"TRADER" SERVICE SHEET

UICK-RELEASE facilities are feature of the Bush AC11 receiver, whose chassis is held only by two push-in pegs and two fixing screws. receiver is a 4-valve (plus rectifier), 3-band superhet, designed to operate from A.C. mains of 100-250 V, 40-100 c/s. Wavebands are 16-50 m, 182-560 m, 830-2,068 m.

Another feature of the design is that the A.C. model can easily be converted to the A.C./D.C. model DAC11. The differences are very small, and the same valves are used in the same heater sequence. The differences between the two are explained in "Circuit Description," which is written basically on the

A.C. model.

Release date and original price, both models: June 1949; £17 13s. 7d. Purchase tax extra.

CIRCUIT DESCRIPTION

Input from external aerial is passed via socket A1 and coupling coils L1 (S.W.), L2 (M.W.) or L3 (L.W.) to single-tuned

BUSH AC11, DAC11

A.C. and A.C./D.C. Superhets

circuits L4, C34 (S.W.), L5, C34 (M.W.) or L6, C34 (L.W.), which precede first valve (V1, Mullard UCH42) operating as frequency changer with internal coupling.

A second aerial socket A2 is intended for use when interference is experienced from the local station, or when a very long aerial is used. It inserts the series capacitor C1 in the aerial lead. A frame aerial winding L7, connected via sockets 5, 6 permits the receiver to be operated without an aerial. In the A.C./D.C. model, isolating capacitors C39 and C40 are inserted in the aerial and earth leads.

V1 triode oscillator grid coils L8 (S.W.), L9 (M.W.) and L10 (L.W.) are tuned by C35. Parallel trimming by C36 (S.W.), C37 (M.W.) and C14, C38 (L.W); series tracking by C12 (M.W.) and C13 (L.W.), but tracking adjustments are made by manipulating the iron-dust cores of the tuning coils. Reaction coupling from tuning coils. anode is provided by coils L11 (S.W.), L12 (M.W.) and L13 (L.W.).

Second valve (V2, Mullard UF41) is a variable-mu R.F. pentode operating as

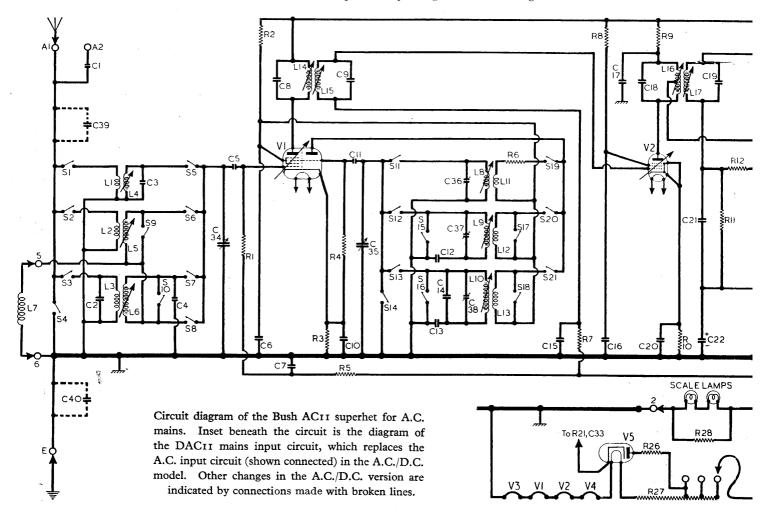
intermediate frequency amplifier with tuned-primary, tuned-secondary transformer couplings C8, L14, L15, C9 and C18, L16, L17, C19.

Intermediate frequency 465 kc/s.

Diode second detector is part of double diode triode valve (V3, Mullard UBC41). Audio frequency component in rectified output is developed across load resistor R11 and passed via I.F. stopper R12, coupling capacitor C24 and manual volume control R13 to control grid of triode sec-

tion, which operates as an A.F. amplifier. I.F. filtering by C21, R12 in diode circuit, and C28 in triode anode circuit. Provision for connection of a gramophone pick-up across R13, via C24 and C25. In A.C./D.C. models two isolating capacitors C41, C42 are inserted in the leads, and R25 is added.

Second diode of V3, fed from a tapping on L16 via C23, provides D.C. potential which is developed across load resistor R17 and fed back via decoupling circuits as G.B., to F.C. and I.F. valves, giving automatic gain control.



Resistance-capacitance coupling by R15, C29 and R18, via grid stopper R19, between V3 anode and pentode output valve (V4, Mullard UL41). Fixed tone correction by C31, R24 and C32 in anode circuit. Variable tone control by R22, C30, also in anode circuit.

In addition, voltages developed across R23 in V4 cathode circuit are fed back via a frequency-selective network R20, C26, C25, R14 to V3 triode control grid circuit. Provision is made for the connection of a low impedance external speaker across the secondary of the output transformer T1, while switch S23 permits the internal speaker to be muted.

In the A.C. model, H.T. current is supplied by half-wave rectifying valve (V5, Mullard UY41), which is fed from the complete secondary winding of the double-wound mains transformer T2. Smoothing is effected by resistor R21 and electrolytic capacitors C27, C33. Valve heaters are connected in series between tappings 7 and 12 (116.6 V) on T2 secondary, and the scale lamps are connected in series between tappings 7 and 10 (9 V).

In the A.C./D.C. model, the A.C. mains input circuit which we show connected in

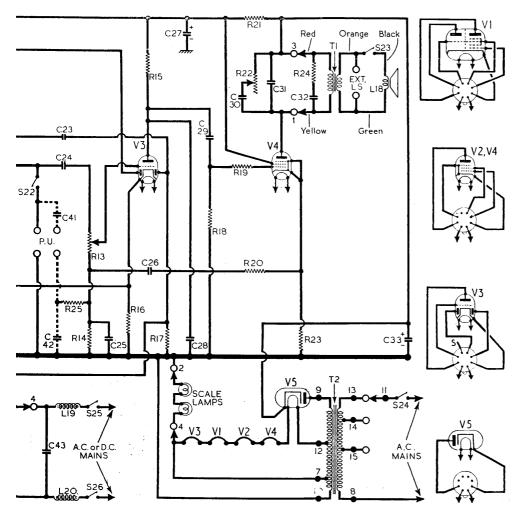
In the A.C./D.C. model, the A.C. mains input circuit which we show connected in our circuit diagram is replaced by the mains input circuit we show inset beneath the circuit diagram, to the left of the A.C. mains circuit. Here the transformer is replaced by the tapped ballast resistor R27, but the valve types and their heater

sequence remain unaltered. The scale lamps, however, are connected in series with the mains input lead to the chassis and are shunted by R28. They carry the heater and H.T. current. L19, L20 and C43 filter out mains-borne interference.

COMPONENTS AND VALUES

X	RESISTORS	Values	Loca- tions	
R1	V1 hex. C.G	$470 \mathrm{k}\Omega$	F4	
R2	H.T. feed	$15 \mathrm{k}\Omega$	F4	
R3	V1 fixed G.B	220Ω	F3	
R4	V1 osc. C.G	$47 \mathrm{k}\Omega$	F3	
R5	A.G.C. decoupling	$1 M\Omega$	E4	
R6	S.W. osc. stabilizer	47Ω	G4	
R7	A.G.C. decoupling	$2 \cdot 2M\Omega$	E4	
R8	V2 S.G. H.T. feed	$47 \mathrm{k}\Omega$	E4	
R9	V2 anode decoup	$10k\Omega$	E4	
R10	V2 fixed G.B	330Ω	E4	
R11	Sig. diode load	$330 \mathrm{k}\Omega$	E4	
R12	I.F. stopper	$100 \mathrm{k}\Omega$	E3	
R13	Volume control	$2M\Omega$	E3	
R14	F-B resistor	$4.7 \text{k}\Omega$	E3	
R15	V3 anode load	$150 \mathrm{k}\Omega$	D4	
R16.	V3 G.B	5.6kΩ	D4	
R17	A.G.C. diode load	1MΩ	E4	
R18	V4 C.G	470kΩ	$\widetilde{\mathbf{D}4}$	
R19	Grid stopper	47kΩ	$\widetilde{\mathbf{E}4}$	
R20	FB. resistor	330Ω	$\widetilde{\mathrm{D}4}$	
R21	H.T. smoothing	10kΩ	C4	
R22	Tone control	$50 \text{k}\Omega$	C3	
R23	V4 G.B	220Ω	D4	
R24	Fixed tone correct	$10 \text{k}\Omega$		
R25	P.U. coupling	47kΩ	E3	
R26	Surge limiter	150Ω	B2	
R27	Heater ballast	1·25kΩ†	BŽ	
R28	Scale lamp shunt	250Ω	100	

† tapped at $950\Omega + 150\Omega + 150\Omega$ from V5 heater.

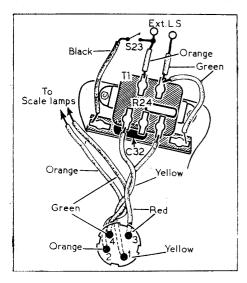




C1 C2 C3 C4 C5 C6 C7 C8 C9 C10 C11 C12 C13	Aerial series L.W. aerial shunt S.W. aerial trim L.W. aerial trim V1 hex. C.G. V1 H.T. decoup A.G.C. decoupling lst I.F. trans. { V1 cath. by-pass V1 cath. by-pass V1 cs. C.G. Osc. M.W. tracker Osc. L.W. tracker Osc. L.W. trim A.G.C. decoupling V2 S.G. decoup	50pF 800pF 20pF 60pF 50pF 0.05µF 110pF 110pF 105µF 50pF 556pF 390pF 0.05µF	G4 G4 H4 G4 F4 A2 F3 G3 G3 G3 G3
C3 C4 C5 C6 C7 C8 C9 C10 C11 C12 C13	S.W. aerial trim L.W. aerial trim V1 hex. C.G V1 H.T. decoup A.G.C. decoupling lst I.F. trans. tuning V1 cath. by-pass V1 osc. C.G Osc. M.W. tracker Osc. L.W. tracker Osc. L.W. tracker Osc. L.W. trim A.G.C. decoupling	20pf 60pf 50pf 0.05µf 0.1µf 110pf 1.00f 50pf 556pf 390pf 180pf 0.05µf	H4 G4 G4 F4 F4 A2 A2 F3 G3 G3 G3
C4 C5 C6 C7 C8 C9 C10 C11 C12 C13	L.W. aerial trim	20pf 60pf 50pf 0.05µf 0.1µf 110pf 1.00f 50pf 556pf 390pf 180pf 0.05µf	G4 G4 F4 F4 A2 A2 F3 G3 G3 G3
C5 C6 C7 C8 C9 C10 C11 C12 C13	V1 hex. C.G. V1 H.T. decoup A.G.C. decoupling 1st I.F. trans. tuning V1 cath. by-pass V1 osc. C.G. Osc. M.W. tracker Osc. L.W. tracker Osc. L.W. tracker Osc. L.W. trin. A.G.C. decoupling	50pF 0.05µF 0.1µF 110pF 110pF 0.05µF 50pF 556pF 390pF 180pF 0.05µF	G4 F4 F4 A2 A2 F3 G3 G3 G3
C6 C7 C8 C9 C10 C11 C12 C13	V1 H.T. decoup. A.G.C. decoupling lst I.F. trans. tuning V1 cath. by-pass V1 osc. C.G. Osc. M.W. tracker Osc. L.W. tranker Osc. L.W. trim. A.G.C. decoupling	0.05µF 0.1µF 110pF 110pF 1.00pF 50pF 556pF 390pF 180pF 0.05µF	F4 F4 A2 A2 F3 G3 G3 G3
C7 C8 C9 C10 C11 C12 C13	A.G.C. decoupling st I.F. trans. tuning V1 cath. by-pass V1 osc. C.G Osc. M.W. tracker Osc. L.W. tracker Osc. L.W. trim A.G.C. decoupling	$0.1\mu F$ $110pF$ $110pF$ $1.0pF$ $0.05\mu F$ $50pF$ $556pF$ $390pF$ $180pF$ $0.05\mu F$	F4 A2 A2 F3 G3 G3 G3 G3
C8 C9 C10 C11 C12 C13	A.G.C. decoupling st I.F. trans. tuning V1 cath. by-pass V1 osc. C.G Osc. M.W. tracker Osc. L.W. tracker Osc. L.W. trim A.G.C. decoupling	110pF 110pF 0·05µF 50pF 556pF 390pF 180pF 0·05µF	A2 A2 F3 G3 G3 G3 G3
C9 C10 C11 C12 C13	tuning { V1 cath. by-pass V1 osc. C.G. Osc. M.W. tracker Osc. L.W. tracker Osc. L.W. trim A.G.C. decoupling	110pF 0·05µF 50pF 556pF 390pF 180pF 0·05µF	A2 F3 G3 G3 G3 G3
C10 C11 C12 C13	V1 cath. by-pass V1 osc. C.G Osc. M.W. tracker Osc. L.W. tracker Osc. L.W. trim A.G.C. decoupling	0·05µF 50pF 556pF 390pF 180pF 0·05µF	F3 G3 G3 G3 G3
C11 C12 C13	V1 osc. C.G. Osc. M.W. tracker Osc. L.W. tracker Osc. L.W. trim. A.G.C. decoupling	50pF 556pF 390pF 180pF 0.05µF	G3 G3 G3 G3
C12 C13	Osc. M.W. tracker Osc. L.W. tracker Osc. L.W. trim A.G.C. decoupling	556pF 390pF 180pF 0.05μF	G3 G3 G3
C13	Osc. L.W. tracker Osc. L.W. trim A.G.C. decoupling	390pF 180pF 0·05μF	G3 G3
	Osc. L.W. trim A.G.C. decoupling	180pF 0·05μF	G3
	A.G.C. decoupling	$0.05\mu F$	G3
C14	A.G.C. decoupling V2 S.G. decoup		
C15	V2 S.G. decoup		F4
C16		$0.05 \mu \mathrm{F}$	F4
C17	V2 anode decoup	$0.05 \mu F$	E4
C18	$\left. \begin{array}{ll} 2nd & \text{I.F. trans.} \\ \text{tuning} & \dots & \dots \end{array} \right\}$	110 pF	B2
C19	\[\tuning \\	$110 \mathrm{pF}$	$\mathbf{B2}$
C20	V2 cath. by-pass	$0.05 \mu F$	E4
C21	I.F. by-pass	$100 \mathrm{pF}$	E4
C22*	V3 cath. by-pass	$50 \mu F$	\mathbf{D}_3
C23	A.G.C. coupling	50 pF	E4
C24	A.F. coupling	$0.01 \mu F$	E3
C25	F-B capacitors {	$0.1 \mu F$	E3
		$0.05 \mu F$	D4
C27*	H.T. smoothing	$16 \mu \mathrm{F}$	B1
C28	I.F. by-pass	$0.002 \mu F$	D4
C29	A.F. coupling	$0.01 \mu F$	D4
C30	Part tone control	$0.05 \mu F$	C3
C31	Part tone correct	$0.001 \mu F$	C3
C32 C33*	Part tone correct	$0.01 \mu F$	70.1
C34†	H.T. smoothing	$32\mu F$	B1
	Aerial tuning	528pF	A1
C35† C36‡	Oscillator tuning	528pF	A1
C371	Osc. S.W. trim	40pF	G3 G3
C381	Osc. M.W. trim Osc. L.W. trim	40pF	G3
C39	Aerial isolator	$^{40 { m pF}}_{0.005 \mu { m F}}$	G4
C40	Earth isolator		G4 G4
		$0.01 \mu F - 0.005 \mu F$	H4
C42	$P.U.$ isolators $\{$	$0.003 \mu F$ $0.1 \mu F$	D3
C43	Mains R.F. by-pass	$0.01 \mu F$	B2

* Electrolytic. † Variable. ‡ Pre-set.

ОТІ	HER COMPONENTS	Approx. Value (ohms)	Loca- tions	
L1 L2 L3 L4 L5 L6 L7 L8 L9 L10 L11 L12 L13 L14 L15 L16 L17 L18 L17 L18 L19 L20 T1 T2 S1-S22 S23 S24-	Acrial coupling coils Acrial tuning coils Frame aerial Oscillator tuning coils Oscillator reaction coils Ist I.F. trans. { Pri. Sec. Pri. Sec. Speech coil Mains R.F. filter { Chokes Output trans. { Pri. Sec. Pri. (total) Sec. Pri. (total) Sec Mains { Pri. (total) Sec Output trans. { Pri. (total) Sec Wains { Pri. (total) Sec Pri. (total) Sec W/band switchs Sp'kr. muting switch		H4 G4 G4 G4 G4 G3 F3 G3 F3 G3 F3 B2 B2 B2 B2 B2	
S26	Mains sw. g'd R13		E3 .	



Sketch of the speaker connections as seen from the rear. The plug is viewed from the free ends of its pins.

GENERAL NOTES

switches.—\$1-\$21 are the waveband and radio muting switches, and \$22 is the pick-up switch, ganged in two rotary units beneath the chassis. These units are indicated in our under-chassis view, where they are identified by the numbers 1 and 2 in diamonds, and shown in detail in the diagrams in col. 3, where they are drawn as seen when viewed from the rear of an inverted chassis.

The table (col. 3) gives the switch positions for the four control settings, starting from the fully anti-clockwise position of the control spindle. A dash indicates

open, and C, closed.

\$23 is a screw-type switch mounted with the external speaker sockets at the top right-hand corner of the cabinet. It opens when screwed a few turns anticlockwise to mute the internal speaker.

\$24 is the Q.M.B. mains switch in the A.C. model, ganged with the volume control R13. In the A.C./D.C. model it is replaced by \$25, \$26.

Scale Lamps.—In the A.C. model these are two M.E.S. types, with large clear spherical bulbs, rated at 6.2 V, 0.3 A. In the A.C./D.C. model they have smaller diameter bulbs and are rated at 3.5 V,

0.15 A. In both cases they are connected via pins 2 and 4 of the speaker connecting plug. In the A.C./D.C. model the lamps are mounted on a panel which can be withdrawn after removing two nuts.

R28 is mounted with them.

External Speaker.—Two sockets are provided on a panel mounted at the top right-hand corner of the cabinet for the connection of a low-impedance (about 2.5 Ω) speaker. The screw-type switch \$23 mounted with them permits the internal speaker to be muted.

Connecting Plugs.—A 4-pin plug and socket device is used to connect the speaker and scale lamps to the chassis. The socket is located at one end of the chassis, where it is indicated on the left in our under-chassis view.

The plug and its connecting leads are shown, together with the leads associated with the speaker in the sketch in col. 1, where the speaker transformer T1 is drawn as seen from the rear of the cabinet and the plug is viewed from the free ends of its pins, which are numbered 1-4.

The frame aerial winding L7 is connected via a 2-pin plug and socket whose pins are numbered 5 and 6. The socket is indicated on the left of our plan view of the chassis. The larger pin (6) goes to chassis

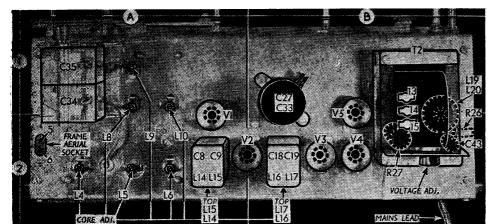
Chassis Divergency. — R16, which was 5.6 k Ω in our chassis, was 3.3 k Ω in earlier models.

VALVE ANALYSIS

Valve voltages and currents given below are those quoted by the manufacturers for the A.C. model only, which was operating from A.C. mains of 230 V using the 210-230 V tapping on **T2.** A similar set of readings taken on a model DAC11 were found to be approximately 25 per cent lower than those in the A.C. model. The receiver was tuned to M.W. and there was

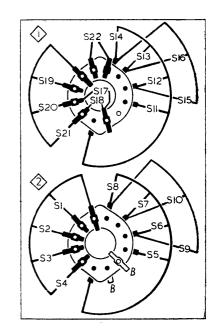
Valve	Anode Voltage (V)		Screen Volt-	Cathode	
vaive			age (V)	(V)	(mA)
V1 UCH42	$ \begin{cases} 120 \\ \text{Oscillator} \\ 60 \end{cases} $	}	60	1.2	6.0
V2 UF41 V3 UBC41 V4 UL41 V5 UY41	84 • 60 260 263†	,	62 120	$ \begin{array}{c} 1.5 \\ 0.8 \\ 8.0 \\ 282.0 \end{array} $	$5.0 \\ 0.2 \\ 35.0 \\ 46.0$

† A.C.



Plan view of the chassis, in which all the core adjustments are indicated.

Switch	S.W.	M.W.	L.W.	Gram.
S1	С			-
S1 S2		С		
83			C	
S3 S4			_	C
S5 S6 S7	C			C
86		C		
87			C	
88 89	0 0 0000 000000		0 0 0 0 0 0 0 0 0 0	00 10 10 10
S9	С	0 0 0		-
S10	С	С		
811	C		-	C
S12		С		
S13	_		C	
S14				C
S15	C	l —		
S16	C	C		
S17	С	_		
S18	C	C		
S19	C	;		
S20		С	c	
S21	<u> </u>		C	
S22				C



Diagrams of the waveband switch units, viewed from the rear of an inverted chassis. The associated table is above them.

no signal input. Anode and screen currents were not quoted.

Except for cathode readings, all voltages were measured on the 1,000 V range of a model 7 Avometer, chassis being the negative connection.

DISMANTLING THE SET

Removing Chassis.—Remove the four control knobs (pull off);

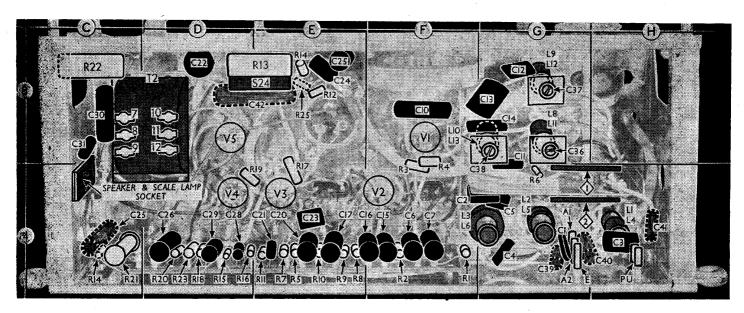
withdraw the frame aerial and speaker plugs located at opposite ends of the chassis;

remove the two chassis retaining bolts (with one large washer and spacing collar each) from the rear lower corners of the chassis;

withdraw chassis about one inch and ensure that the cursor carriage clip disengages with the cursor carriage and remains on the drive cord;

completely withdraw chassis. To operate the receiver in this position, insert frame aerial and speaker plugs.

When replacing, ensure that the rubber grommets in the front locating brackets



Under-chassis view. Six tags of the mains transformer are numbered here to agree with the circuit diagram overleaf. The other three tags are numbered in our plan view. Detailed diagrams of the waveband switch units 1 and 2 appear in col. 3.

are in position. Do not omit to reengage the cursor carriage with its driving clip on the drive cord.

Removing Speaker.—Unsolder four connecting wires and remove three 4 BA nuts (with one washer each).

When replacing, the connections should be resoldered as illustrated in our diagram in col. 1.

CIRCUIT ALIGNMENT

I.F. Stages.—Connect signal generator leads via a 0.1 µF capacitor (use two in the A.C./D.C. receiver) to control grid (pin 6) of **V2** and chassis. Switch set to M.W., tune to 300 m on scale, and turn the volume control to maximum. Keep input low to avoid A.G.C. action, reducing input as circuits come into line.

Unscrew all four I.F. cores fully, then feed in a 465 kc/s (645.16 m) signal, and adjust L17, then L16, for maximum output to the first peak encountered. Transfer signal generator lead to control grid (pin 6) of V1 and adjust the cores of L15, then L14, for maximum output in the same way. Do not readjust the cores.

R.F. and Oscillator Stages.-With the gang at maximum, the centre of the cursor should coincide with the datum lines at the long wavelength ends of the scales. It may be adjusted by sliding the cursor drive wedge along the drive cord. In order that alignment may be performed with the chassis out of its cabinet, calibration marks are scaled on the rear of the gang drum, although all adjustments are accessible while the chassis is in the cabinet. The procedure should in any case be completed, however, by readjusting the M.W. and L.W. aerial circuits with the chassis in its cabinet, as the frame winding, which is wound round the inside of the cabinet, forms part of the aerial circuit. The location references are A1, A2 and G3.

L.W.—Transfer signal generator leads to A1 and E sockets via a suitable dummy aerial (a $0.0002 \mu F$ capacitor will do).

Switch set to L.W., tune to 2,000 m on scale, feed in a 2,000 m (150 kc/s) signal, and adjust the cores of L10, then L6, for maximum output. Tune to 1,000 m on scale, feed in a 1,000 m (300 kc/s) signal, and adjust C38 for maximum output. Check calibration at 2,000 m.

M.W.—Switch set to M.W., tune to 500 m on scale, feed in a 500 m (600 kc/s) signal, and adjust the cores of L9, then L5, for maximum output. Tune to 200 m on scale, feed in a 200 m (1,500 kc/s) signal, and adjust C37 for maximum output.

Check calibration at 500 m.
S.W.—Switch set to S.W., and change dummy aerial to a 400 Ω non-inductive resistor. Tune to 50 m on scale, feed in a 50 m (60 Mc/s) signal, and adjust the cores of L8, then L4, for maximum output. Tune to 25 m on scale, feed in a 25 m (12 Mc/s) signal, and adjust C36 for maximum output. Check again at 50 m.

Finally, fit chassis into cabinet, connect up frame aerial winding (L7), and readjust L5 and L6 cores for maximum output at 500 m and 2,000 m respectively.

DRIVE CORD REPLACEMENT

About three feet of Nylon braided glass yarn is required for a new drive cord, which follows the simple course shown in the sketch below, where the chassis is viewed from the front with the gang at

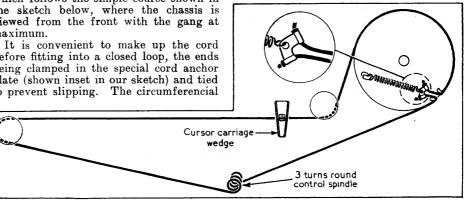
before fitting into a closed loop, the ends being clamped in the special cord anchor plate (shown inset in our sketch) and tied to prevent slipping. The circumferencial

length of the cord when so made up is $32\frac{1}{4}$ -ins. overall; or it measures $16\frac{1}{8}$ -ins. when the loop is stretched between two pins stuck in the bench.

Having made the loop, pull it out straight as for the second measurement quoted, and pass the folded end through the hole in the gang drum groove so that the anchor plate is on the inside. Wind the cord three turns round the tuning control spindle in the direction shown in the sketch, and pass over the pulleys and round the drum as shown. Then anchor the tension-spring.

The wedge which drives the cursor carriage should be fitted loosely until the chassis is fitted in the cabinet, when its grip tag can be tightened after correct positioning of the cursor carriage. This should be done as explained under "Circuit Alignment in col. 4.

It is not permissible to make adjustments of the drum on the gang spindle, as this carries on its rear face a calibrated alignment scale. The line marked "Datum" on this scale should be opposite the brass pointer fixed to the top of the gang frame when the gang is at maximum capacitance.



Sketch of the tuning drive cord, with the anchor plate device shown enlarged inset.