"TRADER" SERVICE SHEET

1149

CAPACITORS	Values	Loca- tions
C1 Aerial and earth C2 isolators Aerial series Aerial series L.W. aerial shunt C5 L.W. aerial trim C6 L.W. aerial trim C7 V1 C.G A.G.C. decoupling Lst I.F. trans. tun- C10 ing V1 cath. by-pass V1 cath. by-pass	0.005µF 0.01µF 50pF 800pF 20pF 60pF 50pF 110pF 110pF 0.05µF	H4 H4 H4 G4 H4 G4 G4 G4 G4 G3
C12 V1 osc. C.G. C13 M.W. osc. tracker C14 L.W. osc. tracker. C16 L.W. osc. trim. C17 A.G.C. decoupling C19 V2 S.G. decoupling C19 L.W. osc. trim. A.G.C. trim. C18 V2 S.G. decoupling C19 L.F. trans C21 tuning C22 Cathode by-passes	45pF 556pF 390pF 180pF 0·05μF 0·05μF 0·05μF 110pF 110pF 110pF 0·05μF	G4 G3 G3 G4 G4 G4 F4 C2 C2 F4
$ \begin{array}{c c} \text{C23*} \\ \text{C24} \\ \text{C25} \\ \text{C26} \\ \text{C27} \\ \text{C27} \\ \text{C29} \\ \text{C30} \\ \text{C31} \\ \text{C32} \\ \end{array} \right\} \begin{array}{c} \text{I.f. by-pass} \\ \text{J.f. isolators} \\ \text{M.F. coupling} \\ \text{A.G.C. coupling} \\ \text{C29} \\ \text{C30} \\ \text{A.F. coupling} \\ \text{A.F. coupling} \\ \text{C31} \\ \text{S22} \\ \end{array} \right\} \text{Neg. feed-back} \\ \text{Meg. feed-back} $	$50 \mu F$ $100 p F$ $0.005 \mu F$ $0.01 \mu F$ $0.01 \mu F$ $50 p F$ $0.002 \mu F$ $0.01 \mu F$ $0.05 \mu F$	F3 F4 H4 F3 F3 F4 E4 E4 E4
C33	$0.05\mu F \ 0.001\mu F \ 0.001\mu F \ 0.01\mu F \ 16\mu F \ 0.01\mu F \ 528pF \ 528pF \ 40pF \ 40pF \ 40pF$	E3 E4 C1 C1 D2 A2 A1 H3 H3 G4
* Electrolytic. † Variable.	‡ Pre-set	•

BUSH DAC34

A.C./D.C. Transportable Superhet

THE Bush DAC34 is a 3-band 4-valve (plus rectifier) transportable table receiver, designed to operate from A.C. or D.C. mains of 200-250 V, 40-100 c/s in the case of A.C. The total mains consumption is approximately 35 watts. The waveband ranges are 16-50 m, 182-560 m and 833-2,068 m.

Release date and original price: August, 1953, £20 0s 3d. Purchase tax extra.

CIRCUIT DESCRIPTION

Aerial input via coupling coils L2, L3, L4 to single-tuned circuits L5, C39 (S.W.) L6, C39 (M.W.) and L7, C39 (L.W.), which precede triode hexode valve (V1, Mullard UCH42)

	RESISTORS Values		Loca- tions	
R1	V1 C.G	470kΩ	G4	
R2	V1 G.B	220Ω	G4	
R3	V1 osc. C.G	$47 \mathrm{k}\Omega$	G4	
R4	A.G.C. decoupling	$1 \mathrm{M}\Omega$	F4	
R5	Osc. stabilizer	47Ω	H4	
R6	H.T. feed	$15 \mathrm{k}\Omega$	G4	
R7	A.G.C. decoupling	$2.2 \text{M}\Omega$	F4	
R8	V2 S.G. feed	$47 \mathrm{k}\Omega$	F4	
R9	V2 G.B	330Ω	F4	
R10	V2 anode decoup	$10 \mathrm{k}\Omega$	F4	
R11	Signal diode load	$330 \mathrm{k}\Omega$	F4	
R12	I.F. filter	$100 \mathrm{k}\Omega$	F3	
R13	Neg. feed-back	$47 \mathrm{k}\Omega$	F3	
R14	Volume control	$2.2 \mathrm{M}\Omega$	F3	
R15	V3 anode load	$150 \mathrm{k}\Omega$	F4	
R16	V3 G.B	$5.6 \mathrm{k}\Omega$	F4	
R17	A.G.C. diode load	$1M\Omega$	F4	
R18	V4 C.G	$470 \mathrm{k}\Omega$	F4	
R19	V4 C.G. stopper	$47 \mathrm{k}\Omega$	F4	
R20	1) [$1 \mathrm{k} \Omega$	E4	
R21	Neg. feed-back {	$10 \mathrm{k}\Omega$	E4	
R22	J	220Ω	E4	
R23 -	Tone control	$-50 \mathrm{k}\Omega$	E3	
R24	Tone corrector	$10 \mathrm{k}\Omega$	l —	
R25) (I	950Ω	D2	
R26	} Heater ballast {	150Ω	D2	
R27		150Ω	D2	
R28	V5 surge limiter	250Ω	D2	
R29	Scale lamp shunt	250Ω	D1	
R30	H.T. smoothing	$\sim 10 \mathrm{k}\Omega$	E4	

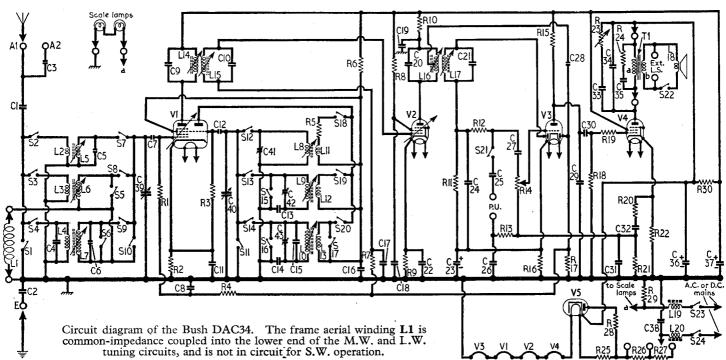


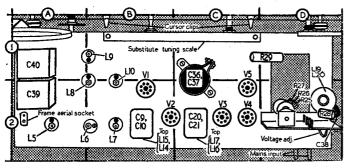
operating as frequency changer. Reception from an internal frame aerial L1 is provided on M.W. and L.W., the winding being connected in series with the chassis end of the two tuning coils.

Oscillator grid coils L8, L9 and L10 are tuned by C40. Parallel triming by C41 (S.W.), C42 (M.W.) and C43 (L.W.); series tracking by

(Continued col. 1 overleaf)

отн	ER COMPONENTS	Approx Values (ohms)	Loca tions
T-1	Frame aerial	0.5	
L2)	_	H4
$\overline{L3}$	Aerial coupling	0.6	G4
L4	coils	32.0	G4
$\widetilde{\mathbf{L5}}$	ls 71		H4
$\tilde{\mathbf{L6}}$	Aerial tuning coils	4.0	G4
$\widetilde{\mathbf{L}}\widetilde{7}$		16.0	G4
$\overline{L}8$	lí a		G3
L9	Oscillator tuning	3.2	G3
$\tilde{L}10$	$\left \left\{ \begin{array}{cccc} \text{coils} & \dots & \dots \end{array} \right\} \right $	4.0	G3
Lii	ا		G3
T.12	Oscillator reaction	0.6	G3
L13	$\left \left\{ \begin{array}{cccc} \text{coils} & \dots & \dots \end{array} \right\} \right $	1.5	G4
L14	State TE Amount (Pri.	12.5	B2
L15	$ $ 1st I.F. trans. $\{ $ Sec. $ $	12.5	B2
L16	Ond TE trans (Pri.	12.5	C2
L17	$\left. ight\}$ 2nd I.F. trans. $\left\{ egin{matrix} ext{Pri.} \ ext{Sec.} \end{matrix} ight.$	12.5	C2
L18	Speech coil	2.5	I
L19	Mains R.F. filters	3.0	D2
-L20		3.0	102
T1	O.P. trans. $\begin{cases} a & \cdots \\ b & \cdots \end{cases}$	500.0	
		0.5	_
S1-	Waveband/gram.		
S21	switches		H.4
S22	Speaker switch	_	
S23,			
S24	Mains sw., g'd R14		F3





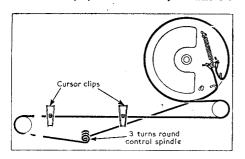
Plan view of the chassis showing the substitute tuning scale referred to in "Circuit Alignment" below.

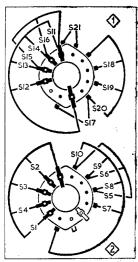
Circuit Description-continued

C13 (M.W.) and C14 (L.W.). Reaction coupling from anode by L11, L12 and L13. Second valve (V2, Mullard UF41) is a variable-mu R.F. pentode operating as intermediate frequency amplifier with tuned transformer couplings C9, L14, L15, C10 and C20, L16, L17, C21.

Intermediate frequency 470 ko/s.

Diode signal detector is part of double diode triode valve (V3, Mullard UBC41). Audio fre-





Above: Sketch of the tuning drive cord of the chassis.

Left: Diagrams of the waveband switch units, drawn as seen in the direction indicated by the arrows in the under - chassis

system as seen from the front

illustration.

quency component in its rectified output is developed across load resistor R11, and passed via C27 and volume control R14 to grid of triode section. I.F. filtering by C24, R12 and the capacitance of the screened leads.

Second diode of V3 is fed from V2 anode via C28, and the resulting D.C. potential developed across load resistor R17 is fed back as bias to V1 and V2, giving automatic gain control.

Resistance-capacitance coupling by R15, C30 and R18 between V3 and pentode output valve (V4, Mullard UL41). Tone correction in anode circuit by C34, R24 and C35. Variable tone control by R23 and C33. Negative feed-back tone correction between V4 cathode circuit and V3 grid circuit via R22, R20, C32, R21, C31 and R13.

V3 grid circuit via H22, H20, G32, H21, G31 and R13.

H.T. current is supplied by I.H.C. half-wave rectifying valve (V5, Mullard UY41).

H.T. smoothing by R30 and electrolytic capacitors G36, G37. Valve heaters, together with ballast resistors R25, R26, R27 and scale lamps, are connected in series across the mains input. Mains R.F. filtering by G38 and chokes L19, L20.

CIRCUIT ALIGNMENT

CIRCUIT ALIGNMENT

1.F. Stages.—Switch receiver to medium waves and tune it to 300 m. Connect output of signal generator, via an 0.1 µF capacitor in each lead, to control grid (pin 6) of V2 and chassis, feed in a 470 kc/s (638.3 m) signal and adjust the cores of L17 (location reference C2) and L16 (C2) for maximum output. Transfer signal generator leads to control grid (pin 6) of V1 and chassis, and, feeding in a 470 kc/s signal adjust the cores of L15 (B2) and L14 (B2) for maximum output. Repeat these adjustments until no further improvement results.

R.F. and Oscillator Stages.—In order that the receiver may be aligned with the chassis in its cabinet, three holes are provided in the cabinet base to give access to C41, C42 and C43. If, however, the chassis is removed from its cabinet for alignment, the frame aerial should be disconnected and a shorting link placed across the frame aerial sockets. As the tuning scale is fixed to the cabinet, reference should be made in this case to the substitute tuning scale fixed along the front of the chassis deck. A temporary cursor, such as a paper clip, should be fixed to the tuning drive, and, with the gang at maximum, aligned with the datum line on the substitute tuning scale.

L.W.—Switch receiver to L.W. and connect signal generator output leads to A and E

L.W.—Switch receiver to L.W. and connect signal generator output leads to A and E sockets. Tune receiver to 2,000 m, feed in a 2,000 m (150 kc/s) signal and adjust the cores of L10 (B2) and L7 (B2) for maximum output. Tune receiver to 1,000 m, feed in a 1,000 m (300 kc/s) signal and adjust 643 (G4) for maximum output. Repeat these adjustments until no further improvement results.

M.W.—Switch receiver to M.W., tune to 500 m, feed in a 500 m (600 kc/s) signal and adjust the cores of L9 (B1) and L6 (B2) for maximum output. Tune receiver to 200 m, feed in a 200 m (1,500 kc/s) signal and adjust 642 (H3) for maximum output. Repeat these adjustments until no further improvement results.

S.W.—Switch receiver to S.W., tune to 50 m, feed in a 50 m (6 Mc/s) signal and adjust the cores of L8 (B2) and L5 (A2) for maximum output. Tune receiver to 25 m, feed in a 25 m (12 Mc/s) signal and adjust 641 (H4) for maximum output. Repeat these adjustments until no further improvement results.

L.W. Check.—If alignment has been carried out with the chassis out of its cabinet, the cores of L7 and L10 should be re-adjusted for maximum output at 2,000 m (150 kc/s) after the chassis has been replaced in its cabinet and the frame aerial re-connected.

GENERAL NOTES

Switches .- S1-S21 are the waveband and radio/ Switches.—\$1-\$21 are the waveband and radio/
gram change-over switches, ganged in two rotary
units beneath the chassis. These units are indicated in our underside illustration of the
chassis and shown in detail in the switch diagram in column 1, where they are drawn as
seen in the direction of the indicating arrows
in the chassis view. In the associated switch
table, a dash indicates open, and c, closed.

\$22 is the internal speaker muting switch and
is mounted, together with the external speaker

Switches	s.w.	M.W.	L.W.	Gram.
S1				С
S2	C	-		l —
S1 S2 S3 S4 S5 S5 S5 S7 S8 S9		C	C	
S4		· —	С	-
S5	C	-		
86	C	С		
S7	C	<u> </u>		
88	_	С		
89			C	
S10		_		C
811			- - - - - -	C C C
S12 S13	C		<u> </u>	-
S13		C		
S14			С	l —
S15	C	i		
S16	C	С		
\$17 \$18	С	C	/	
S18	С			
S19	0 0000 0 00000	0 0 0 0 0 0 0		
S20			c	
S21				C

sockets, in the top rear corner of the cabinet.

Scale Lamps.—These are 3.5 V, 0.15 A lamps with large clear spherical bulbs and M.E.S.

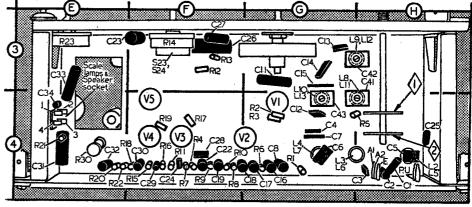
Drive Cord Replacemnt.—About 4ft 6in of nylon braided glass yarn is required for a new drive cord which should be run as shown in the sketch of the drive cord system, starting with the gang at maximum capacitance and running the cord off clockwise round the drum.

VALVE ANALYSIS

Valve voltages and currents given in the table below are those derived from the manufacturer's information. They were measured on a receiver which was operated from A.C. mains of 230 V and tuned to the highest wavelength end of M.W. There was no signal input. Voltages were measured on the 10 V and 1,000 V ranges of a Model 7 Avometer, chassis being the negative connection in every case.

Valve	Anode		Screen		Cath.
	v	mA	v	mA	v
V1 UCH42	$\begin{cases} 100 \\ \text{Oscil} \\ 48 \end{cases}$	$\left. egin{array}{c} 2\cdot 4 \ \mathrm{lator} \ 1\cdot 2 \end{array} \right\}$	48	1.2	1.0
V2 UF41 V3 UBC41	68	2·8 0·16	50	1.2	1·2 0·6
V4 UL41 V5 UY41	212 211*	25.0	96	3.2	6·4 226·0†

* A.C. reading. † Cathode current 37 mA.



Underside view of chassis. Switch units, indicated here, are shown in detail in col. 1.