"TRADER" SERVICE SHEET 1256/T104

MPLOYING a 12-position turret tuner and non-gated vision A.G.C., the Ambassador TV17TM is a 17in table receiver designed for operation

from A.C. mains of 200-250V, 40-60 c/s. The receiver is fitted with sixteen Mazda valves and a Mazda C.R. tube.

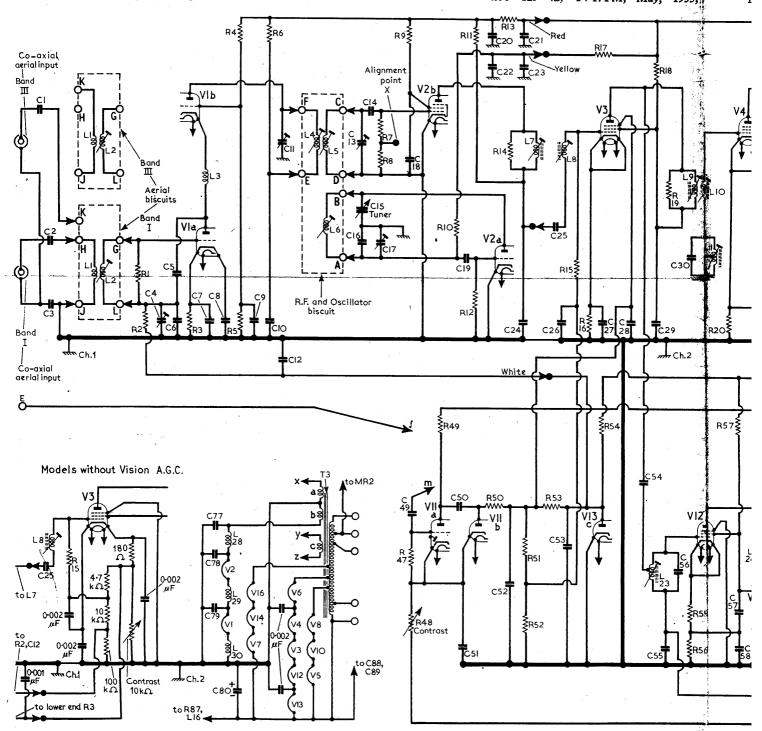
Models TV14TM and TV14CC are 14in versions, and models TV15C, TV15CC, TV15CR, TV17C, TV17CC, TV17CR are 15in and 17in versions of TV17TM. Models 21CC and TV21C are 21in console versions. Baird receivers employing the same chassis are T5614, C5614, T5617, C5617, CD5617, CR5617, C5717 and C5621. Further details of all these models are given under "Associated Models" overleaf.

AMBASSAD

Covering Nineteen

Release dates and original prices:—Ambassador Models: TV14TM, August, 1955, £52 3s 7d; TV14CC, August, 1955, £60 0s 10d; TV15CC, August, 1954, £66 3s 10d; TV15C, August, 1954, £77 12s 4d; TV15CR, August, 1954, £90 12s 4d; TV17TM, May, 1955,

£60 £61 £79 £99 £91



ADOR TV17TM Series

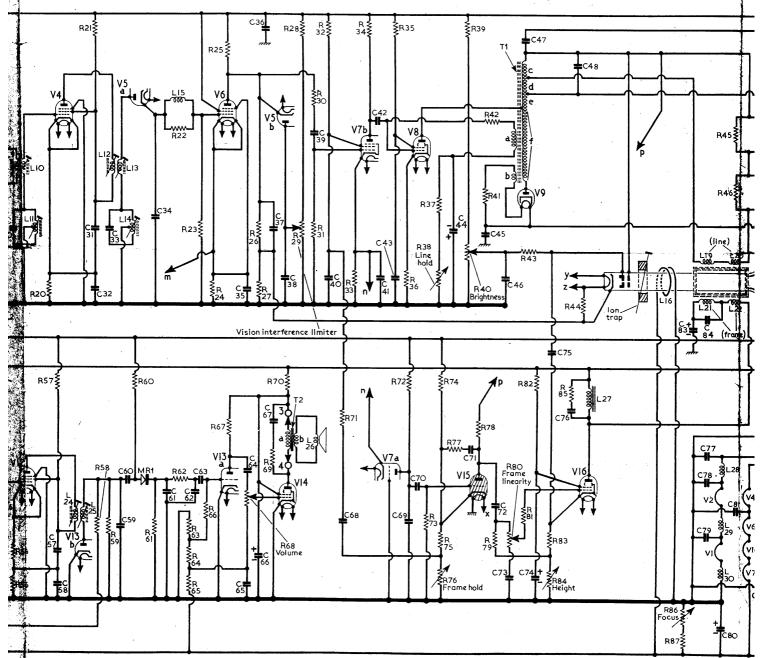
L60 15s 2d; TV17CC, May, 1955, £50 5s 5s 1 £68 5s 2d; TV17CC, May, 1955, £60 0s 10d; £68 5s 2d; TV17CR, November, 1955, £60 0s 10d; £79 6s 10d; TV17CR, November, 1955, May, 1955, £97 11s 5d; 21CC, June, 1956, £78 16s 2d. ber, 1955, £77 6s Purchase tax extra. 1955, £77 6s 15s 11d

£50 5s 9d; C5614, August, 1955, £60 0s 10d; T5617, May 1955, £57 9s 10d; C5617, May, 1955, £66 16s 0d; CD5617, May, 1955, £18 16s 0d; CR5617, November, 1955, £102 1s 6d; C5621, November, 1955, £77 6s 6d; C5717, November, 1955, £101 1s 1d. Purchase tax extra.

CIRCUIT DESCRIPTION

Separate Band I/Band III 80Ω coaxial inputs to 12-channel turret tuner unit employing a cascode connected double triode (V1, 30L1) as R.F. amplifier and a triode pentode (V2, 30C1) as frequency changer. V1a is neutralized by C4, C5 and C6. L3 resonates with the internal capacitances of V1b to maintain the gain at the high frequency end of Band III.

Output from local oscillator V2a is coupled by inter-electrode and circuit



capacitances to the mixer V2b where it combines with the output of V1 to produce separate sound and vision intermediate frequencies of 37.75 Mc/s and 34.25 Mc/s respectively.

Two-valve vision I.F. amplifier (V3, V4, 10Fi's) is coupled by stagger-tuned I.F. transformers to vision detector diode, section a of V5 (20D1). Sound channel rejection by C30, L11, and C33, 14.

Positive-going output from V5a is developed across R23 and passed to video amplifier V6 (10F1). Video correction by

L15 which resonates with stray capacitances at about 2.5 Mc/s. Negative-going output from V6 is coupled via D.C. to cathode of C.R. tube (CRT, CRM141 or CRM142 (14 in models) or CRM153 (15 in models) or CRM171 (17 in models) or CRM211 (21 in models)). The C.R. tube is focused via L16 which is energized by connecting it in series with the H.T. negative circuit. R86, R87 shunt the coil to give control of focus.

Interference pulses in V6 output drive the cathode of vision interference limiter diode V5b negative, causing it to conduct and short-circuit the video output via C38. Limiter control R29 biases

via C38. Limiter control R29 biases V5b anode positively and determines the level at which the diode conducts.

Positive-going video signal appearing in V6 cathode circuit is passed via C49 to section a of V11 (10LD11), where it is amplified and passed on to diode section b of V11. The resulting rectified output of V11b is developed across R51, R52 and is fed as vision A.G.C. bias to R52 and is fed as vision A.G.C. bias to V1a and V3. Contrast control R48

(Continued col. 1 overleaf)

	<u> </u>
VIO VIO	1
L17 Width	
LI8 Line linearity	
CRT	
	R89
C85 MR2	C89_
*** SI	L32 F1
y → d	
V6 V11 V8 V8 V10	
V7 VI2 VIO \$ / S2 C86	L33 F2
	A.C. VE I

					(Communea Con 1 Overheaf)			
	Cana	citors		C79	0.002F	K10	R67 100kΩ F6	
	Ci	$0.001 \mu F$	H_5	Č80	$0.002 \mu F$ $25 \mu F$	F7	R68 500kΩ E9	
	$\ddot{\mathbf{C}}$ 2	$0.001 \mu F$	H5	C81	0.002μ F	Ĝ5	R69 4.7kΩ F9	
	Č3	$0.001 \mu F$	Ħ5	C82	0.002μ F	Ğő	$ \begin{array}{ccccccccccccccccccccccccccccccccc$	
	Č4		H5 K11	C83	$32\mu F$	$\mathbf{E}7$	$R71 ext{ } 47k\Omega ext{ } G7$	
	C5	2pF	K11 K11	C84	$0.001 \mu F$	B2	$R72$ $47k\Omega$ $G7$	
	C6 C7	7pF 500pF	K11	C85	$32\mu F$	E7	$R/3$ $47R\Omega$ Ω	
	C7	500pF	K11	C86	$0.05 \mu \mathbf{F}$	<u>G8</u>	$R74$ 220k Ω G7	
	C 8	aqoogr	K11	C87	$0.05 \mu F$	H8	R75 3·3kΩ G7	
	C9	$0.001 \mu F$	C1	C88	$100 \mu F$	C4	R76 2.5kΩ B1	
	C10	$500 \mathrm{pF}$	J11	C89	$200 \mu F$	C4	R77 68Ω F9	
	C11		C1				R78 680kΩ G7	
	Č12	$0.001 \mu \mathrm{F}$	Ð1	Resist		K 10	R79 1MΩ H9	
	C13		J11 J10	R1	$22 k\Omega$ $47 k\Omega$	K10	R80 1MΩ H9	
	C14	33pF	J10 J10	R2 R3	120Ω	K10	R81 47kΩ G8 R82 10kΩ F9	
	C15	1001	J11	R4	120kΩ	J10	R82 10kΩ F9 R83 180Ω H8	
	C16 C17	10pF	Jii	R5	100kΩ	J 10	R84 1kΩ H9	
	C18	500pF	.T10	R6	2·2kΩ	J10	R85 15kΩ F9	
	C19	22pF	J11 K10 K10	R7	$10 \text{k}\Omega$	J10	R86 400Ω E8	
	C20	$0.002 \mu F$	K10	R8	$22k\Omega$	J10	R87 110Ω E7	
	Č21	0.002µF	K10	R9	$15k\Omega$	J10	R88 720Ω F8	
	\ddot{c} 22	0·002μF 0·001μF	Či	R10	$6.8k\Omega$	J10		
	C23	0.002μ F	K10	R11	$4.7k\Omega$	J10	Colls†	
	C24	150pF	J10	R12	$47k\Omega$	J11	T.1 17.11	
	C25	500pF	C1	R13	470Ω	J11 K10	L1 — K11 L2 — K11	
	C25 C26	500pF 0·002µF	G5	R14	$15k\Omega$	J10	L3 — K11	
	C27	$0.002 \mu F$	G5	R15 R16	$47 \mathrm{k}\Omega$	G 5	L4 — J11	
	C28	$0.002 \mu F$	G5	R16	180Ω	<u>G</u> 5	L5 — J11	
	C29	$0.001 \mu F$	G5	R17	$10 \mathrm{k}\Omega$	F6	<u>L6</u> — J11	
	C30	140pF	B1	R18	3.3 k Ω	G5	L7 — J10	
,	C31	$0.001 \mu E$		R19	10kΩ	B1	L8 — C1	
	C32*	$0.003 \mu F$	G5	R20 R21	180Ω 1kΩ	G5 G5	L9 — B1 L10 — B1	
	C33 C34	140pF 6pF	U+0	R22	47kΩ	H6	L10 — B1 L11 — B1	
	004	1 500mF	G6 H6 H6	R23	5.6kΩ	H6	L12 — B1	
	C35 C36	1,500pF 0·002μF	H6	R24	270Ω	Ħĕ	Lii Bi	
	C37	$0.25\mu F$	Hő	R.25	6·8kΩ	Ĥ6	L14 — G6	
	C38	$0.1 \mu F$	Ħ5	R26	150kΩ	Ĥ6	L15 4·5 H6	
	C39	$0.1\mu F$	H6	R27	470kΩ	H7	L16 140.0 A3	
	C40	0.05μ F	G7	R28	$220 \mathrm{k}\Omega$	H6	L17 1.3 B2	
	Č41	$0.25 \mu F$	G8	R29	$1 \mathrm{M}\Omega$	$\mathbf{H6}$	L18 1.75 B2	
	C42	300 pF	H7	R30	$10k\Omega$	H 6	L19] 4 - 4 - 1 0 0 (B2	
	C43	$300 \mathrm{pF}$	H7	R31	470kΩ	G8	L20 } total 8.3 { B2	
	C44	$2\mu \mathbf{F}$	H7	R32	$100 \mathrm{k}\Omega$	G7	L21 \ 1,100.0 \ B2	
	C45	$0.001 \mu F$	C2	R33	470Ω	G8	L22 } total { B2	
	C46	$0.1 \mu F$	G-7	R34 R35	68kΩ	H8	L23 C1	
	C47	$1.25 \mu F$	H7	K30	3kΩ	G8 H8	L24 — B2 L25 — B2	
	C48‡	200pF	B3 G6	R26 R37	$^{33\Omega}_{680\Omega}$	G7	L25 — B2 L26 3.5 —	
	C49	$0.002\mu F$		R38	10kΩ	B1	L27 1,000·0 C4	
	C50 C51	0.001µF	H6 G6	R 30	68kΩ	F8	L28 - J10	
	C52	$0.1 \mu F \ 0.25 \mu F$	G6	R39 R40	100kΩ	E9	L29 — J10	
	C52	$0.25\mu F$ $0.05\mu F$	G6	R41	10Ω	Ã2	L30 — K10	
	C54	3pF	G6	R42	ĺkΩ	H8	L31 19·0 H9	
	C55¶	.053µF	G6	R43	$47k\Omega$	G7	L32 — H8	
	C56	120pF	Βĭ	R44	$100 \mathrm{k}\Omega$	H8	L33 H8	
	C57	$0.003 \mu F$	G6	R45	2.8 k Ω	B2		
	C58	$0.003 \mu F$	G6	R46 R47	$2.8 k\Omega$	B2	Transformers†	
	C59	25pF	G6	R47	220 k Ω	<u>G</u> 6	(a 9.2)	
	C60	$0.02 \mu F$	F6	R48	$15k\Omega$	E 6	b =	
	C61	$0.001 \mu F$	F6	R49	39kΩ	H7	$T_1 < c$ 3.6 B_2	
	C62	300 pF	F6	R50	100kΩ	H 6	\ 0	
	C63	$0.02 \mu F$	F6	R51 R52	3·3 MΩ	G6 .	e 4.2 f 68.4**	
	C64	0.05μ F	F6	Koz	100kΩ	G6 G6	(f 68·4**)	
	C65,	$\begin{array}{c} 0.25 \mu \mathrm{F} \\ 32 \mu \mathrm{F} \end{array}$	F8 C4	R53 R54	470kΩ 4·7MΩ	H6	$T2 = \begin{cases} a & 340.0 \uparrow \uparrow \\ b & 1.2 \downarrow \downarrow \end{cases} H9$	
	C66	$0.005 \mu F$	F9	R55	33Ω	G6	(a 1-2++)	
	C67	0.00.45	Ġ7	R56	180Ω	ĞĞ	$\begin{bmatrix} a \\ b \end{bmatrix}$ 1.5	
	C68 C69	$0.02 \mu \mathrm{F} \\ 0.01 \mu \mathrm{F}$	G7	R57	2·2kΩ	G6	1.0	
	C70	100pF	G8	R58	$1M\Omega$	Ğő	13 \ d 110 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	
	C71§	$0.2\mu F$	F8	R59	100 k Ω	G6	e 2.5	
	C72	0·5μF	G9	R60	$10M\Omega$	F6 F6	e 2.5 f 5.5	
	Č73	0.01µF	Ğ9	R61	$1M\Omega$	F6	1	
	C74	$32\mu F$	C4	R.62	$33k\Omega$	F6	Miscella neous	
	C75	$0.005 \mu F$	G7	R63	. 150kΩ	E8	MR1 M188 F6	
	C76	$0.1 \mu F$	F9	R64	680kΩ	F7		
	C77 C78	$0.002 \mu F$	K10	R65	1MΩ	F7	F1, F2 2A fuse H8 S1, S2 — E9	
	C78	$500 \mathrm{pF}$	J10	R66	$1M\Omega$	F6	S1, S2 — E9	
_	+ m		1115 0.009	I in nor	Ilal + A nnrc	rimata D	Tesistance in chara +000-11-14	

*Two capacitors, $0.001\mu\text{F} + 0.002\mu\text{F}$, in parallel. †Approximate D.C. resistance in ohms. †260pF in 14in todels. \$Two $0.1\mu\text{F}$ capacitors in parallel. ¶Two capacitors, $0.05\mu\text{F} + 0.003\mu\text{F}$ in parallel. **May be 14·4 Ω . ††270 Ω in 14in models. ‡‡0·4 Ω in 14in models. \$\$S.T.C.

Left: Circuit diagram of Ambassador TV17TM. C71 is the charging capacitor associated with the frame time-base thyraton oscillator V15. Non-A.G.C differences are shown inset.

AMBASSADOR/BAIRD Series

Circuit Description-continued

varies the cathode bias on V11b and control the level of A.G.C. voltage.

In order to prevent the input impedance of V3 from varying with changes in the A.G.C. level, the full A.G.C. voltage is applied to its supressor grid, but only a proportion of it, that developed across R52 to its control grid.

V6 output is also fed via R30, C39 to sync separator valve, section b of V7 (10C2). Line sync pulses in V7b output are coupled via differentiator C42 to single-valve line time-base and output stage (V8, 20P4). Reaction coupling via grid winding a on line output transformer T1. Output from V8 is coupled via winding c-e on T1 to line deflector coils L19, L20.

Efficiency diode V10 (U301) is fed with energy from windings c, d on T1, and the resulting rectified output is developed across reservoir capacitor C47 and is used to boost the H.T. supply to V8 anode, CRT first anode and V15.

E.H.T. current is obtained from the line fly-back energy and is rectified by V9 (U25), sections c-e and f on T1 forming an auto-transformer to step-up the fly-back pulse voltage. V9 draws its heater current from winding b on T1 via R41, which drops excess volts.

To maintain a steady frame time-base interlace, the frame time-base is synchronized via two separate sync pulse paths. The first feeds sync pulses developed in V7b screen grid circuit via R71, C68 to the cathode circuit of the thyraton frame time-base oscillator valve (V15, 6K25); the second feeds sync pulses developed in V7b cathode circuit, via earthed-grid sync amplifier V7a, to the grid circuit of V15.

Saw-tooth voltage appearing at V15 anode is resistance-capacitance coupled via R78, C72, R79 to frame output valve V16 (10P14). Frame linearity control by R80, C73 in V16 control grid circuit. Frame pulses appearing in V16 cathode circuit are fed via C75 to CRT grid circuit where they suppress the frame flyback trace. V16 output is choke-capacitance coupled by L27, C83 to the frame deflector coils L21, L22.



Appearance of the Baird C5617.

Supplement to Wireless & Electrical Trader, 30 June 1956

ASSOCIATED MODELS

This Service Sheet was prepared from an Ambassador TV17TM, a 17in table receiver employing a CRM171 C.R. tube. Model TV14TM.—This is a 14in version

Model TV14TM.—This is a 14in version of the TV17TM employing a CRM141 or CRM142 C.R. tube.

Model TV14CC.—Corner console version of the TV14TM.

Model TV15CC.—This is a 15in corner console version of the TV17TM employing a CRM153 C.R. tube. Vision A.G.C. is omitted in this model (see "Modification")

Model TV15C.—This is a de-luxe version of the TV15CC.

Model TV15CR.—This is a de-luxe version of the TV15CC employing a 5-valve 3-band Ambassador "Coronet" radio chassis.

Model TV17CC.—This is a corner console version of the TV17TM.

Model TV17C.—This is a corner console version of the TV17TM with doors.

Model TV17CR.—This is a corner console receiver fitted with a TV17TM chassis and the Ambassador A.M./F.M. radio chassis.

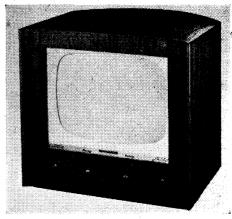
Model TV21C.—This is a 21in console version of the TV17TM with doors. It employs a CRM211 C.R. tube.

Model 21CC.—This is a 21in Continental-styled console version of the TV17TM. It employs a CRM211 C.R. tube.

Baird receivers employing a basic TV17TM chassis are as follows:—

Model T5614.—14in table receiver employing CRM141 or CRM142 C.R. tube.

1256/T104



Appearance of the Ambassador TV17TM.

Model C5614.—Corner console version of the T5614.

Model T5617.—17in version of the T5614 employing a CRM171 C.R. tube.

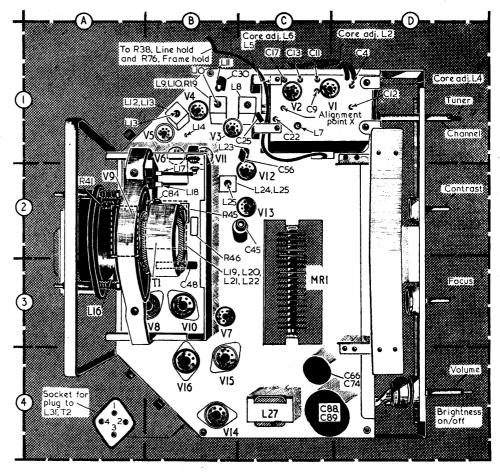
Model C5617.—17in corner console version of the T5614 employing a CRM171 C.R. tube.

Model CD5617.— A_s model C5617 but with doors.

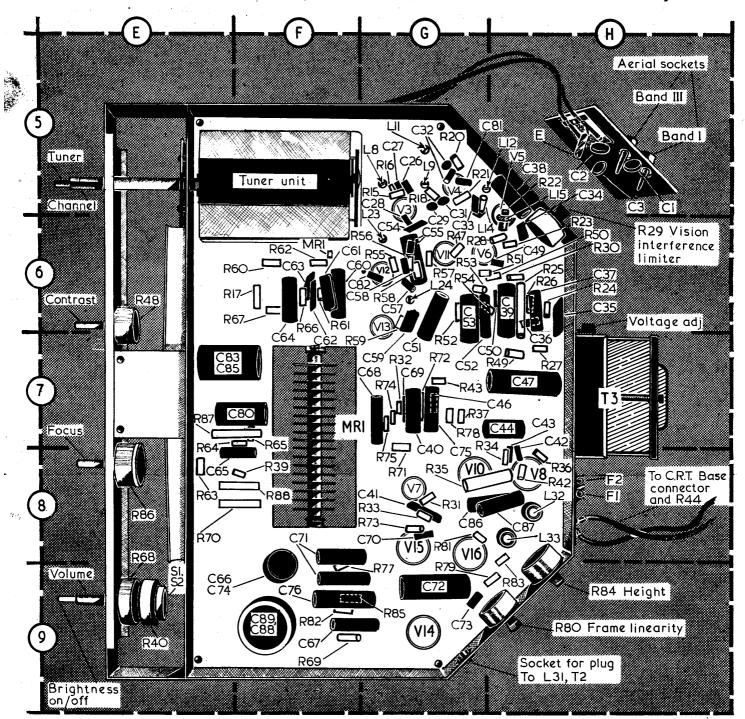
Model CR5617.—As model C5617 but with doors and Baird 301 A.M./F.M. radio chassis.

Model C5621.—21in console version of the T5614 employing CRM211 C.R. tube.

Model C5717.—As model C5617 but in cheaper cabinet.

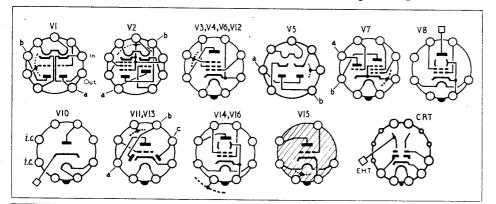


Plan view of the chassis. The H.T. choke and speaker transformer are connected to the chassis via the 4-pin socket shown, location reference A4.



Above: Under-chassis illustration.

Below: Valve base diagrams.



MODIFICATION

The vision A.G.C. circuit was not fitted to any of the 15in models, or to early versions of the 14in and 17in models. A section of circuit showing the differences in V3 cathode circuit and in the heater circuit in models not employing vision A.G.C. is inset the lower left corner of the diagram overleaf. The lower end of R3 was returned to the top of the contrast control in V3 cathode instead of to chassis. V13c anode was strapped to chassis.

VALVE ANALYSIS

Valve voltages and currents given in the table (next col.) are derived from the manufacturers' information. They

were measured with the receiver operating from 230 V mains. The contrast control was turned to maximum and the remaining controls were set as for normal operation. There was no signal input.

Voltages were measured on a Model 8 Avometer, chassis being the negative connection in every case. The voltage measured across C80 was 22 V positive connection to chassis.

	Valve	Anode (V)	Screen (V)	Cath.	
V1	30L1 ·	a 85 b 175	_	0·6 85·0	
V2	30C1	a 40 b 145	145		
V3			145		
	10F1	150	150	1.5	
	10F1	175	175	1.7	
	20D1	··· . 			
V6	10F1	140	185	2.0	
V7		a 45		2.0	
		b 150	120	2.0	
	20P4	*	175	4.8**	
V9	U25	*		11.5kV†	
V10	U301	225		430.0±	
V11	10LD11 {	a 80		-20.0	
V 11	TOPDIT &	b *		-20.0	
V12	10F1	165	165	1.8	
-		a 65			
V13	10LD11 <	b —	_		
		e -	<u> </u>		
	10P14	160	178		
V15	6K25	80	1 -	7.5	
V16	10P14	165	155	45.011	
MR1		230¶		230.0‡‡	
CRT CRM171§ Cathode 105V; 1st anode 430V; final anode 11.5kV†.					

*No reading given. †Measured on electrostatic meter; 10.5kV in 14in models; 15.5kV in 21in. models. †Measured at junction C47, C48, \$CRM141 or CRM142 (14in models). CRM153 (15in models) CRM211 (21in models). ¶A.C. reading.

**125mA
††45mA
‡;285mA
Cathode currents.

CIRCUIT ALIGNMENT

Apparatus Required.—An accurately calibrated signal generator with an output impedance of 80Ω ; a 0-100 V D.C. voltmeter for use as vision output meter: a 0-200 mW meter for use as sound output meter; and a damping unit consisting of a $470\,\Omega$ resistor in series with an $0.003\,\mu\mathrm{F}$ capacitor.

Connect vision output meter across R25 (location reference H6); connect sound output meter across T2 secondary winding. Feed in an unmodulated signal for vision alignment, and a 30%

I.F. Alignment Table

Sig. Gen. Output (Mc/s)	Shunt	Adjust	Loca- tion	Meter deflec- tion			
35.5*	L13‡	L12	H5	Max. V			
36.0*	L12	L13	B1	Max. V			
37.75*		L14	Βî	Min. V			
Rei	peat the		tments	DEIII. Y			
35.5*	L108	L9	G5	Max. V			
36.75*	L9	L10	Βĭ	Max. V			
37.75*		· L11	$\widetilde{\mathbf{G}}\widetilde{5}$	Min. V			
Repea	t last t	hree adj					
37.75*	1 -	L24	G6	Max. S			
37.75*	l —	$\tilde{L}25$	$\tilde{\mathbf{B}}\tilde{2}$	Max. S			
Repeat	last two			11011. 15			
37.75*		L23	G6	Min. V			
37.75*		L14	B1	Min. V			
37.75*	_	Ĺii	$\widetilde{G}\overline{5}$	Min. V			
37.75*		$\tilde{L}23$	Ğ6	Min. V			
37.0†	L8	17°	Čĭ	Max. V			
35·0†	L7	L8	Ğ5	Max. V			
	eat last		iustment				
respons the the adjustments.							

*Feed in at V3 control grid (pin 6). †Feed in at alignment point X (location C1). ‡Connect damping unit between chassis and V5a

anode (pin 2).

§Connect damping unit between chassis and V4 control grid (pin 6).

modulated signal for sound alignment. "V" under "Meter deflection" in the in the alignment tables means vision, and "S" means sound. "Max. V" means maximum reading on the vision meter.

I.F. STAGES

Connect output of signal generator as indicated in the I.F. alignment table. Connect damping unit as indicated under "Shunt" in the table. If two peaks are found when making a core adjustment, the core should be set to the one nearer the adjusting end of the former. Adjust as instructed in the I.F. table.

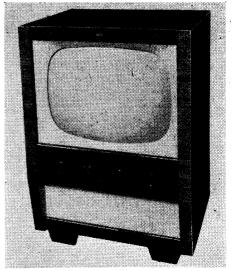
Tuner Unit Alignment Table

Sig. Gen. Output	Shunt	Adjust	Loca- tion	Meter deflec- tion	
*		L6	C1	Min. V	
†	L_5	L4	D1	Max. V	
†	L4	L5	C1	Max. V	
Repe	at last	two ad	justment	s.	
†		L2	D1	Max. V	

*Sound carrier frequency. †Sound carrier plus 2 Mc/s for ch. 1; plus $2\cdot25$ Mc/s for ch. 2-5; or plus $1\cdot75$ Mc/s for ch. 6-13.

R.F. and Oscillator Stages

Switch receiver to local channel and transfer signal generator leads to appropriate aerial socket. Adjust tuner control C15 to its mid-position. Trimmers C4, C11, C13 and C17 have been accur1256/T104



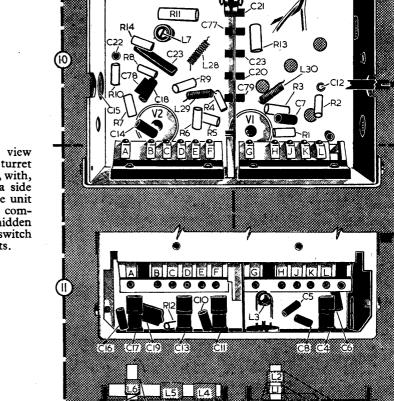
Appearance of the Baird C5621.

ately adjusted at the factory and should not normally be disturbed. If, however, the replacement of a valve in the tuner unit affects the alignment of the unit, the appropriate trimmers (C4, C11 for V1; C13, C17 for V2) should be carefully adjusted to correct this. Carry out the adjustments in the order given in the tuner unit alignment table.

Band I

Band III

Corris		Band III Channel Frequencies in Mc/s							
Carrier		6	7	8	9	10	11	12	13
Sound Vision		176·25 179·75	181·25 184·75	186·25 189·75	191·25 194·75	196·25 199·75	201·25 204·75	206·25 209·75	211·25 214·75



Underside view of the turret tuner unit, with, below it, a side view of the unit showing ponents hidden by the switch contacts.