the drivedrum.
- 4. Remove the tuning-capacitor drive-drum and lean it against the front sub-chassis, then fix it with adhesive tape as shown in Fig. 2-3.
- 5. Remove the nut and two screws (+K 2.6×4) that secure the front-end block to the chassis, and take out the front-end board. See Fig. 2-3.

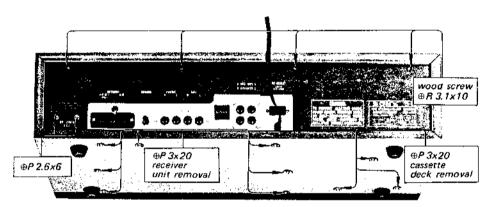


Fig. 2-2 Rear panel and bottom view



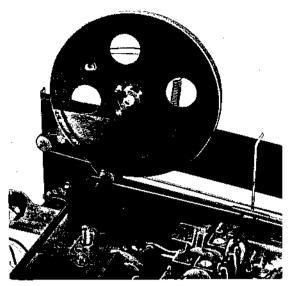


Fig. 2-3 Tuning-capacitor drive-drum removal

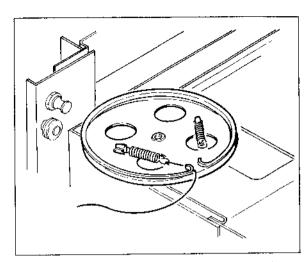


Fig. 2-4 Tuning-capacitor drive-drum installation

2-5. DIAL-CORD RESTRINGING

- 1. Cut a 45-inch (1,150mm) length of dial cord.
- Rotate the tuning-capacitor shaft fully clockwise to set the tuning capacitor at its minimum capacitance position.
- 3. Install the tuning-capacitor drive-drum as illustrate in Fig. 2-4, then tighten the two set screws of the drive-drum.
- 4. Tie the end of the cord to a spring and hook it to the appropriate tab of the drum. Hook a

- spring to the other tab of the drum, as shown in Fig. 2-4.
- 5. Wrap the cord a half turn clockwise along the groove of the drum. See Fig. 2-5.
- 6. Run the cord over pulleys A and B, and wrap two turns counterclockwise around the tuning shaft. See Fig. 2-5.
- 7. Run the cord over pulley C and wrap a half turn clockwise around the drive-drum. See Fig. 2-5.
- 8. Hook the cord to the other end of the coil spring.

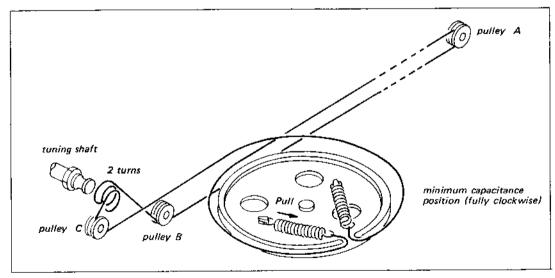


Fig. 2-5 Complete dial cord stringing

- 9. Puil the cord and tie it to the end of the spring to give it the proper tension while stretching the coil spring. See Fig. 2-5.
- 10. After completing the dial-cord stringing, make sure that the tuning system works properly.
- 11. Put the dial-pointer on the cord, and move it two-inches (50mm) away from the right end of the dial-scale back-plate at the minimum capacitance position of the tuning capacitor, as shown in Fig. 2-6.
- Apply a drop of contact cement to the tabs of the dial-pointer and the knot on the coil spring.

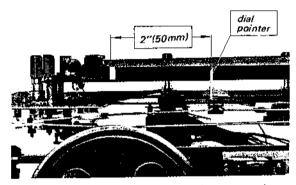


Fig. 2-6 Dial pointer position at minimum capacitance position

2-6. PILOT-LAMP REPLACEMENT

Dial Lamp

- 1. Remove the receiver unit as described in Procedure 2-3.
- Pry out the defective lamp from the socket, and then install the replacement lamp.

Stereo Lamp

1. Remove the receiver unit as described in Procedure 2-3.

- Mark on the dial-cord close to the tabs of the dial-pointer to facilitate reinstallation.
- 3. Apply a drop of paint-solvent to the tabs.

 After a few seconds, remove the pointer from the cord.
- Remove the dial-scale back-plate by loosening four screws (+P 2.6x6).
- 5. Remove the adhesive tape that fixes the stereo lamp and its shade, then take out the lamp.
- 6. Cut the leads of the stereo lamp approximately in the middle, but about 3/4-inch different in length,
- Solder the new lamp leads (also cut with a 3/4-inch difference in length) to the leads coming from the printed circuit board.
- Wrap the connection point with insulating tape.
- 9. Install the new stereo lamp and reassemble the dial-tuning system.

2-7. CONTROL AND SWITCH REPLACEMENT

First, remove the receiver unit as described in Procedure 2-3, then perform the following procedures.

POWER/VOLUME Control

- Remove the hex nut securing the POWER/ VOLUME control.
- 2. Remove the control and unsolder the wires and leads connected to the control lugs.
- 3. Solder these leads to a new control, then install it on the chassis.



FUNCTION Switch

- I. Unhook the dial pointer from the cord.
- Remove the four screws (+P 2.6×6) securing front subchassis to the main chassis as shown in Fig. 2-7.
- 3. Pull the front subchassis out.
- Remove the defective switch, and unsolder the leads from its lugs. Solder them to the new switch.
- 5. Install it to the front subchassis.

TONE and BALANCE Controls

- Remove the hex nut that secures the defective control or switch to the front of the chassis.
- 2. Take out the control or switch, and replace it.

AFC Switch

- Remove the two screws (+P 3 x 8) that secure the bar-antenna holders to the chassis.
- 2. Remove the screw (+P3x8) securing the ground lug near the AFC switch.
- Remove the hex nut that secures the AFC switch.

4. Move the bar antenna to permit removing the AFC switch, then take out the switch.

HEADPHONE Jack

- Remove the hex nut securing the HEADPHONE jack.
- 2. Take out the jack.
- Unsolder the leads from the jack, and resolder them to the replacement jack.
- 4. Install it to the front chassis.

2-8. POWER TRANSISTOR REPLACEMENT

- 1. Remove the four screws (+P 3×8) at each side of the chassis and two screws (+K 3×6) securing the power transformer bracket to the rear panel.
- 2. Push down the rear panel to allow applying a screwdriver to the heat-sink retaining screws (+P 3×16), as shown in Fig. 2-8.
- 3. Unscrew the screw while holding the nut on the transistor-mounting board with pliers, then remove the heat sink.
- Unsolder and straighten the transistor leads to permit transistor removal. Cut the leads if necessary.
- 5. Remove the transistor from the chassis.
- 6. When reinstalling the power transistor, make

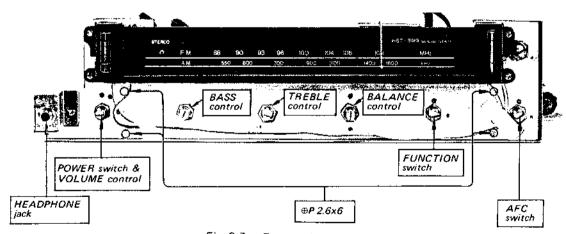


Fig. 2-7 Front subchassis removal



- sure that the transistor leads are sleeved with insulating tubing.
- Solder the transistor leads and install the heat sink with a coat of silicone grease inside the heat-sink depression in which the transistor is housed.
- 8. Secure the heat sink, then reassemble the rear chassis.

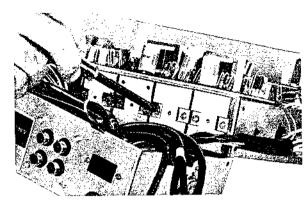
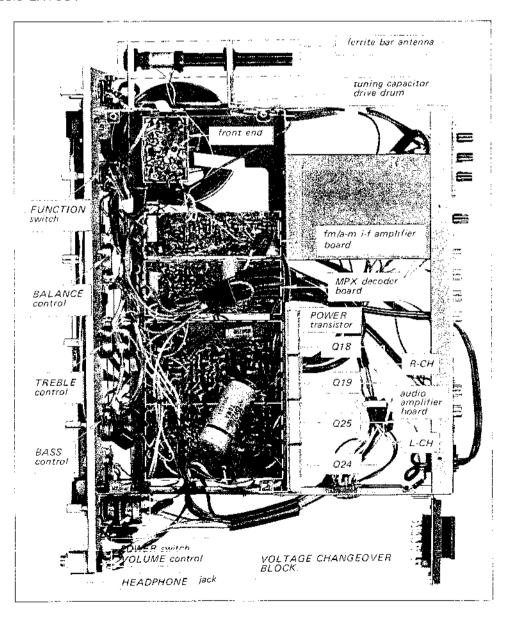


Fig. 2-8 Power transistor removal

2.9. CHASSIS LAYOUT





SECTION 3 ALIGNMENT AND ADJUSTMENT PROCEDURES

3-1, FM I-F STRIP ALIGNMENT

NOTE: There are two methods of fm i-f strip alignment. One is sweep generator alignment, and the other is signal generator alignment. You can use either of them.

Sweep Generator Alignment

Test Equipment Required

- 1. 10.7 MHz sweep generator
- 2. Oscilloscope
- 3, I-f probe (See Fig. 3-1.)
- 4. Alignment tools

Preparation

 Remove the receiver unit as described in Procedure 2-3.

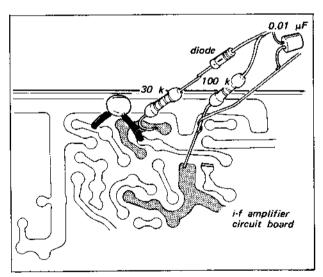


Fig. 3-2 1-f probe and oscilloscope connection

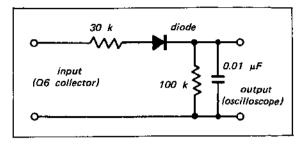


Fig. 3-1 1-f probe

- 2. Solder the input leads of the i-f probe to the collector of Q6 and ground on the i-f amplifier board (as shown in Fig. 3-2), and connect the output leads of the probe to the input cable of the oscilloscope.
- 3. Connect the output cable of the sweep generator across L3 on the front-end circuit board with alligator clips, as shown in Fig. 3-3.

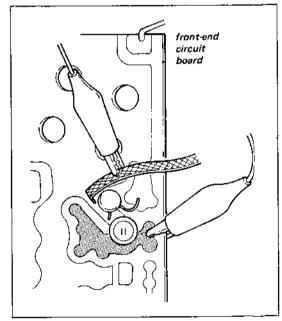


Fig. 3-3 Sweep generator connection

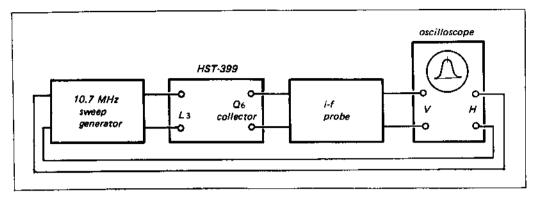


Fig. 3-4 Fm i-f strip alignment test setup, sweep generator alignment

Procedure

 With the equipment connected as shown in Fig. 3-4, set the sweep generator's controls as follows:

Center frequency 10.7 MHz Sweep width 1 MHz

Set the receiver's controls as follows:

VOLUME control Minimum FUNCTION switch FM AFC switch OFF

- 2. Adjust the oscilloscope controls to provide a visible indication.
- 3. Rotate the TUNING shaft to locate the hole of the tuning-capacitor drive-drum above transformer FM IFT-A on the front-end circuit board. This allows you to align transformer FM IFT-A with an alignment tool through the hole in the drum, as shown in Fig. 3-5.
- 4. Turn the cores of fm i-f transformers FM IFT-A (yellow), FM IFT-B (green), FM IFT-D (blue), to obtain a maximum and symmetrical response as shown in Fig. 3-6.
- 5. Repeat Step 4 until an optimum response is obtained,

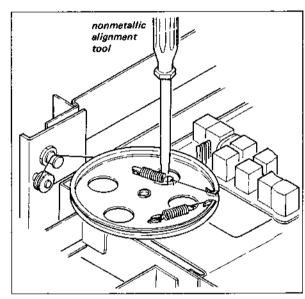


Fig. 3-5 Transformer FM IFT-A alignment

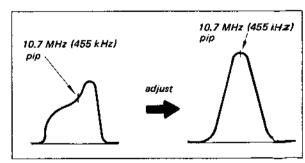


Fig. 3-6 Fm and a-m i-f alignment response curve

Signal Generator Alignment

Test Equipment Required

- 1. Standard fm signal generator
- 2. Ac VTVM
- 3. Alignment tools

Preparation

- 1. Remove the receiver unit as described in Procedure 2-3.
- Connect the input cable of the ac VTVM across the VOLUME-control lugs, as shown in Fig. 3-7.
- Connect the output cable of the signal generator to the lugs of the terminal strip located in back of the ANTENNA terminal, as shown in Fig. 3-8.

Procedure

 With the equipment connected as shown in Fig. 3-9, set the signal generator's controls as follows.

Carrier frequency	98 MHz
Modulation	
Output level	$60 \mu V (36 dB)$

Set the receiver's controls as follows:

VOLUME control	Minimum
FUNCTION switch	ΓM
AFC switch	OFF

2. Tune the set to 98 MHz precisely.

- 3. Turn the cores of fm i-f transformers 1-M IFT-A (yellow), FM IFT-B (green), FM IFT-C (green), and FM IFT-D (blue), to obtain a maximum reading on the VTVM.
- 4. Repeat Step 3 until a maximum reading is obtained.

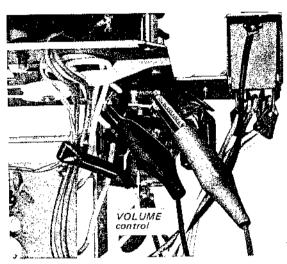


Fig. 3-7 VTVM connection

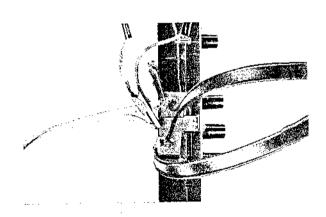


Fig. 3-8 Signal generator connection

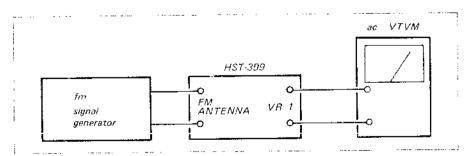


Fig. 3-9 Fm i-f strip alignment test setup, signal generator alignment

3-2. FM DISCRIMINATOR ALIGNMENT

NOTE: Two methods of discriminator alignment are available, sweep-generator alignment and signal generator alignment. You can use either of them.

Sweep Generator Alignment

Test Equipment Required

- 1. 10.7 MHz sweep generator
- 2. Oscilloscope
- 3. Mylar capacitor, 0.01µF
- 4. Alignment tools

Preparation

- 1. Remove the receiver unit as described in Procedure 2-3.
- 2. Solder a 0.01- μ F mylar capacitor across C36 on the i-f amplifier circuit board, as shown in Fig. 3-10.
- Connect the input cable of the oscilloscope across the mylar capacitor with alligator clips, as shown in Fig. 3-10.
- Connect the output cable of the sweep generator across L3 on the front-end circuit board with alligator clips, as shown in Fig. 3-3 on page 12.

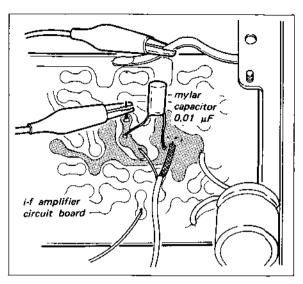


Fig. 3-10 Discriminator output connection

Procedure

 With the equipment connected as shown in Fig. 3-11, set the sweep generator's controls as follows:

Center frequency 10.7 MHz Sweep width 1 MHz

Set the receiver's controls as follows:

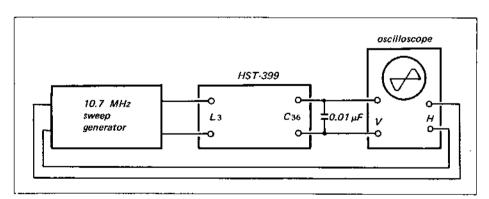


Fig. 3-11 Discriminator alignment test setup, sweep generator alignment



2. Adjust the controls of the oscilloscope to provide a visible indication.

NOTE: Two or three traces will be observed on the oscilloscope as the center frequency of the sweep generator varies. The trace you are looking for has the largest amplitude. Once you get it, decrease the sweep-generator output as low as possible.

3. Turn the core of transformer FM 1FT-E (pink) with an alignment tool to obtain the "S" curve response shown in Fig. 3-12.

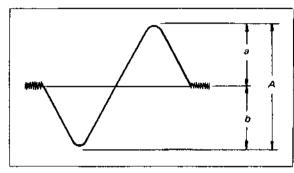


Fig. 3-12 "S" curve response

- 4. Turn the core of transformer FM IFT-D (blue) to obtain a maximum-amplitude indication on the oscilloscope.
- 5. Turn the core of FM IFT-E slightly to equalize the positive and negative peaks, as shown in Fig. 3-12.

$$\frac{A}{2} = a = b$$

 Disconnect the sweep generator and make sure that the oscilloscope displays only noise.

Signal Generator Alignment

Test Equipment Required

- 1. Standard fm/a-m signal generator
- 2. Oscilloscope

- 3. Mylar capacitor 0.01 μ F
- 4. Alignment tools

Preparation

- Remove the receiver unit as described in Procedure 2-3.
- Solder a 0.01-μF mylar capacitor across C36 on the i-f amplifier circuit board, as shown in Fig. 3-10 on page 15.
- Connect the input cable of the oscilloscope across the mylar capacitor with alligator clips as shown in Fig. 3-10.
- 4. Connect the output cable of the sweep generator across L3 on the front-end circuit board with alligator clips, as shown in Fig. 3-3 on page 12.

Procedure

1. With the equipment connected as shown in Fig. 3-13 on page 17, set the signal generator's controls as follows:

Carrier frequency10.7 MHz
ModulationA-m, 400 Hz, 30%
Output level1,000 µV (60 dB)

Set the receiver's controls as follows:

VOLUME control	Minimum
FUNCTION switch	FM
AFC switch	OFF

 Adjust the controls of the oscilloscope to provide a visible indication. A sine wave (400 Hz) should be observed on the oscilloscope.

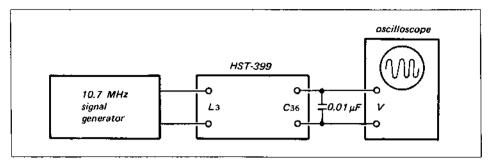


Fig. 3-13 Discriminator alignment test setup, signal generator alignment

3. Turn the core of transformer FM IFT-E (pink) to obtain minimum output, as shown in Fig. 3-14.

NOTE: At both extremes of core positions of FM IFT-E, decreased output will be observed. The real null point be obtained in the middle of the core thread length and maximum output occurs at each side of the true null point. Slowly and carefully turn the core to obtain minimum output.

33. FM FRONT-END ALIGNMENT

NOTE: Discriminator alignment should be performed first.

Test Equipment Required

Standard fm signal generator
 In case the generator is unavailable, off-the-air signals at end of the band will suffice.

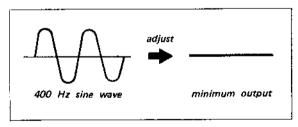


Fig. 3-14 Discriminator alignment output response

- 2. Ac VTVM
- 3. Alignment tools

Preparation

- Remove the receiver unit as described in Procedure 2-3.
- Connect the input cable of the ac VTVM across the VOLUME-control lugs, as shown in Fig. 3-7 on page 14.
- Connect the output cable of the signal generator to the lugs of the terminal strip located in back of the ANTENNA terminal, as shown in Fig. 3-8 on page 14.
- 4. With the equipment connected as shown in Fig. 3-15, set the receiver's controls as follows:

VOLUME control	Minimum
FUNCTION switch	FM
AFC switch	OFF

Signal-Generator Alignment

- 1. Follow the procedures given in Tables 1 and 2.
- 2. Repeat these procedures two or three times until an optimum response is obtained.



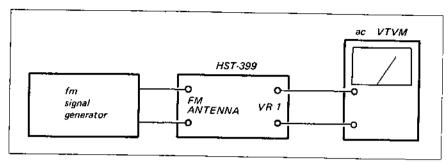


Fig. 3-15 Fm front-end alignment test setup

TABLE 1. Fm Frequency Coverage Alignment

Coupling Between Front End and SSG	SSG Frequency and Output Level	Tuning Capacitor	Ac VTVM Connection	Adjust	Indication
Direct	86 MHz 400 Hz, 100%, fm 60 μV (36 dB)	Maximum capacitance position	Across volume control lugs Fig. 3-7	OSC coil L3 Fig. 3-16	Maximum VTVM reading
Direct	109.5 MHz 400 Hz, 100%, fm 60 µV (36 dB)	Minimum capacitance position	Across volume control lugs Fig. 3-7	OSC trimmer CT-F2 Fig. 3-16	Maximum VTVM reading

TABLE 2. Fm Tracking Alignment

Coupling Between Fron End and SSG	SSG Frequency and Output Level	Tuning Capacitor	Ac VTVM Connection	Adjust	Indication
Direct	86 MHz 400 Hz, 100%, fm 60 µV (36 dB)	Maximum capacitance position	Across volume control lugs Fig. 3-7	RF coil L4 Fig. 3-16	Maximum VTVM reading
Direct	109.5 MHz 400 Hz, 100%, fm 60 μV (36 dB)	Minimum capacitance position	Across volume control lugs Fig. 3-7	RF trimmer CT-F1 Fig. 3-16	Maximum VTVM reading

Off-the-air Alignment

Accurate frequency coverage and tracking alignment can also be performed by utilizing off-the-air local fm signals. However, before performing the following procedure, be sure that the dial-pointer is correctly positioned, as described in Procedure 2-5 and AFC switch is set to OFF position.

NOTE: Tune in weak stations or use an inefficient antenna to obtain signals as weak as possible for accurate fm front-end alignment.

- 1. Follow the procedures given in Tables 3 and 4.
- Repeat these procedures two or three times until an optimum response is obtained.

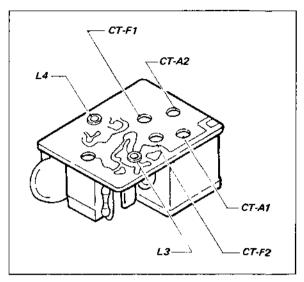


Fig. 3-16 Location of L3, L4, CT-F1, CT-F2, CT-A1 and CT-A2

TABLE 3. Fm Frequency Coverage Alignment

Receiver	Output Detector Connection	Adjust	Indication
Tune to the lowest-frequency station	Plug in headphone	OSC coil L3 Fig. 3-16	Maximum sound
Tune to the highest-frequency station	Plug in headphone	OSC trimmer CT-F2 Fig. 3-16	Maximum sound

TABLE 4. Fm Tracking Alignment

Receiver	Output Detector Connection	Adjust	Indication
Tune to the lowest-frequency station	Plug in headphone	RF coil L4 Fig. 3-16	Maximum sound
Tune to the highest-frequency station	Plug in headphone	RF trimmer CT-F1 Fig. 3-16	Maximum sound



3-4. SWITCHING TRANSFORMER ADJUSTMENT

Test Equipment Required

- 1. Standard fm signal generator
- 2. MPX stereo signal generator
- 3. Audio oscillator
- 4, Ac VTVM
- 5. Alignment tools

Preparation

- 1. Remove the receiver unit as described in Procedure 2-3.
- 2. Setup the equipment to produce fm stereo signals.
- 3. Connect the input cable of the distortion meter across the VOLUME-control lugs, as shown in Fig. 3-7.
- 4. Connect the output cable of the signal generator to the lugs of the terminal strip located in back of the GROUND terminal, as shown in Fig. 3-8.

Procedure

1. With the equipment connected as shown in Fig. 3-17, set the signal generator's controls as follows:

Carrier frequency	98 MHz
Modulation	External mod.
Output level	1,000 µV (60 dB)

The frequency modulation produced by the MPX stereo generator should be as follows:

```
Main channel (400 Hz) ...... 45% (33.75 kHz)
Sub channel (38 kHz) ....... 45% (33.75 kHz)
Pilot signal (19 kHz) ........ 10% (7.5 kHz)
```

The above mentioned modulation levels can be set as follows:

(a) With the equipment connected as shown in Fig. 3-17, set the MPX stereo generator's controls as follows:

MAIN CHANNEL C)FF
SUB CHANNEL	FF
19 kHz (PILOT)	N

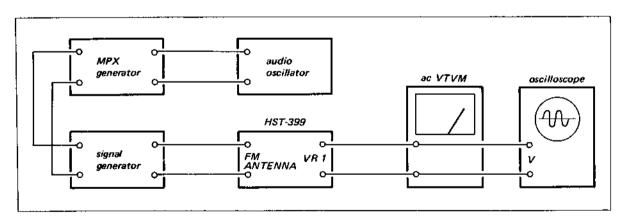


Fig. 3-17 Fm stereo distortion adjustment test setup



- (b) Adjust the MPX stereo generator output level to obtain a 7.5-kHz deviation on the fm SSG modulation indicator.
- (c) Reset the MPX stereo generator's controls as follows:

MAIN CHANNELON
SUB CHANNEL OFF
19 kHz (PILOT) OFF

- (d) Adjust the audio oscillator output controls to obtain a 33.75-kHz deviation on the fm SSG modulation indicator.
- (e) Set all controls to the ON position.
- 2. Set the receiver's controls as follows:

VOLUME control Minimum	
FUNCTION switch FM AUTO STER	ΕO
AFC switchOFF	

 Turn the core of switching transformer MT-B in the multiplex decoder board to obtain maximum output.

3-5. CHANNEL SEPARATION

Test Equipment Required

- 1. Standard fm signal generator
- 2. MPX stereo signal generator
- 3. Audio oscillator
- 4. Ac VTVM
- Alignment tools

Preparation

 Follow the preparation procedure described in 3-4, SWITCHING TRANSFORMER ADJUST-MENT.

Procedure

- Follow the procedure described in Steps 1 and 2 of 3-4, SWITCHING TRANSFORMER ADJUSTMENT.
- Record the output level of the left channel when the MPX generator input selector is set to the left channel.
- 3. Switch the input selector to the right, and read the residual signal level in the left channel.
- 4. The output-level to residual-level ratio represents the channel separation. Adjust separation adj. control VR5 (5k-B) on the multiplex decoder board for minimum residual level. Check the right channel for separation. Usually, some difference in channel separation exists. Readjust VR5 for minimum difference between left- and right-channel separation. While doing this, remember that the output level also changes according to the setting of VR5.

3-6. A-M I-F ALIGNMENT

NOTE: There are two methods of a-m i-f alignment. One is sweep generator alignment, and the other is signal generator alignment. You can use either of them

Sweep Generator Alignment

Test Equipment Required

- 1. 455-kHz sweep generator
- 2. Oscilloscope
- 3. Alignment tools



Preparation

- Remove the receiver unit as described in Procedure 2-3.
- Shunt the local oscillator capacitor CV-A2 with a 0.02μF capacitor to kill the local oscillator's operation as shown in Fig. 3-18.
- Connect the input cable of the oscilloscope across R148 on the i-f amplifier board, as shown in Fig. 3-19.
- 4. Connect the sweep generator's output cable to the AM external antenna terminal.

Procedure

 With the equipment connected as shown in Fig. 3-20, set the sweep generator's controls as follows:

Center	freque	quency		kHz
Sween	width		25	kHz

Set the receiver's controls as follows:

VOLUME control·····	.,	Minimum
FUNCTION switch		AM

- 2. Adjust the oscilloscope controls to provide a visible indication.
- Turn the cores of i-f transformer A-M IFT-F (yellow), A-M IFT-G (white) and A-M IFT-H (black) to obtain a maximum and symmetrical response as shown in Fig. 3-6 on page 13.
- 4. Repeat Step 3 above until an optimum response is obtained.

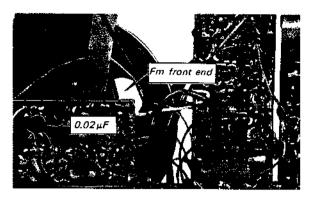


Fig. 3-18 Interruption of a-m local oscillator operation

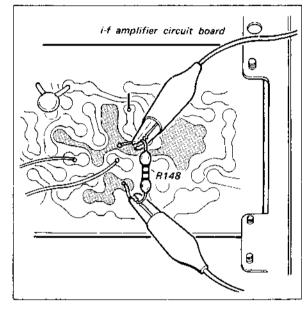


Fig. 3-19 A-m detector output connection

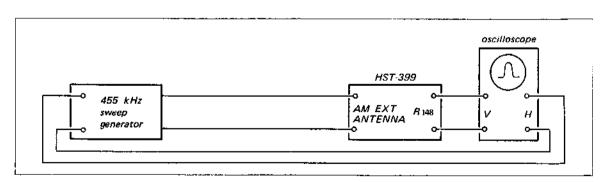


Fig. 3-20 A-m i-f alignment test setup, sweep generator alignment

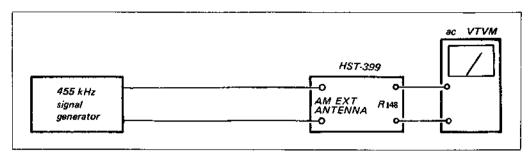


Fig. 3-21 A-m i-f alignment test setup, signal generator alignment

Signal Generator Alignment

Test Equipment Required

- 1. Standard a-m signal generator
- 2. Ac VTVM
- 3. Alignment tools

Preparation

Same as described in sweep generator alignment.

Procedure

1. With the equipment connected as shown in

Fig. 3-21, set the signal generator's controls as follows:

Carrier frequency	455 kHz
Modulation	A-m, 400Hz, 30%
Output level	1,000µV (60 dB)

Set the receiver's controls as follows:

VOLUME control ·	•••••	Minimum
FUNCTION switch		AM

- Turn the cores of i-f transformers A-M IFT-F (yellow), A-M IFT-G (white), and A-M IFT-H (black), to obtain a maximum reading on the meter.
- 3. Repeat Step 2 until a maximum reading on the meter is obtained.

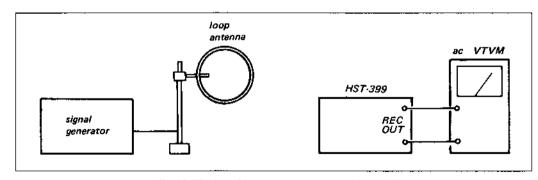


Fig. 3-22 A-m frequency coverage and tracking alignment test setup



3-7. A-M TUNER FREQUENCY COVERAGE AND TRACKING ALIGNMENT

Test Equipment Required.

1. Standard a-m signal generator

In case the generator is unavailable, off-the-air signals at end of the band will suffice.

- 2. Loop antenna
- 3. Ac VTVM
- 4. Alignment tools

Preparation

1. Remove the receiver unit as described in Procedure 2-3.

- 2. Connect the input cable of the ac VTVM to the REC OUT terminal.
- 3. With the equipment connected as shown in Fig. 3-22, set the receiver's controls as follows:

VOLUME control Minimum FUNCTION switch AM

Procedure

Signal Generator Alignment

- 1. Follow the procedures given in Tables 5 and 6.
- 2. Repeat these procedures two or three times until an optimum response is obtained.

TABLE 5. A-m Frequency Coverage Alignment

Coupling Between Receiver and SSG	SSG Frequency and Output Level	Tuning Capacitor	Ac VTVM Connector	Adjust	Indication
Loop or radiating antenna	520 kHz 400 Hz, 30%, a-m 1,000μV (60 dB)	Maximum capacitance position	REC OUT	OSC coil L2 Fig. 3-23	Maximum VTVM reading
Loop or radiating antenna	1,680 kHz 400 Hz, 30%, a-m 1,000 µV (60 dB)	Minimum capacitance position	Same as above	OSC trimmer CT-A2 Fig. 3-16	Maximum VTVM reading

TABLE 6. A-m Tracking Alignment

Coupling Between Receiver and SSG	SSG Frequency and Output Level	Tuning Capacitor	Ac VTVM Connector	Adjust	Indication
Loop or radiating antenna	620 kHz 400 Hz, 30%, a-m 1,000 µV (60 dB)	Tune to 620 kHz signal	REC OUT	Ant coil L1 Fig. 3-24	Maximum VTVM reading
Loop or radiating antenna	1,400 kHz 400 Hz, 30%, a-m 1,000 µV (60 dB)	Tune to 1,400 kHz signal	Same as above	Ant trimmer CT-A1 Fig. 3-16	Maximum VTVM reading



Off-the-air Alignment

Accurate frequency coverage and tracking alignment can also be performed by utilizing off-the-air local a-m signals. However, before performing the following procedure, be sure that the dial-pointer is correctly positioned, as in Procedure 2-5.

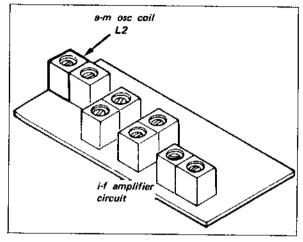


Fig. 3-23 Location of osc coil L2

NOTE: Tune in weak or long distance stations to obtain signals as low as possible for an accurate a-m tuner alignment.

- 1. Follow the procedures given in Tables 7 and 8.
- 2. Repeat these procedures two or three times until an optimum response is obtained.

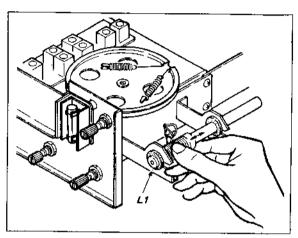


Fig. 3-24 Antenna coil L1 position adjustment

TABLE 7. A-m Frequency Coverage Alignment

Receiver	Output Detector Connection	Adjust	Indication
Tune in the lowest-frequency station	Plug-in headphone	OSC coil L2 Fig. 3-23	Maximum sound
Tune in the highest-frequency station	Plug-in headphone	OSC trimmer CT-A2 Fig. 3-16	Maximum sound

TABLE 8. A-m Tracking Alignment

Receiver	Output Detector Connection	A djust	Indication
Tune in the station around 620 kHz	Plug-in headphone	Ant coil L1 Fig. 3-24	Maximum sound
Tune in the station around 1,400 kHz	Plug-in headphone	Antenna trimmer CT-A1 Fig. 3-16	Maximum sound



SECTION 4 REPACKING

The HST-399's original shipping carton and packing material are the ideal container for shipping the unit. However, to secure the maximum

protection, the HST-399 must be repacked in these materials precisely as before. The proper repacking procedure is shown in Fig. 4-1.

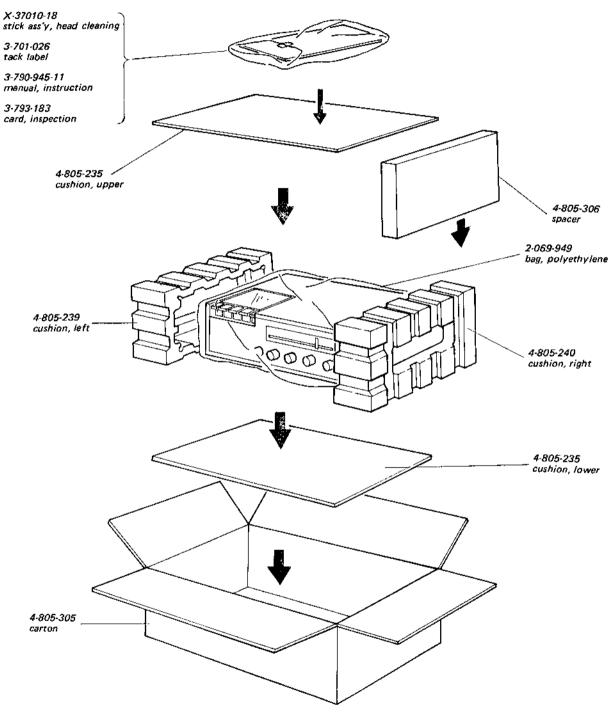


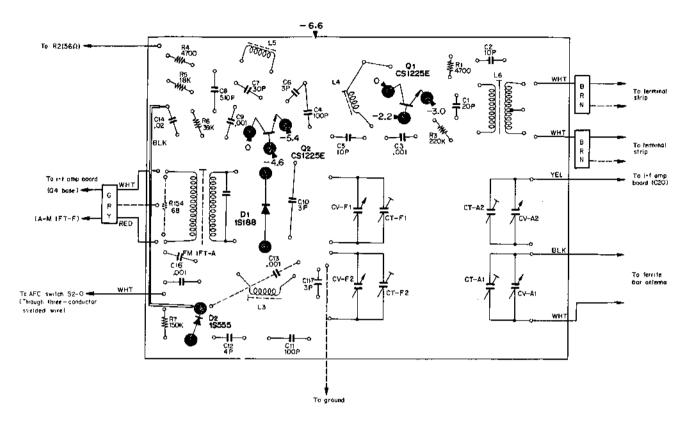
Fig. 4-1 Repacking



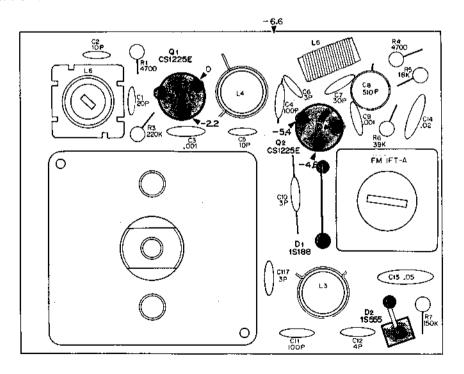
SECTIONS 5 DIAGRAMS

5-1. MOUNTING DIAGRAM - Fm Front-End Section -

- Conductor Side -



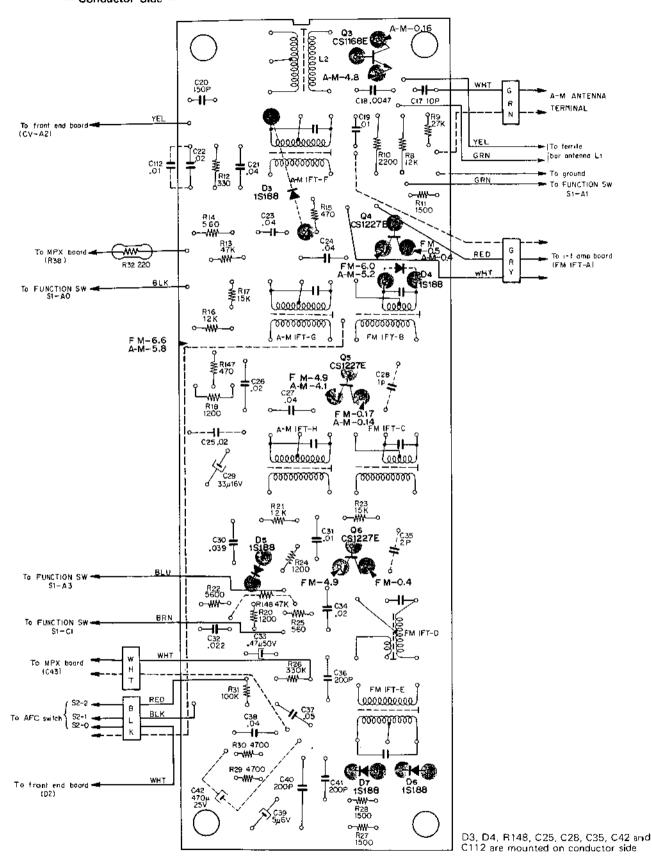
- Component Side -



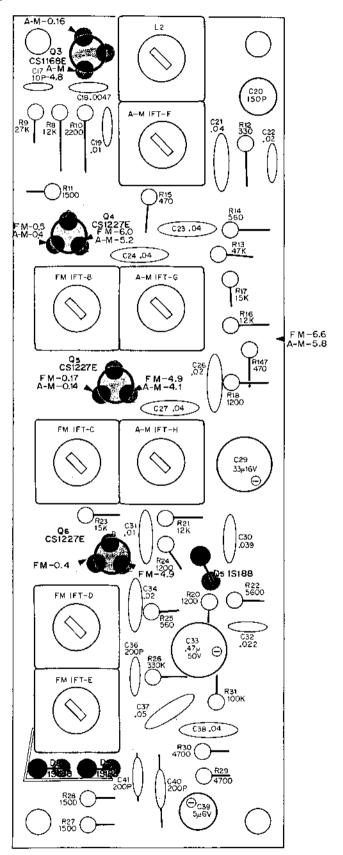


5-2. MOUNTING DIAGRAM - 1-f Amplifier Section -

- Conductor Side -



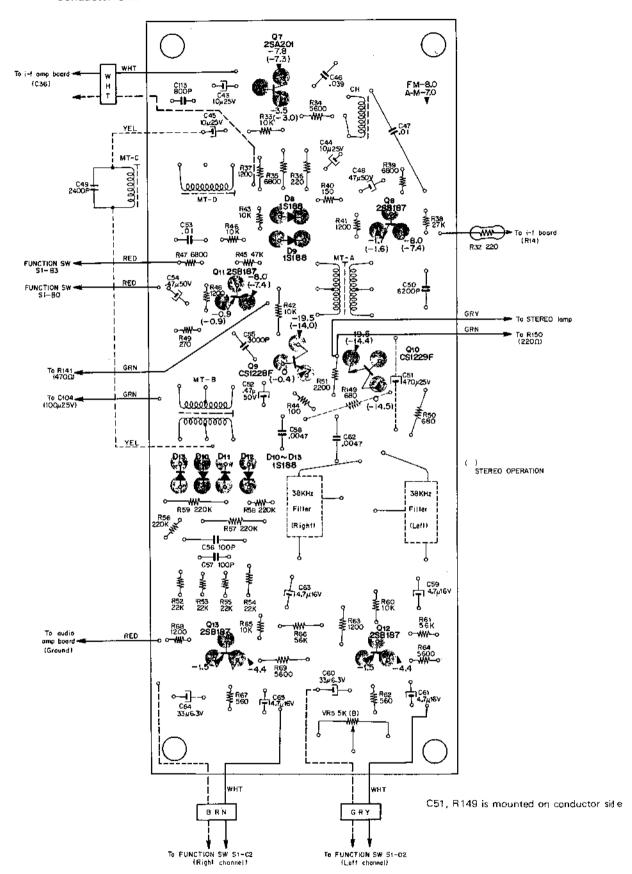
- Component Side -



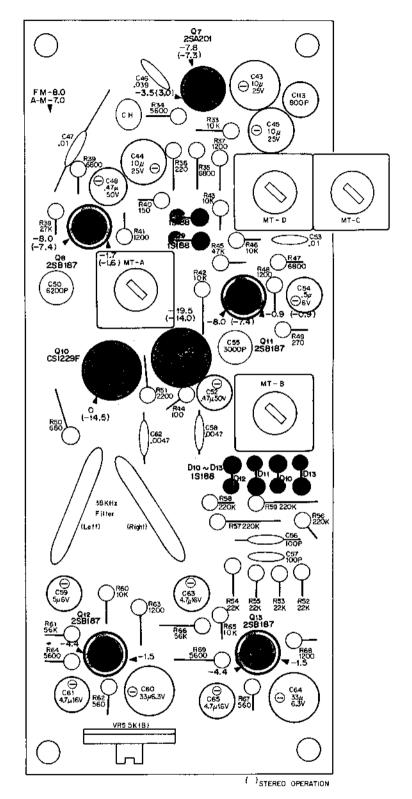


5-3. MOUNTING DIAGRAM - Multiplex Decoder Section -

- Conductor Side -



- Component Side -

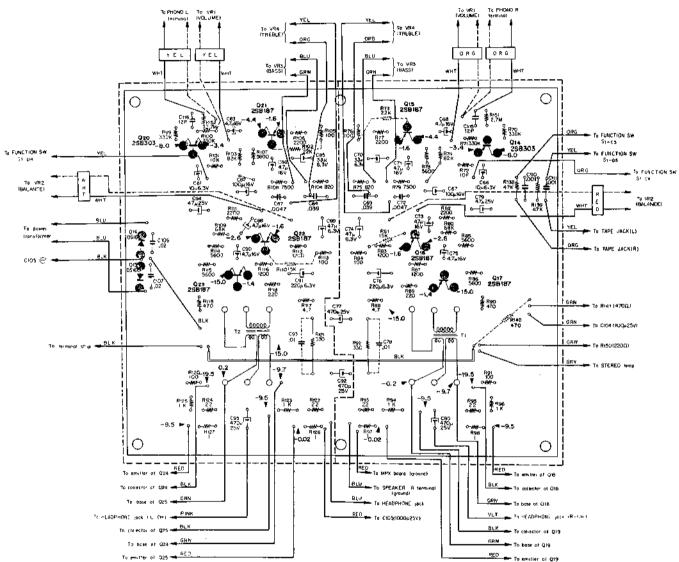




5-4. MOUNTING DIAGRAM - Audio Amplifier Section -

- Conductor Side -



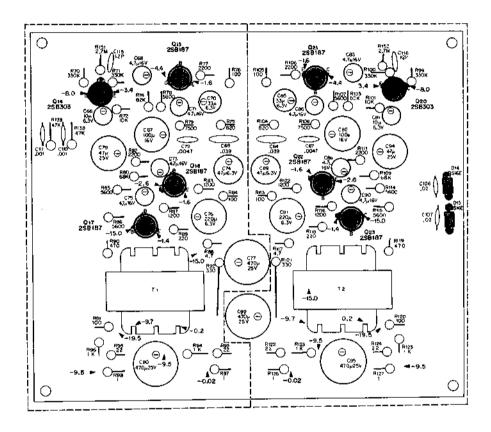


R73.R61.R102R110.H140.C76 and C93 are maunited on conductor 3.de

- Component Side -

RIGHT CHANNEL

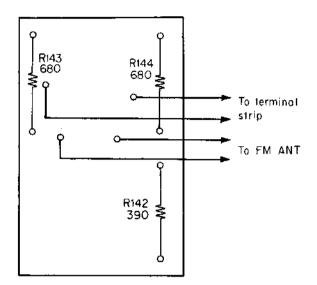
LEFT Channel



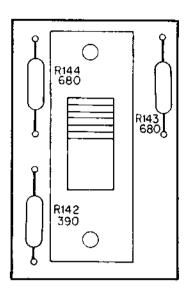


5-5. MOUNTING DIAGRAM - ATT Circuit Board -

- Conductor Side -

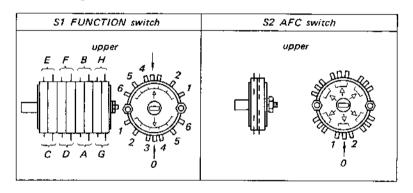


- Component Side -

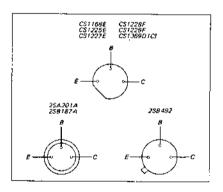


5-6. SCHEMATIC DIAGRAM NOTE

- Switch-lug Guide -



- Transistor-lead Guide -



Switch Position -

Symbol	Description	Position
<i>S1</i>	FUNCTION switch (AM-FM-STEREO -PHONO-TAPE-CASSETTE)	AM
S2	AFC switch	OFF

Note:

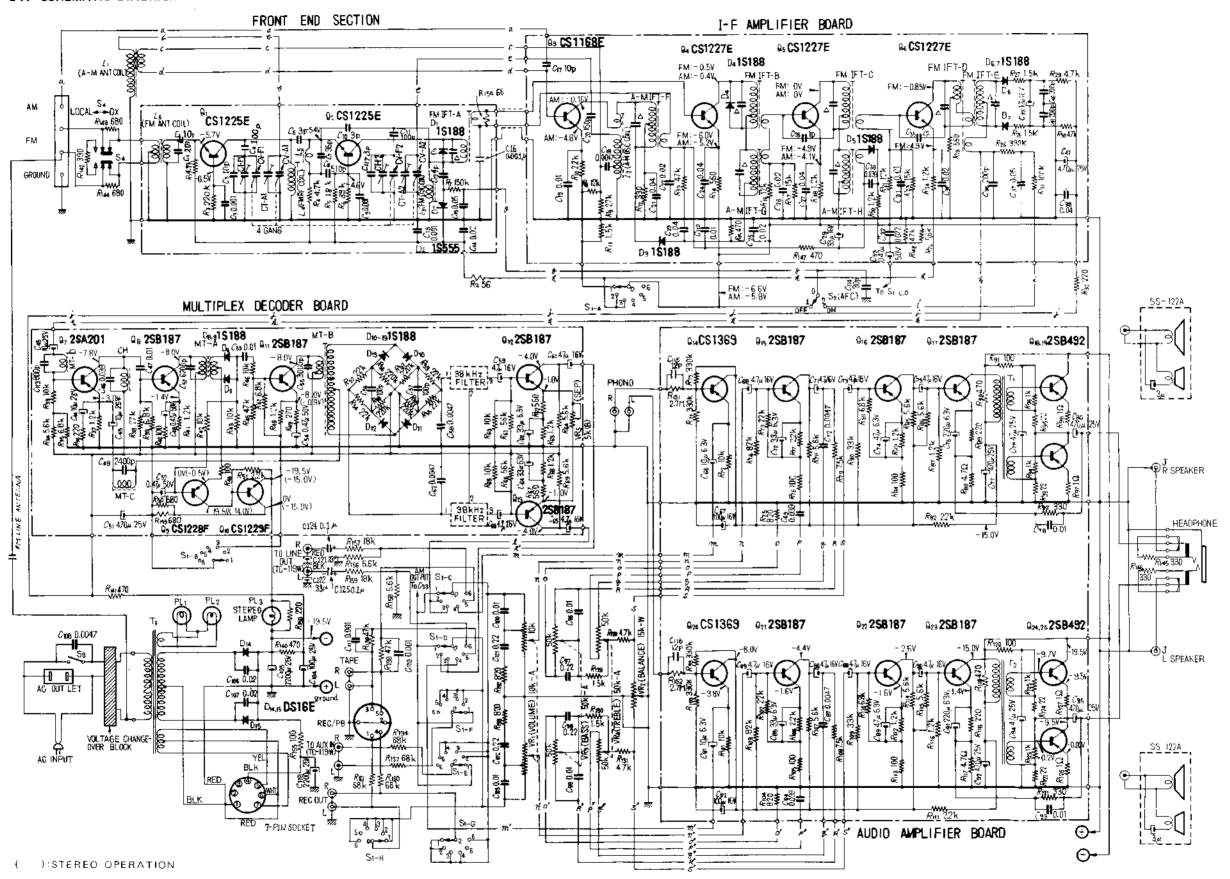
All resistance values are in ohms. $k=1\,000$, $M=1\,000\,k$

All capacitance values are in μF except as indicated with p, which means $\mu \mu F$.

All voltages represent an average value and should hold within $\pm 20\%$.

All voltages are dc measured with a VOM (DC 20 k ohms/V) at no signal.

5-7. SCHEMATIC DIAGRAM

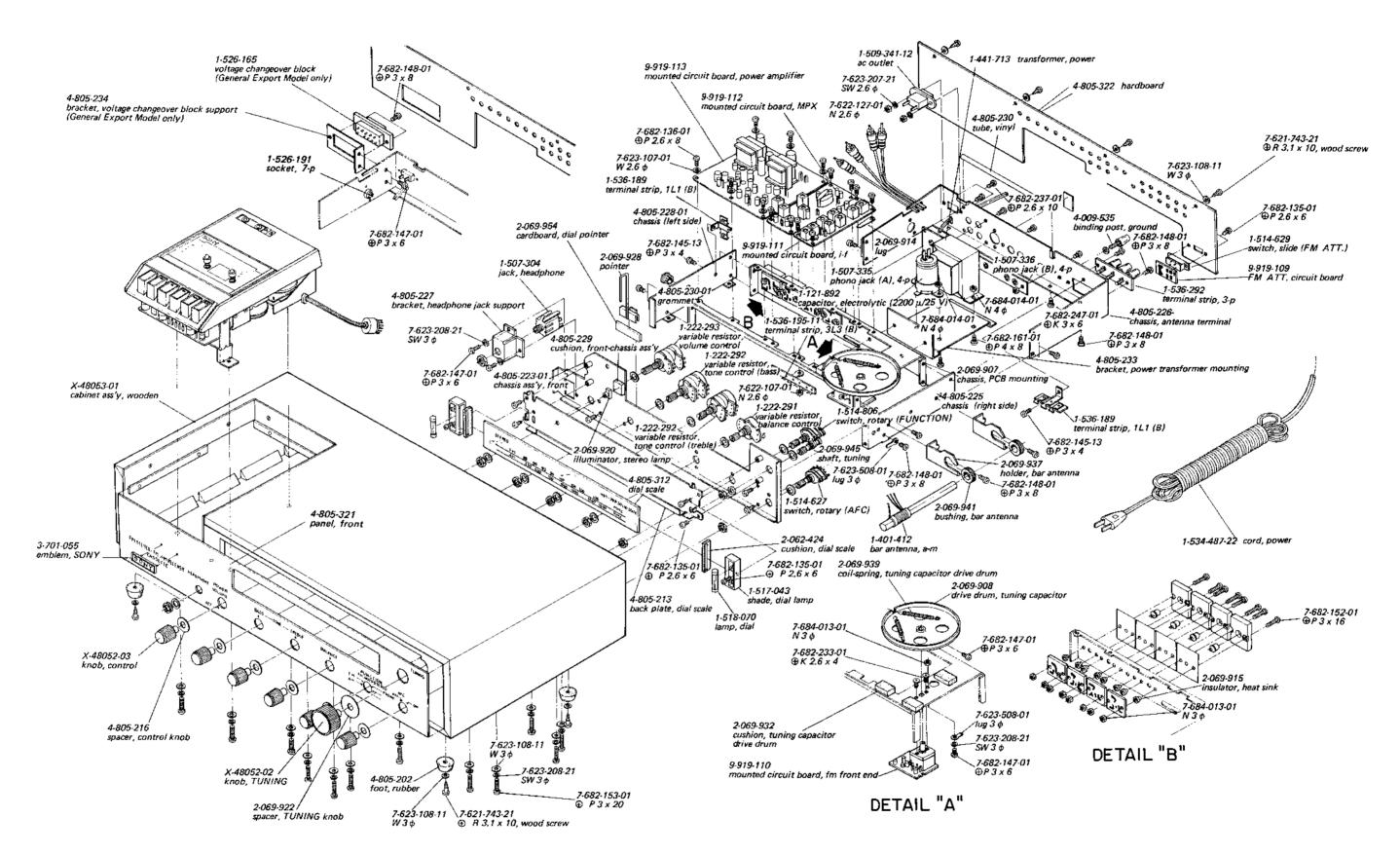


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SECTION 6 EXPLODED VIEW



SECTION 7 ELECTRICAL PARTS LIST

Ref. No.	Part No. Description	Ref. No. Part No. Description	Ref. No.	Part No. Description	Ref. No. Part No. Description
		IFT-A 1-403-558 IFT, 10.7 MHz	C23	1-101-925 0.04 $\pm \frac{80}{20}\%$ 25V, ceramic	C80(C95) 1-121-733 470 $\pm \frac{100}{10}\%$ 25V, electrolytic
	Mounted Circuit Boards	IFT-B 1-403-559 IFT, 10.7 MHz	C24	1-101-925 0.04 ±80% 25V, ceramic	C96(C99) 1-105-673-12 0.01 ±10% 50V, mylar
	9-919-110 fm front-end circuit board	IFT-C 1-403-559 IFT, 10.7 MHz	C25	1-101-924 0.02 $\pm \frac{80}{20}\%$ 25V, ceramic	C97(C98) 1-105-689-12 0.22 ±10% 50V, mylar
	9-919-111 i-f circuit board	IFT-D 1-403-560 IFT, 10.7 MHz	C26	1-101-924 0.02 $\pm \frac{50}{20}\%$ 25V, ceramic	C100(C103) 1-105-673-12 0.01 ±10% 50V, mylar
	9-919-112 MPX circuit board	IFT-E 1-403-561 IFT, 10.7 MHz	C27	1-101-925 0.04 $\pm \frac{80}{20}\%$ 25V, ceramic	C101(C102) 1-105-689-12 0.22 ±10% 50V, mylar
	9-919-113 audio amplifier circuit board	IFT-F 1-403-170 IFT, 455 kHz	C28	1-101-951 1 p ±0.5 pF 50V, ceramic	C104 1-121-377 100 $\pm ^{150}_{10}\%$ 25V, electrolytic
	, , , , , , , , , , , , , , , , , , ,	IFT-G 1-403-169 IFT, 455 kHz	C29	1-121-485 33 ±100% 16V, electrolytic	C105 1-121-892 2,200 $\pm \frac{100}{10}\%$ 25V, electrolytic
		IFT-H 1-403-171 IFT, 455 kHz	C30	1-105-680-12 0.039 ±10% 50V, mylar	C106(C107) 1-101-073 0.02 $\pm \frac{80}{20}\%$ 50V, ceramic
	Semiconductors	Í	C31	1-101-924 0.02 $\pm \frac{80}{20}\%$ 25V, ceramic	C108 1-102-192 0.0047 ±10% 1,400V, ceramic
Dİ	diode 1S188	L1 1-401-412 coil, a-m antenna	C32	1-105-677-12 0.022 ±10% 50V, mylar	C110(C111) 1-105-661-12 0.001 ±10% 50V, mylar
D2	diode 1S555	L2 1-405-416 coil, a-m osc	C33	1-121-434 0.47 $\pm \frac{150}{16}\%$ 50V, electrolytic	C112 1-105-673-12 0.01 ±10% 50V, mylar
D3	diode 1S188	L3 1-405-415 coil, fm osc	C34	1-101-924 0.02 $\pm \frac{80}{20}\%$ 25V, ceramic	C113 1-103-823 820 p ±5% 50V, styro1
D4	diode 1\$188	L4 1-425-588 coil, fm rf	C35	1-101-952 2 p ± 0.5 pF 50V, ceramic	C114 1-101-871 30 p ±5% 50V, ceramic
D5	diode 1S188	L5 1-409-182 coil, i-f trap	C36	1-101-030 200 p ±5% 50V, ceramic	C115(C116) 1-101-961 12 p ±5% 50V, cerarnic
D6	diode 1S188	L6 1-401-411 coil, fm antenna	C37	1-101-926 0.05 $\pm \frac{80}{20}\%$ 25V, ceramic	C117 1-101-953 3p ±0.5 pF 50V, ceramic
D7	diode IS188		C38	1-101-925 0.04 $\pm \frac{80}{20}\%$ 25V, ceramic	C118 1-119-159 2,200 25V, electrolytic
D8	diode 1S188	MT-A 1-425-590 MPX coil, 19 kHz	C39	$\frac{1}{1}$ 121-464 4.7 $\pm \frac{1}{10}$ % 25V, electrolytic	C121 1-121-402 33 $\pm {}^{100}$ % 10V, electrolytic
D9	diode 15188	MT-B 1-425-589 MPX coil, 38 kHz	C40	1-101-030 200 p ±5% 50V, ceramic	C122 1-121-402 33 $\pm \frac{100}{10\%}$ 10V, electrolytic
D10	diode 1S188	MT-C 1-409-183 MPX coil, 19 kHz	C41	1-101-030 200 p ±5% 50V, ceramic	C124 1-127-019 0.1 ±20% 10V, electrolytic
D11	diode 1S188	MT-D 1-425-591 MPX coil, 67 kHz	C42	1-121-425 470 $\pm \frac{100}{100}$ % 10V, electrolytic	(aluminum)
D12	diode 1S188		C43	1-121-471 10 $\pm \frac{100}{10}\%$ 16V, electrolytic	C125 1-127-019 0.1 ±20% 10V, electrolytic
D13	diode 1S188	T1 1-425-146 transformer, input	C44	1-121-471 10 $\pm \frac{100}{100}\%$ 16V, electrolytic	(aluminum)
D14	diode DS16E	T2 1-425-146 transformer, input	C45	1-121-471 10 $\pm \frac{10\%}{10\%}$ 16V, electrolytic	CV 1-151-203 capacitor, tuning
D15	diode D\$16E	T3 1-441-713 transformer, power	C46	$1-105-680-12$ 0.039 $\pm 10\%$ 50V, mylar	CV 1-151 255 capacitos, taning
		11,7,75	C47	1-105-673-12 0.01 ±10% 50V, mylar	Resistors
Q1	transistor CS1225E		C48	1-121-434 0.47 $\pm {}^{150}_{10}\%$ 50V, electrolytic	
Q2	transistor CS1225E		C49	1-103-834 2,400 p ±5% 50V, styrol	All resistance values are in ohms, ±5%, ¼ watts and carbon type unless otherwise indicated.
Q3	transistor CS1168E		C50	1-103-844 6,200 p ±5% 50V, styrol	R1 1-244-689 4.7 k
Q4	transistor CS1227E	Capacitors	C51	1-121-425 470 $\pm {}^{100}\%$ 10V, electrolytic	R2 1-244-643 56
Q5	transistor CS1227E	All capacitance values are in µF except as	C52	1-121-434 0.47 ± 10% 50V, electrolytic	R3 1-244-729 220 k
Q6	transistor CS1227E	indicated with p, which means $\mu\mu$ F.	C53	1-105-673-12 0.01 ±10% 50V, mylar	R4 1-244-689 4.7 k
Q7	transistor 2SA201A	C1 1-101-864 20 p ±5% 50V, ceramic	C54	1-121-434 0.47 $\pm ^{150}_{10}\%$ 50V, electrolytic	R5 1-244-703 18 k
Q8	transistor 2SB187A	C2 1-101-959 10 p ±5% 50V, ceramic	C55	1-103-836 3,000 p ±5% 50V, styrol	R6 1-244-711 39 k
Q9	transistor CS1228	C3 1-101-918 0.001 $\pm_{20}^{80}\%$ 25V, ceramic	C56	1-101-896 100 p ±5% 50V, ceramic	R7 1-244-725 150k
Q10	transistor CS1229	C4 1-101-896 100 p ±5% 50V, ceramic	C57	1-101-896 100 p ±5% 50V, ceramic	R8 1-244-699 12 k
Q11	transistor 2SB187A	C5 1-101-959 10 p ±5% 50V, ceramic	C58(C62)	1-105-669-12 0.0047 ±10% 50V, mylar	R9 1-244-707 27 k
Q12	transistor 2SB187A	C6 1-101-953 3 p ±0.5 pF 50V, ceramic	C59(C63)	1-121-464 4.7 $\pm \frac{150}{10}\%$ 25V, electrolytic	R10 1-244-681 2.2 k
Q13	transistor 2SB187A	C7 1-101-871 30 p ±5% 50V, ceramic	C60(C64)	1-121-483 33 $\pm \frac{100}{10}\%$ 10V, electrolytic	R11 1-244-677 1.5 k
Q14	transistor CS1369D(C)	C8 1-101-059 510 p ±5% 50V, ceramic	C61(C65)	1-121-464 4.7 $\pm {}^{150}_{10}\%$ 25V, electrolytic	R12 1-244-661 330
Q15	transistor 2SB187A	C9 1-101-918 0.001 $\pm \frac{80}{20}\%$ 25V, ceramic	C66(C81)	1-121-471 10 $\pm \frac{100}{10}\%$ 16V, electrolytic	R13 1-244-713 47 k
Q16	transistor 2SB187A	C10 1-101-953 3 p ±0.5 pF 50V, ceramic	C67(C82)	1-121-377 100 $\pm {}^{150}_{10}\%$ 25V, electrolytic	R14 1-244-667 560
Q17	transistor 2SB187A	C11 1-101-896 100 p ±5% 50V, ceramic	C68(C83)	1-121-464 4.7 $\pm \frac{150}{10}\%$ 25V, electrolytic	R15 1-244-665 470
Q18	transistor 2SB492	C12 1-101-954 4p ±0.5 pF 50V, ceramic	C69 (C84)	1-105-680-12 0.039 ±10% 50V, mylar	R16 1-244-699 12 k
Q19	transistor 2\$B492	C13 1-101-918 0.001 $\pm \frac{80}{20}\%$ 25V, ceramic	C70(C85)	1-121-483 33 ±10% 10V, electrolytic	R17 1-244-701 15 k
Q20	transistor CS1369D(C)	C14 1-101-924 0.02 $\pm \frac{80}{20}\%$ 25V, ceramic	C71(C86)	1-121-464 4.7 $\pm ^{150}_{10}\%$ 25V, electrolytic	R18 1-244-675 1.2 k
Q21	transistor 2SB187A	C15 1-101-926 0.05 $\pm \frac{80}{20}\%$ 25V, ceramic	C72(C87)	1-105-669-12 0.0047 ±10% 50V, mylar	R20 1-244-675 1,2 k
Q22	transistor 2SB187A	C16 1-101-918 0.001 $\pm_{20}^{80}\%$ 25V, ceramic	C73(C88)	1-121-464 4.7 $\pm ^{150}$ % 25V, electrolytic	R21 1-244-699 12 k
Q23	transistor 2SB187A	C17 1-101-959 10 p ±5% 50V, ceramic	C74(C89)	1-121-487 47 $\pm \frac{100}{10}\%$ 6.3V, electrolytic	R22 1-244-691 5.6 k
Q24	transistor 2SB492	C18 1-105-669-12 0.0047 ±10% 50V, mylar	C75(C90)	1-121-464 4.7 ±150% 25V, electrolytic	R23 1-244-701 15 k
Q25	transistor 2SB492	C19 1-105-673-12 0.01 ±10% 50V, mylar	C76(C91)	1-121-420 220 $\pm \frac{100}{10}\%$ 10V, electrolytic	R24 1-244-675 1.2 k
		C20 1-103-805 150 p ±5% 50V, styroi	C77 (C92)	1-121-733 470 $\pm \frac{100}{10}\%$ 25V, electrolytic	R25 1-244-667 560
	Transformers, Coils and Inductors	C21 1-101-925 0.04 $\pm \frac{80}{20}\%$ 25V, ceramic	C78(C93)	1-105-673-12 0.01 ±10% 50V, mylar	R26 1-244-733 330 k
СН	1-407-416 coil, choke	C22 1-101-924 0.02 $\pm \frac{90}{20}\%$ 25V, ceramic	C79(C94)	1-121-375 47 $\pm ^{150}_{10}\%$ 25V, electrolytic	R27 1-244-677 1.5 k
		1			1

HST-399 HST-399 TC-119W2 TC-119W2

Ref. No.

Part No.

1-507-304

1-507-335

1-507-336

1-509-029

1-509-341

1-517-043

1-518-070

Description

phono jack (A), 4-P (SPEAKER)

phono jack (B), 4-P (PHONO, TAPE)

jack, headphone

REC/PB connector

socket, dial lamp

AC outlet

lamp, dial

Miscellaneous 1-506-316-11 phono plug

1-506-316-21 phono plug

Ref. No.

Part No.

1-518-106

1-526-165

1-526-191

1-534-666

1-536-189

1-536-292

9-919-109

Description

voltage changeover block

lamp, stereo

socket, 7-P

cord, fm antenna

terminal strip, 3-P

terminal strip, 1L1 (B)

printed circuit board, fm ATT

1-534-487-22 cord, power

Ref. No.	Part No.		Description	Ref. No.	Part No.	4	Description
R28	1-244-677	1.5 k		R86(R115)	1-244-691	5.6 k	
R29	1-244-689	4.7 k			1-244-675	1,2 k	
R30	1-244-689	4.7 k			1-244-617	4.7	
R31	1-244-721	100 k		,	1-244-657	220	
R32	1-244-657	220		1	1-244-665	470	
R33	1-244-697	10 k		1	1-244-649	100	
R34	1-244-691	5.6 k		R92(R121)		330	
R35	1-244-693	6,8 k		1	1-244-633	22	
R36	1-244-657	220		R94(R123)	1-244-673	1 k	
R37	1-244-675	1.2 k		R95(R124)	1-244-633	22	
R38	1-244-707	27 k		R96(R125)	1-244-673	1 k	
R39	1-244-693	6.8 k		R97(R126)	1-244-601	1	
R40	1-244-649	100		R98(R127)	1-244-601	1	
R41	1-244-675	1.2 k		R128(R131)	1-244-689	4.7 k	
R42	1-244-697	10 k		R129(R130)	1-244-677	1,5 k	
R43	1-244-697	10 k		R132(R133)		820	
R44	1-244-649	100		R134(R137)		68 k	
R45 R46	1-244-713	47 k		R138(R139)	1-244-713	47 k	
R47	1-244-697 1-244-693	10 k		R140	1-244-665	470	
R48	1-244-675	6.8 k 1.2 k		R141	1-244-665	470	
R49	1-244-659	270		R142	1-244-663	390	
R50	1-202-569	680	±10% ½W, composition	R143	1-244-669	680	
R51	1-244-681	2.2 k	210% /2#, composition	R144	1-244-669	680	
R52	1-244-705	22 k		R145(R146)			±10% ½W, composition
R53	1-244-705	22 k		R147 R148	1-244-665	470	
R54	1-244-705	22 k		R149	1-244-713	47 k	410 <i>m</i> 1/35
R55	1-244-705	22 k		R150	1-202-569 1-202-557		±10% ½W, composition
RS6	1-244-729	220 k		R151 (R152)			±10% ½W, composition ±10% ½W, composition
R57	1-244-729	220 k		1	1-244-645	68	#10% 72W, Composition
R58	1-244-729	220 k			1-244-649	100	
R59 .	1-244-729	220 k		i	1-244-691	5.6 k	
R60(R65)	1-244-697	10 k		R157	1-244-713	47 k	
R61(R66)	1-244-715	56 k		R158	1-244-691	5.6 k	
R62(R67)	1-244-667	560		R159	1-244-713	47 k	
R63(R68)	1-244-675	1.2 k		R160	1-244-717	68 k	
R64(R69)	1-244-691	5.6 k		ļ	1-244-717	68 k	
R70(R99)	1-244-733	330 k		VR1	1-222-293	10 k va	riable (volume control)
R71(R100)		330 k		VR2	1-222-291		riable (balance control)
R72 (R101)		10 k		VR3	1-222-292		riable (tone control, bass)
R73 (R102)		22 k		VR4	1-222-292	50k var	riable (tone control, treble)
R74(R103)		82 k		VR5	1-222-709		mi-fixed
R75 (R104)		820					
R76(R105)		100			Switch	A C	
R77 (R106)		2.2 k		\$1	1-514-806		rotary (FUNCTION)
R78(R107)		5.6 k			1-514-627		rotary (AFC)
R79 (R108) R80 (R109)		7.5 k		. .	1-514-629		slide (FM ATT)
R81(R110)		33 k				Jtvii, 3	(4 412 62.4 1)
R82(R111)		6.8 k 2.2 k	}				
R83(R112)		2.2 k 1.2 k			Filter		
R84(R113)		100			1-231-098	LPF, 38	5 kHz
R85 (R114)		5.6 k	}				

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STEREO CASSETTE RECORDER (TC-119W2)



Note: TC-119W2 is a stereo cussette deck installed in HST-399.





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SECTION 1 TECHNICAL DESCRIPTION

1-1. TECHNICAL SPECIFICATIONS

Technical specifications for the TC-119W2 stereo cassette tape deck are listed in Table 1.

Table 1. Technical Specifications

Tape speed : 4.8 cm/sec

(1 % inch/sec)

Frequency response : 50 Hz to 10 kHz

(-15 dB)

Recording bias frequency : 85 kHz

Flutter and wow : 0.5 %

1-2. CIRCUIT ANALYSIS

The following text describes the function or operation of all stages and controls. The text sequence follows signal paths. Stages are listed by transistor reference designation at the left margin; major components are also listed in a similar manner. Refer to the block diagram on page 47 and the schematic diagram on page 59.

Since the REC/PB amplifier section contains two identical amplifier chains, only the left channel will be described. The right channel is identical except for reference symbol numbers.

Stage/Control	Function

Preamplifier This stage has two functions.

Q101, Q102 It works as a flat amplifier for playback, but has an NAB equalizing characteristic for recording.

REC/PB change-over switch S1 In the record mode, input signal is fed to the base of Q101 through S1-2L, and is then amplified to the level required for driving the record amplifier by the three-stage direct-coupled preamplifier. Flat response and operation are obtained by the negative feedback loop consisting of R115, C108, R114, R104 and the impedance between collector and emitter of Q104.

In the playback mode, the voltage induced in the playback head is applied to the preamplifier.

Playback equalization is achieved by means of a negative feedback loop containing C107, R113, R112

and R111.

Stage/Control Function

The signal is now delivered to LINE OUT jack J103, through R117 and R301 (balance adj.). R301 is set to obtain the same output voltage at each LINE OUT jack. Input signals appear at J103 even in the recording and is available for monitoring.

AGC circuit Q104, Q105 Q301

D102

Q301

R303

The TC-119W2's automatic gain control circuit is essentially a compressor to prevent overmodulation in the recording system. Although age restricts the volume range to some extent, it aids in flattening out excessive program peaks.

Age operation is achieved by changing the value of negative feedback voltage in the preamplifier by varying the impedance between collector and emitter of Q104.

The agc circuit works as follows:

In the record mode, output signal from the preamplifier is directly fed to emitter follower Q105. Since the emitter follower has a high input impedance, it works as a buffer amplifier and has no effect upon the preamplifier's operation.

The signal is rectified by D102 and then supplied to the base of Q301 through S1-5R.

Q301 is a dc amplifier which amplifies the dc component of the rectified signal (which is proportional to the input signal level) to the level required to drive Q104. It responds to signal peaks also, since the agc circuit is required to control sudden variations in the program.

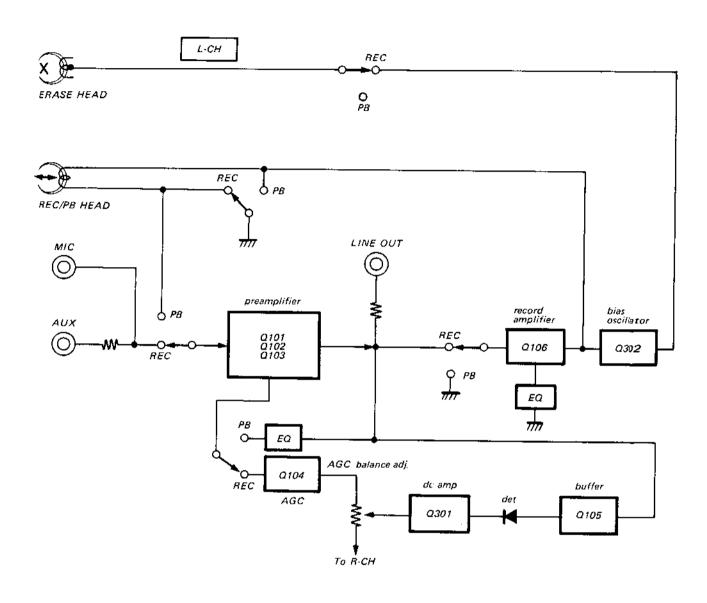
D101, Q104,

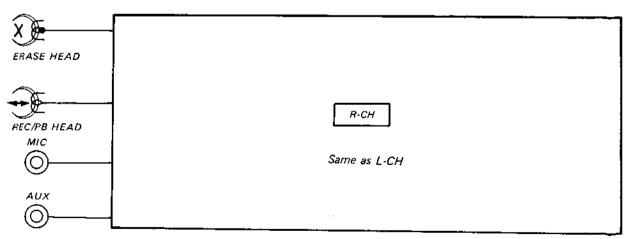
The dc output of Q301 is applied to the base of control transistor Q104 through R303 (agc balance adj.) and D101. The base current of Q104 determines the impedance between the collector and emitter of Q104, which in turn determines



Stage/Control	Function	Stage/Control	Function
	the amount of negative feedback and hence the preamplifier gain. D101 is employed to extend the age response. R303 balances the age response between "L" and "R" channels.	Bias oscillator Q302 T301	This oscillator supplies bias current to the record head through T301 and coupling capacitor C118. The circuit is a Hartley oscillator with the feedback applied to the base from the collector circuit.
Record amplifier Q106	Amplifies the preamplifier output signal to the level required to drive the record head. In the emitter circuit of Q106. L101 and C114 (in series resonance) compensate for the high-frequency	Erase head	C303, C314, and the inductance of the erase head form a resonant circuit at the bias frequency to make the bias current flow in the erase head more efficiently.
	(11 kHz) loss that occurs in the record head and produce a flat frequency responseduring playback.	Power Supply CD-2	Diode D303 (a double diode) forms a full-wave rectifier to supply do operating voltage to the drive motor. Accurrent for this rectifier
Bias current trap L102, C116	Prevents bias current leak in the record amplifier. This trap is a parallel-tuned circuit.		is supplied through connector CNP1 from the power transformer in the receiver section.
Bias current adj. C117 C118 C119	These coupling capacitors should be selected to obtain optimum bias current in the record head.	Note	The well filtered and stabilized dc volt- age for amplifiers is supplied from receiver section through connector CNP1.

1-3. BLOOK DIAGRAM

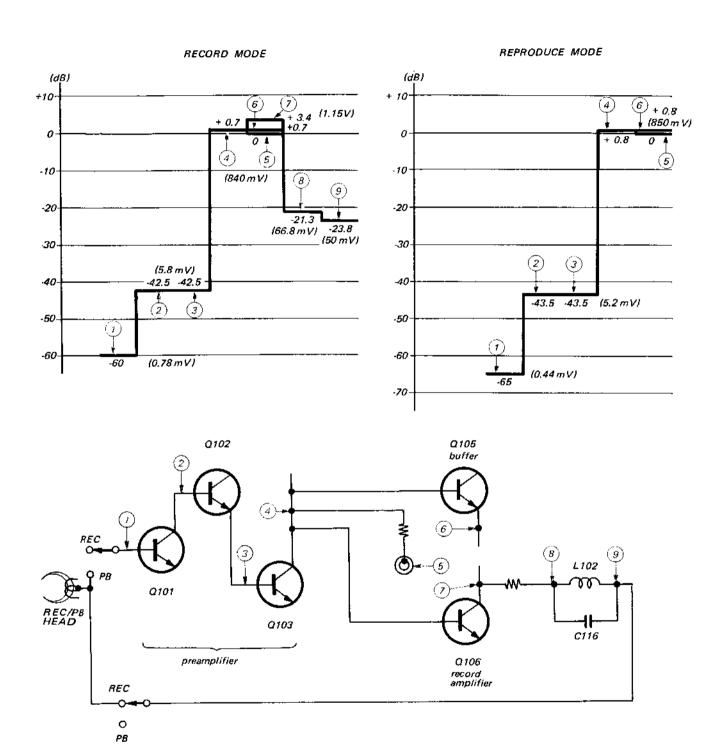






1-4. LEVEL DIAGRAM

Note: Signal voltages are measured with ac VTVM and expressed in dB referred to 0.775V, 1 kHz.



SECTION 2 DISASSEMBLY AND REPLACEMENT PROCEDURES

WARNING

Unplug the ac power cord before starting any disassembly or replacement procedures.

2-1. TOOLS REQUIRED

The tools required to perform the following disassembly and replacement procedures on the TC-119W2 are listed below.

Screwdrive, Philips-head Pliers, long-nose

2-2. HARDWARE IDENTIFICATION GUIDE

The following chart will help you to decipher the hardware codes given in this service manual.

 Hardware Nomenclature -PS - Pan Head Screw K - Flat Countersunk Head Screw ... () RK - Oval Countersunk Head Screw .. () R - Round Head Screw F - Flat Fillister Head Screw SC - Set Screw..... ⊜ E - Retaining Ring (E Washer)...... W - Washer SW - Spring Washer LW - Lock Washer N - Nut - Example -— Type of Slot ⊕ P 3x10 Length in mm (L) -Diameter in mm (D) 1... - Type of Head

Note: All screws in the TC-119W2 are manufactured to the specifications of the International Organization for Standardization (ISO). This means that the new and old screws are not interchangeable because ISO screws have a different number of threads per mm compared to the old ones. The ISO screws have an identification mark on their heads as shown in Fig. 2-1.

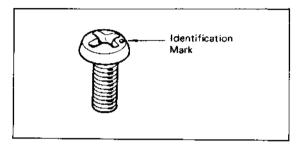


Fig. 2-1 ISO screw

2-3. CASSETTE DECK REMOVAL

- 1. Remove the six screws at the rear hardboard, two of them ($\oplus P 2.6 \times 6$) secure the ATT switch, and the four others (wood screw $\oplus R 3.1 \times 10$) secure the hardboard to the wooden case as shown in Fig. 2-2.
- Remove the three screws (@P3x20) securing the cassette deck from the bottom as shown in Fig. 2-2. This frees the cassette deck.
- 3. Disconnect 7 pin plug and two-pairs of phono plug connecting between the cassette leck and the receiver unit.

2-4. TOP COVER REMOVAL

1. Remove the two screws (#PS 3x6, #P 2.6c6) from the bottom of the chassis. See Fig. 1-3.



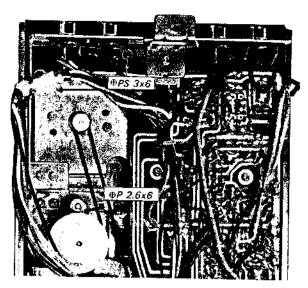


Fig. 2-3 Top cover removal (1)

- 2. Remove the two nuts securing the microphone jack to the top cover, and the two screws (#P 2.6x4, #P 2.6x8) securing the top cover to the chassis. See Fig. 2-4.
- 3. Lift the top cover straight up.

2-5. PRINTED-CIRCUIT BOARD REMOVAL

- 1. Remove the recorder from the wooden case as described in Procedure 2-3.
- Remove the three screws (⊕ PS 3x6, ⊕ P 2.6x4) securing the brackets to the chassis as shown in Fig. 2-5 and Fig. 2-6.

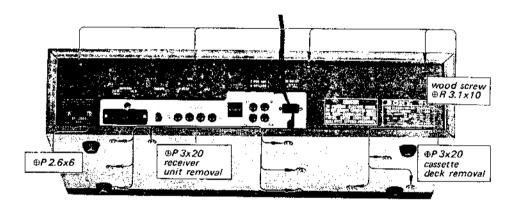


Fig. 2-2 Cassette deck removal

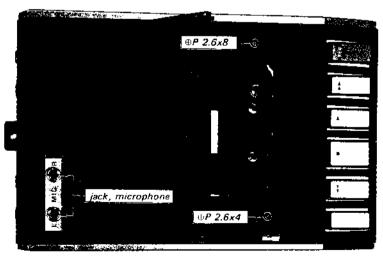


Fig. 2-4 Top cover removal (2)

- 3. Remove the four screws (#P 2.6x4) securing the printed circuit board to the chassis as shown in Fig. 2-7.
- 4. Now the printed circuit board can be removed for servicing.

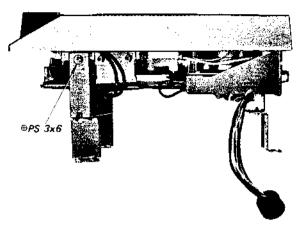


Fig. 2-5 Chassis bracket removal (1)

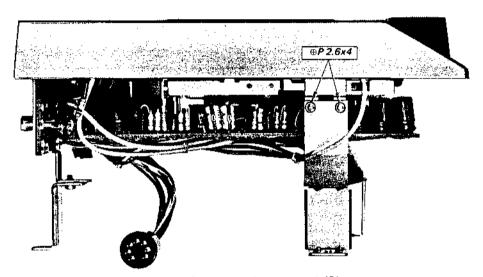


Fig. 2-6 Chassis bracket removal (2)

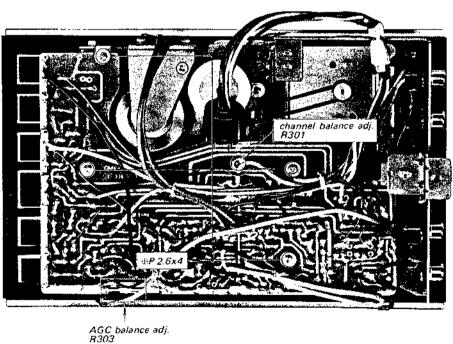


Fig. 2-7 PCB removal



SECTION 3 MECHANICAL ADJUSTMENT PROCEDURES

Note: The mechanical assembly is shipped from the factory with all adjustments set for correct performance. It should be unnecessary to change any adjustment before putting the equipment into service, unless shipping damage has occurred. In the course of normal service, or in the event of component failure and replacement of parts, some readjustment may be necessary.

3-1. TOOLS REQUIRED

The following tools are required to perform mechanical adjustment procedures on the TC-119W2.

Screwdriver, Phillips-head Screwdriver, 3 mm blade Pliers, long-nose Contact cement

3-2. PUSH-BUTTON HEIGHT ADJUSTMENT

- Check that the top surfaces of all push buttons line up in the STOP mode.
- 2. Push-button height can be adjusted by bending the tab on the push-button mechanism with a screwdriver. See Fig. 3-1.

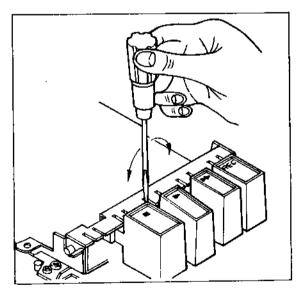


Fig. 3-1 Push-button height adjustment

3-3. CLEARANCE ADJUSTMENT BETWEEN PULLEY "C" AND REEL TABLES

- With the equipment in the STOP mode, make sure that pulley "C" does not touch the reel tables. At the same time the clearance (b) between pulley "C" and the take-up reel table should be larger than the clearance (a) between pulley "C" and the supply-reel table as shown in Fig. 3-2.
- 2. The clearance can be changed by bending the Rewind/Fast Forward spring in the back of the chassis with pliers as shown in Fig. 3-3.

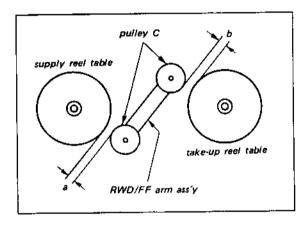


Fig. 3-2 Clearance between pulley "C" and reel tables

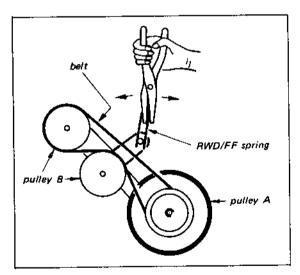


Fig. 3-3 Spring adjustment for pulley "C" clearance



3-4. PULLEY "C" HEIGHT ADJUSTMENT

- In the Fast Forward or Rewind mode, the reel tables should run in the center of puliey "C" as shown in Fig. 3-4.
- 2. To adjust the pulley height, bend the tab of the Fast Forward/Rewind spring to obtain proper operation as shown in Fig. 3-5.

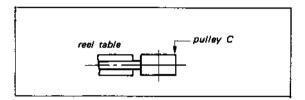


Fig. 3-4 Pulley "C" height adjustment

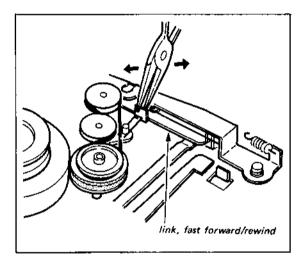


Fig. 3-5 Tab adjustment for pulley "C" height

3-5. FLYWHEEL END-PLAY ADJUSTMENT

- 1. In the STOP mode, check the end play of the flywheel. There should be 0.2 mm to 0.5 mm end play between the flywheel and its housing as shown in Fig. 3-6.
- End play can be changed by turning the screw marked ▲ in Fig. 3-6.
- 3. After completing the adjustment, apply a drop of contact cement to the screw.

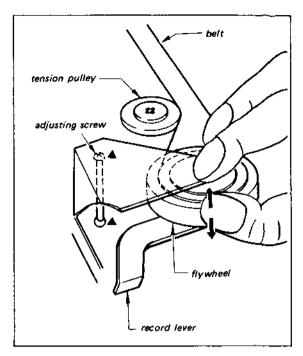


Fig. 3-6 Flywheel end-play adjustment

3-6. TAKE-UP TENSION CHECKOUT

Serious malfunctions such as tape sticking in the pinch roller will result if the take-up tension is not sufficient.

Take-up tension is checked by measuring the take-up reel table's torque in the playback mode with the special torque driver (or equivalent) as follows:

Equipment Required

* Torque driver (See Fig. 3-7.) or equivalent.

Procedure

- 1. Press the EJECT button to open the lid.
- 2. Turn the power switch "ON" and press the playback button to allow the counterclockwise motion of the take-up reel table.
- Release the torque driver clamp first, and then
 place it slowly onto the take-up-reel table's
 shaft as shown in Fig. 3-7.
 Be certain that the torque driver clutches the



4. Observe the readings on the scale. It should be between 40 and 60 gram-cm as shown in Fig. 3-9.

Note: If the proper reading is not obtained, all mechanisms related to take-up motion such as the friction pulley assembly, capstan drive belt, drive-motor and take-up-reel table assembly, should be checked and replaced.

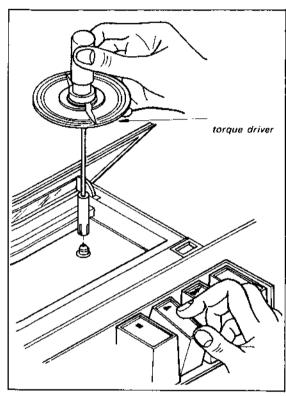


Fig. 3-7 Tack-up tension checkout

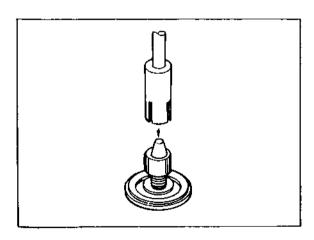


Fig. 3-8 Torque driver installation

- (a) Friction pulley assembly replacement
 - 1. Remove the top cover as described in Procedure 2-4.
 - 2. Remove the take-up reel table drive pulley by loosening the set screw as shown in Fig. 3-10.
 - 3. Pull the defective friction pulley assembly out from the bottom and then install the replacement friction pulley assembly.
- (b) Take-up or supply reel table assembly replacement
 - Open the lid of the top cover and then pry out the cap on the shaft with a jeweler's screw driver.

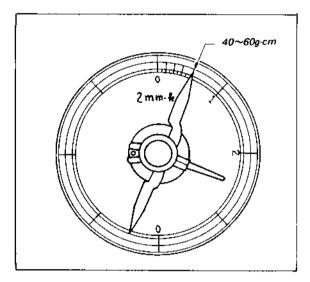


Fig. 3-9 Torque driver indication

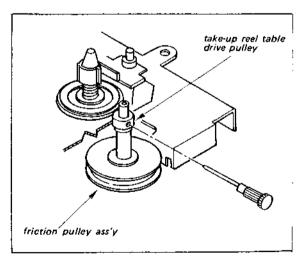


Fig. 3-10 Friction pulley removal



2. Remove the defective reel table and then install the replacement.

3-7. PINCH ROLLER PRESSURE CHECKOUT

The pinch roller is forced against the capstan by the action of pressure spring.

insufficient pressure may cause slippage on the capstan while excessive pressure throws an unnecessary load on the capstan bearing causing speed reduction.

Pinch roller pressure should be maintained within the recommended value.

Equipment Required

 Special spring scale as shown in Fig. 3-11 or equivalent.

Procedure

- 1. Press the EJECT button to open the lid.
- 2. Press the playback button.
- Check the pressure applied to the pinch roller by using a special spring scale as shown in Fig. 3-11 and 3-12.

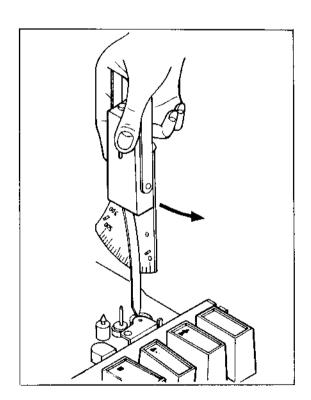


Fig. 3-11 Pinch roller pressure checkout

- 4. Take a reading only when the pinch roller is pulled backward by the spring scale and then slowly returned toward the capstan. The force required to overcome the static friction will produce an excessively high initial reading; this technique eliminates this source of error.
- 5. The readings should be between 280 and 400 grams as shown in Fig. 3-13.

Note: If the proper reading is not obtained, replace the pressure spring.

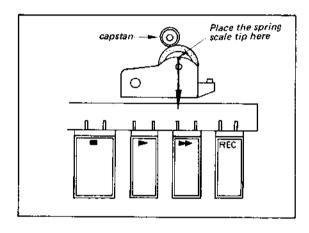


Fig. 3-12 Detail of measuring point

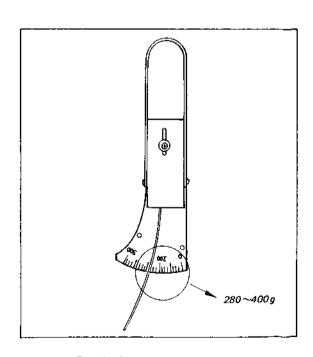


Fig. 3-13 Spring scale reading



SECTION 4 MAINTENANCE AND ADJUSTMENT

4-1. HEAD CLEANING

Most tape manufacturers lubricate their tapes to reduce head and tape wear. Unfortunately deposits of this lubricant will gradually build up on the heads. These deposits cause loss of high frequencies, therefore the heads should be cleaned before adjustment. To clean the heads, use a solvent specially manufactured for tape head cleaning.

Do not use any metallic cleaning tool or other device which will scratch the heads.

4-2. DEMAGNETIZING

The record/playback head may occasionally acquire a degree of permanent magnetization. This results in an increase in noise, distortion of any recorded signal, and a gradual erasure of high frequencies on any recorded tape which passes over it.

Head demagnetizing is easily accomplished by using the head eraser.

To demagnetize the head, proceed as follows:

Procedure

- Make certain that all controls are in their OFF position.
- Connect the head eraser to a source of ac power.
- 3. Bring the tips of the head eraser in close proximity to; but not in contact with, the record/playback head so that the tips straddle the gap in the center of the head. Run the tips up and down over the head several times,

and then slowly withdraw the head eraser. The slow withdrawal is essential to proper demagnetization.

4. Repeat Step 3 at the erase head and tape guides.

4-3. SPEED ADJUSTMENT

Note: This adjustment should be performed only if precise tape speed is required.

Test Equipment Required

- 1. SONY SPC-4 test tape or equivalent
- 2. Frequency counter
- 3. Connecting cord SONY RK-46
- Three kinds of motor pulley. See Fig. 4-2.
- 5. Screwdriver, 3 mm

Procedure

- With the equipment connected as shown in Fig. 4-1, set the counter's gate control to 1 second.
- Reproduce the test tape. Wait 10 seconds then note the counter's indication.
- The indication should be within the limit of 1,000±30 Hz. If not, replace the pulley.
- 4. Three kinds of motor pulley are available for precise speed adjustment as shown in Fig. 4-2.

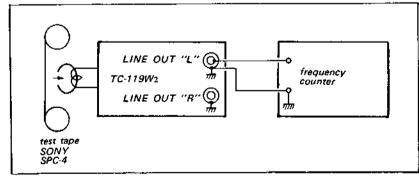


Fig. 4-1 Speed adjustment test setup

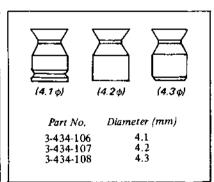


Fig. 4-2 Motor pulleys

44. RECORD/PLAYBACK HEAD AZIMUTH ADJUSTMENT

CAUTION

The test tape used in the following procedure may be partially erased. If the head is permanently magnetized, demagnetize the heads as described in Procedure 4-2 before starting this procedure.

Test Equipment Required

- 1. SONY P-4-A81 test tape
- 2. Ac VTVM
- 3. Oscilloscope
- 4. Connecting cord RK-46 2
- 5. Screwdriver 3 mm

Note: Head azimuth adjustment, bias adjustment (4-5), and channel balance adjustment (4-6) should be performed only after replacing the record/playback head.

Procedure

- 1. With the equipment connected as shown in Fig. 4-4, play the 6 kHz signal recorded on the test tape.
- Adjust the azimuth adjusting screw (See Fig. 4-3) on the record/playback head for maximum output on the VTVM, and an inphase indication on the oscilloscope as shown in Fig. 4-4.

Note:

(1) The in-phase condition may not coincide with maximum output.

- It is permissible that the in-phase condition be obtained while the output level is within 1 dB below maximum output.
- (2) If the head azimuth is far out of alignment, minor peaks may observed on both sides of maximum peak. The proper setting is higher than these peaks.

4-5. BIAS ADJUSTMENT

Note: Bias adjustment should be performed only after replacing the record/playback head and azimuth adjustment.

Test Equipment Required

- 1. Blank cassette tape
- 2. Ac VTVM
- 3. 600 Ω unbalanced attenuator
- 4. Connecting cordSONY RK-46 (2)
- 5. Aduio oscillator
- 6. Solder and soldering iron, 40 to 50W.
- 7. 600Ω resistor, 4W, $\pm 5\%$

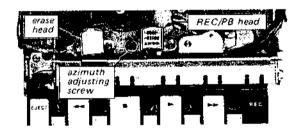


Fig. 4-3 Azimuth adjusting screw

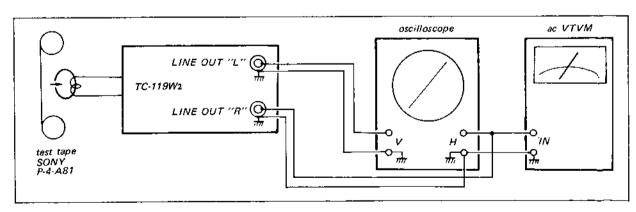


Fig. 4-4 Head azimuth and phase adjustment test setup



Procedure

1. With the equipment connected as shown in Fig. 4-4, record the signals as follows:

Level
-90 dB
-90 dB
-90 dB

- * 0 dB = 0.775 V
- Playback the recorded signals and measure the output levels of the 1,000 Hz, 150 Hz, and 6,000 Hz test tones. The 150 Hz and 6,000 Hz output levels should be within ±3 dB of the 1,000 Hz output level.
- 3. Proper frequency response will achieved by changing the bias current as follows:
 - (a) If the output at 150 and 6,000 Hz is too high, connect 27 pF capacitor C117
 (C217) instead of 22 pF capacitor C118
 (C218). See Fig. 4-6.
 - (b) If the output at 150 and 6,000 Hz is too low, connect 18 pF capacitor C119 (C219) instead of C118 (C218). See Fig. 4-6.

46. CHANNEL BALANCE AND AGC BALANCE

Note: These adjustments should be performed after replacing the record/playback head.

Test Equipment Required

- 1. Blank cassette tape
- 2. Ac VTVM
- 3. Connecting cord ... SONY RK-46 or equivalent
- 4. 600 Ω unbalanced attenuator
- 5. Audio oscillator

- 6. Screwdriver, 3 mm
- 7. 600Ω resistor, 4W, $\pm 5\%$

Channel Balance

Procedure

- With the equipment connected as shown in Fig. 4-5, record a 1,000 Hz, -60 dB signal and then play it back.
- Adjust semifixed resistor R301 (See Fig. 2-7) to obtain the same output voltage from each channel.

AGC Balance

Procedure

 With the equipment connected as shown in Fig. 4-5, record a 1,000 Hz, -50 dB signal. Play it back. Adjust semifixed resistor R303 (see Fig. 2-7) to obtain the same output voltage from each channel while recording.

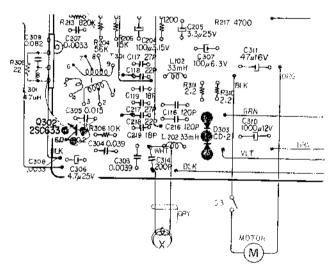


Fig. 4-6 Bias current adjustment

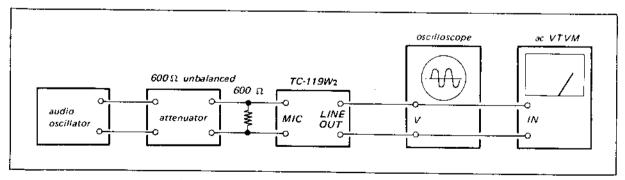
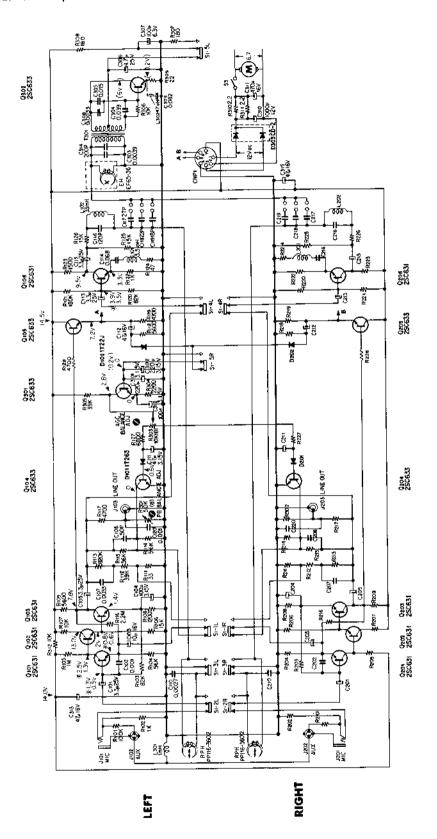


Fig. 4-5 Cassette recorder adjustment test setup



SECTIONS 5 DIAGRAMS

SCHEMATIC DIAGRAM REC/PB Amplifier Board



TC-119W2 © 1970

SONY

28.0631 633 E C B

All capacitance values are in μF except as indicated with p, which means $\mu \mu F$. All voltages represent an average value and should hold within $\pm 20\%$.

All resistance values are in Ω k = 1000, M = 1000 k

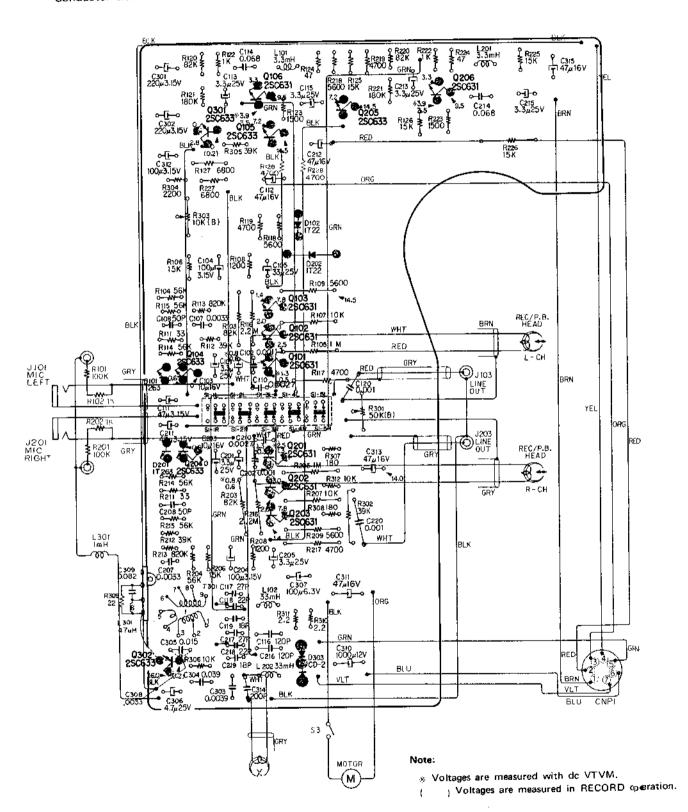
All voltages are dc measured with a VOM which has an input impedance of $20\,k\Omega/V$. No signal in. . Vulluges are measured with de VTVM

Voltages are measured in RECORD operation.



MOUNTING DIAGRAM REC/PB Amplifier Board

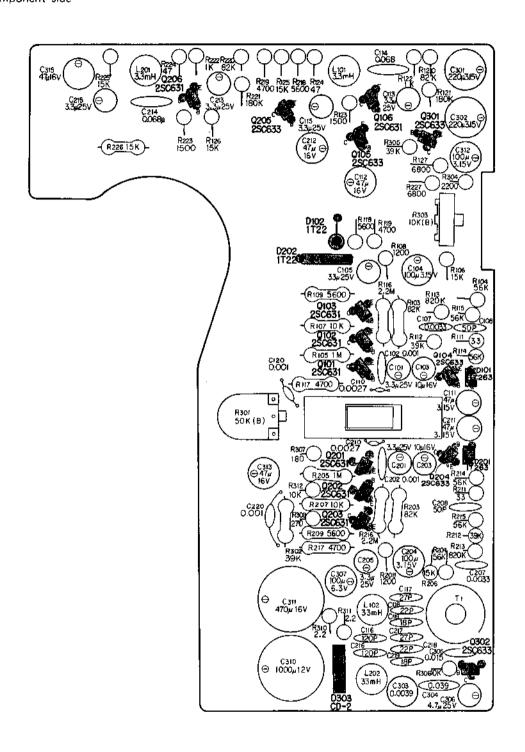
- Conductor side -





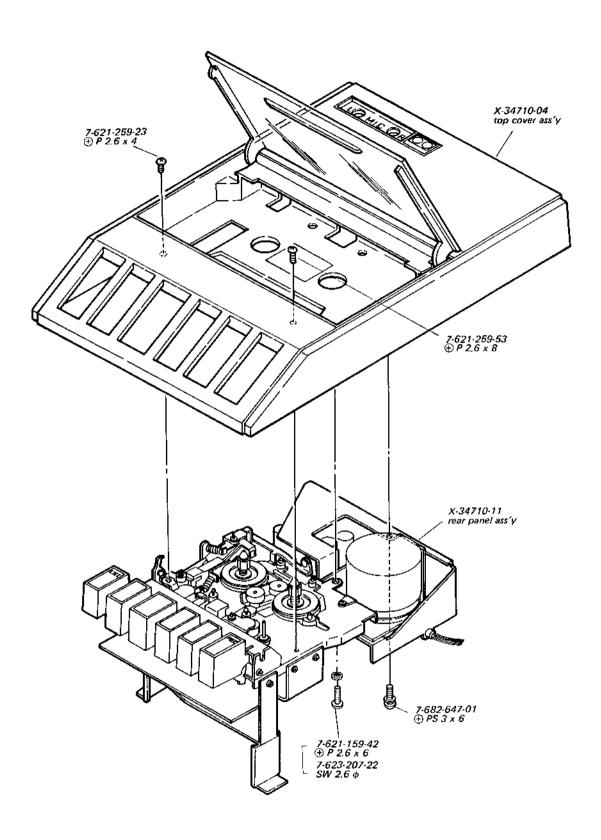
MOUNTING DIAGRAM REC/PB Amplifier Board

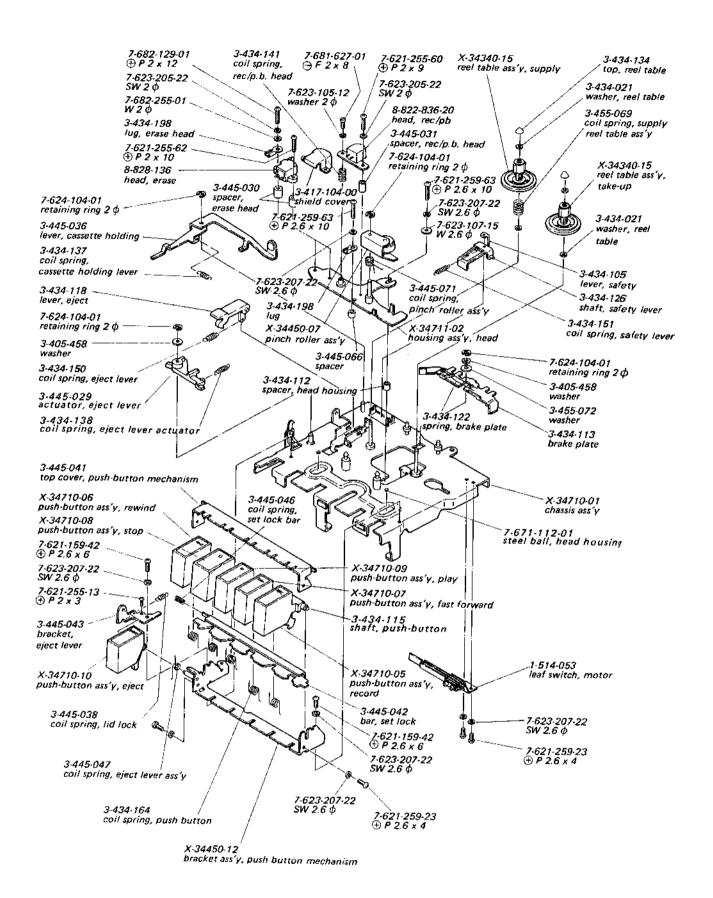
- Component side -

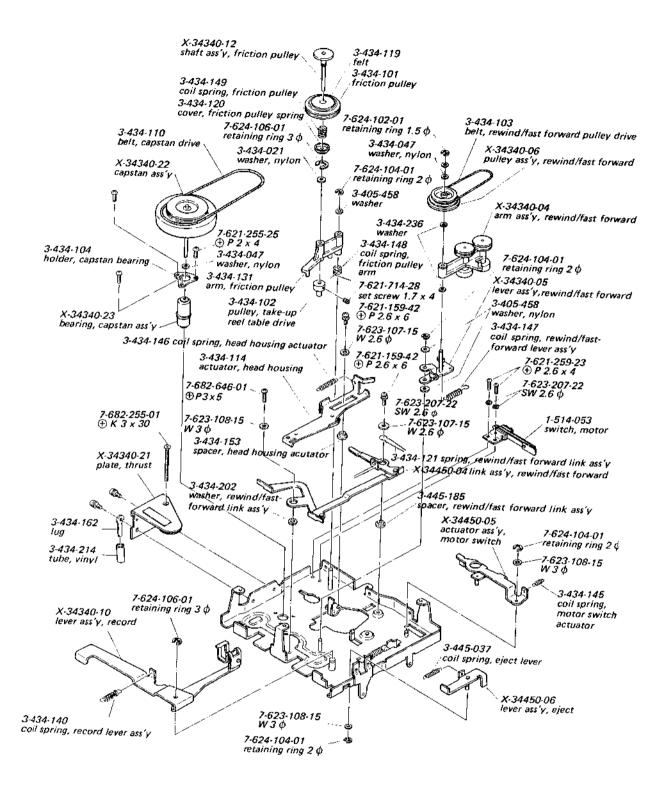




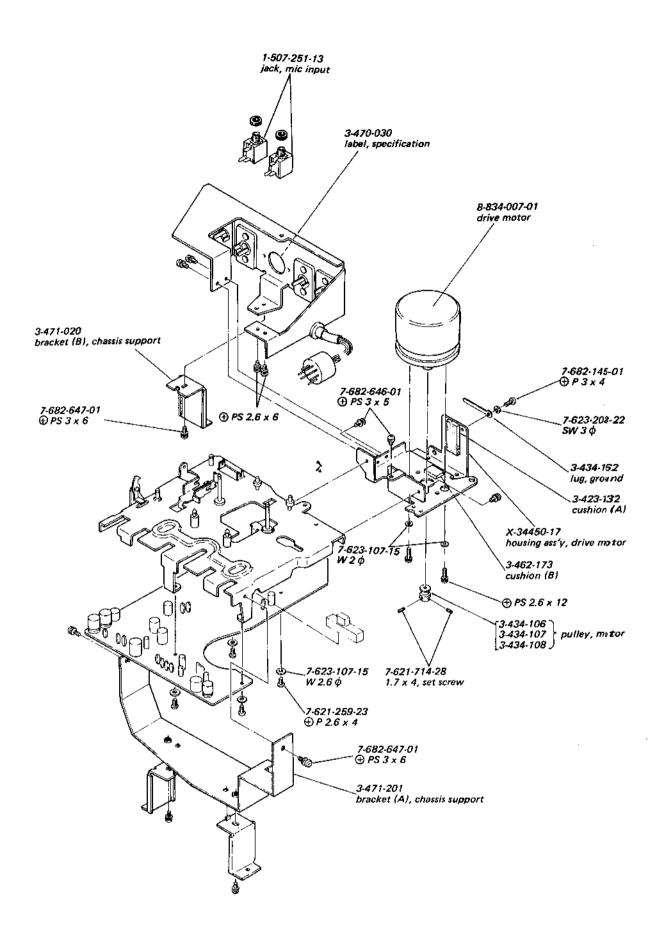
SECTION 6 EXPLODED VIEW













SECTION 7 ELECTRICAL PARTS LIST

<u>Ref. No</u> .	Part No.		Description	Ref. No.	Part No.		Description
	MOUNTED	CIRCU	IT BOARD	C314	1-107-024	200	11000 0000
	X-34710-21		/P.B amplifier circuit board		1-107-024 1-121 -4 09	200р 47	$\pm 10\%$ 500V, silvered mica $\pm {}^{100}\%$ 16V, electrolytic
	SEMIC	ONDUC	TORS		DE	SISTORS	•
D101(D20		đíod			NE: All resistance val		O 450 100
D102(D20	(2)	diod					erwise indicated.
D303		diod	e CD2		1) 1-244-721	100 k	erwise indicated.
Q101(Q20	1)	trans	istor 2SC631		2) 1-242-673	i k	
Q102(Q20	2)	trans	istor 2SC631		3) 1-244-719	82 k	
Q103(Q20	3)	trans	istor 2SC631		4) 1-242-715	56 k	
Q104(Q20		trans	istor 2SC633	ľ	5) 1-244-745	1 M	
Q105(Q20	5)	trans	istor 2SC633		6) 1-242-701	15 k	
Q106(Q20	6)	trans	istor 2SC631		7) 1-244-697	10 k	
Q301		trans	istor 2SC633	R108(R208	B) 1-242-675	1.2 k	
Q302		trans	istor 2SC633	·	9) 1-244-691	5.6 k	
TI	RANSFORME	R AND	INDUCTORS	R111(R211	1-242-637	33	
L101(L201) 1-407-200		etor, micro 3.3 mH	R112(R212	2) 1-242-771	39 k	
L102(L202			tor, micro 33 mH	R113(R213	3) 1-242-743	820 k	
L301	1-407-195		tor, micro 1 mH	R114(R214	1-242-715	56 k	
L302	1-407-165		tor, micro 47 µH	R115(R215) 1-242-715	56 k	
T301	1-433-132-2		former, osc	R116(R216	5) 1-244-753	2.2 M	
			•	R117(R217	1-244-689	4.7 k	
		ACITO		I	1-242-691	5.6 k	
			e in μF except as	l l) 1-242-689	4.7 k	
	ndicated with p			ſ) [-242-719	82 k	
) 1-121-344	3.3	±150% 25V, electrolyt) 1-242-727	180 k	
) 1-105-661-12			1) 1-242-673	1 k	
) 1-121-398	10	$\pm \frac{100}{10}\%$ 25V, electroly(~) 1-242-677	1.5 k	
) 1-121-290	100	$\pm \frac{100}{10}\%$ 3.15V, electrolyti) 1-242-641	47	
) 1-121-344	3.3	$\pm {}^{150}\%$ 25V, electrolyti	R125(R225)	1-242-701	15 k	
	1-105-667-12		3 ±10% 50V, mylar	2000	1-244-701	15 k	
	1-107-002	50 p	±10% 500V, silvered m	ica	1-242-701 1-242-693	15 k	
) 1-105-666-12) 1-121-406		7 ±10% 50V, mylar	1		6.8 k	
	1-121-409	47 4 7	±100% 3.15V, electrolyti	· 1	1-244-689	4.7 k	
	1-121-344	3.3	±100% 16 V, electrolyti		1-221-953	50 k, sem	i-fixed
	1-105-683-12		±150% 25V, electrolyti	1	1-244-711	39 k	
	1-121-344	3.3	±10% 50V, mylar ±150% 25V, electrolytic	R303 R304	1-221-401	10 k, sem	ı-tixed
	1-107-058	120p			1-242-681	2.2 k	
	1-107-053	27 p	± 10 % 500V, silvered mi		1-242-771 1-242-697	39 k	
	1-107-052	22p	±10% 500V, silvered mi		1-202-555	10 k 180 ±	F1.007 3/1V
C119(C219)	f-107-001	18p	±10% 500V, silvered mi		1-202-555		10% ¼W, composition 10% ¼W, composition
C1 20(C2 20)	1-105-661-12	0.001	±10% 50V, mylar	R309	1-244-633	22	cross viw, composition
C301	1 121 410	220	+100		1-242-609		
C302	1-121-419 1-121-419	220 220	±100% 6.3V, electrolytic	· I	1-242-609	2.2 2.2	
C303	1-129-709		$\pm \frac{100}{10}\%$ 6.3V, electrolytic		1-242-697	10 k	
C304	1-105-680-12	0.0039	± 10% 630V, polypropyl ± 10% 50V, mylar	ene		10 K	
C305	1-105-675-12	0.015	±10% 50V, mylar ±10% 50V, mylar	6,		<u> CHES</u>	
C306	1-121-396	4.7	$\pm \frac{10\%}{10\%}$ 50V, electrolytic	S1	1-514-254		ide (REC/P.B.)
C307	1-121-413	100	$\pm \frac{100}{10}\%$ 6.3V, electrolytic		1-514-053	switch, le	af (MOTOR)
C308	1-105-667-12		±10% 50V, mylar		MISCELL	ANEOUS	
C309	1-105-684-12	0.082	50V, mylar		1-506-133	7-P plu	g
C310	I-121-530	1000	±100% 12V, electrolytic		1-507-176-12	phono j	~
C311	1-121-426	470	$\pm \frac{100}{10}\%$ 16V, electrolytic		1-507-251-13	jack, m	icrophone
C312	1-121-290	100	±100% 3.15V, electrolytic		1-536-181	termina	l strip, 2L1
C313	1-121-409	47	$\pm \frac{100}{10}\%$ 16V, electrolytic		8-822-836-20		B. head
			- 10 % 10 +, electrolytic	1	8-828-136-00	erase he	
					8-834-007-01	motor,	D-007G

Sony Corporation