

## $220-240$ Volts or $100-120$ Volts <br> Model X25

Model CCN 220 volss or 240 vols
The leakage current of the NEW $\times 25$
is only a few microamps and cannot harm the most delicate equipment even when soldered "live" Tested at 1500 v . A.C. This 25 watt iron with it's truly remarkable heat-capacity will easily "out-solder" any conventionally made 40 and 60 watt soldering irons, due to its unique construction advantages.

Fitted long-life iron-coated bit $1 / 8^{\prime \prime}$
2 other bits available $3 / 32^{\prime \prime}$ and $3 / 16^{\prime \prime}$.

Totally enclosed element in ceramic and steel shaft Bits do not "freeze" and can easily be removed

PRICE: $£ 1.75$ (rec. retail) Suitable for production work and as a general purpose iron

The 15 watt miniature model CCN also has negligible leakage. - Test voltage 4000 v . A.C. Totally enciosed element in ceramic shaft. Fitted long-life iron-coated bit $3 / 32^{\prime \prime}$ 4 other bits available $1 / 8^{\prime \prime}, 3 / 16^{\prime \prime} 1 / 4^{\prime \prime}$ and $1 / 16^{\prime \prime}$ PRICE: $£ 1.80$ (rec. retail) OR Fitted with triple-coated, (iron, nickel and Chromium) bit $1 / 8^{\prime \prime}$ PRICE: $£ 1.95$ (rec. retail)


## MODEL CN

Miniature 15 watt soldering iron fitted $3 / 32^{\prime \prime}$ ironcoated bit. Many other bits available from $3 / 64^{\prime \prime}$ to $3 / 16^{\prime \prime}$. Voltages $240,220,110,50$ or 24
PRICE: £1.70 (rec. retail)
MODEL CN2
Miniature 15 watt soldering iron fitted with nickel plated bit $3 / 32^{\prime \prime}$. Voltages 240 or 220 .
PRICE. $£ 1.70$ (rec. retail)


## MODEL G

18 Watt miniature iron, fitted with long life ironcoated bit $3 / 32^{\prime \prime}$. Voltages 240,220 or 110. PRICE. $£ 1.83$ (rec. retail)
contains 15 Watt miniature iron fitted with $3 / 16^{\prime \prime}$ bit, 2 spare bits $5 / 32^{\prime \prime}$ and $3 / 32^{\prime \prime}$, heat sink, solder, stand and "How to Solder" booklet.
PRICE $£ 2.75$
miniature iron fitted with $3 / 16^{\prime \prime}$ bit,

(Rec. retail)
MODEL SK. 2 KIT
contains 15 Watt
2 spare bits $5 / 32^{\prime \prime}$ and $3 / 32^{\prime \prime}$
heat sink solder and booklet"How to Solder

MODEL


PRICE £2.40
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| 1 | 5\% | 2.2-10M | E12 | 2p | 1.5p |
| 4 | 10\% | 1-10 0 hm | El 2 | 6p |  |
| Quantity | ces availabl | any select | Ignore fr | ns on | or |

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$25 \mathrm{~V}, 220 \mu \mathrm{~F}, 11 \mathrm{p}, 25 \mathrm{~V}, 470 \mu \mathrm{~F}, 13 \mathrm{p}, 25 \mathrm{~V}, 680 \mu \mathrm{~F}, 20 \mathrm{p}, 25 \mathrm{~V}, 1000,25 \mathrm{p}$ $25 \mathrm{~V}, 220 \mu \mathrm{~F}, 11 \mathrm{p} ; 25 \mathrm{~V}, 470 \mu \mathrm{~F}, 13 \mathrm{p} ; 25 \mathrm{~V}, 680 \mu \mathrm{~F}, 20 \mathrm{p}: 25 \mathrm{~V}$, $1.000 \mu \mathrm{~F}, \mathbf{2 5 p}$.
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| Stereo screened | 30p | 3.5 mm screened | 10p |
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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AC126 | 12p | BC109 | 8 p | BFYSO | 22p | $0 \mathrm{OC7O}$ | 10p |
| ACl27 | 12 p | BC147 | $12 p$ | BFY51 | 22p | OC71 | 10 p |
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OAB5 7p; OA90 5p: OA91 5p; IN4001 6p; IN4004 7p; IN4007 7p. Bridge Rectifier WOI IA 100 V price 35p.

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$1 K-2 M$ log or linear. Single gang, $12 p$.
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$5 K-2 M$
log or or linear. Dual gang, $37 p$
24 p .
Knobs for above. 10 p .

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|  | Matrix | Matrix |  | Matrix |
| $2 \operatorname{lin} \times \mathrm{in}$ | 22p | 10p | IVin $\times$ Sin (plain) | 82p |
| 3in $\times 3 \pm i n$ | 24p | 24p | 17in 2 tin (plain) | 42 p |
| 3 l in $\times 5 \mathrm{in}$ | 27p | 27p | PIN INSERTION TOOL | 52 p |
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## MODEL TH-12

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## 50 . 1



MODEL C-7080 EN
Giant fin mirrer
 $1,000 / 5,000 \mathrm{Vd,c} 0 / 2 \cdot 5 / 1$ $0 / 50 \mu \mathrm{~A} / 1 / 10 / 100 / 200 \mathrm{ma}$ 10 amp. d.c. $0 / 2 \mathrm{k} / 200 \mathrm{~K}$ 20 meg.
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U4312 MULTIMETER Fxtrmely sturdy instrume
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$0 / 300 \mu \mathrm{~A} / 1 \cdot \mathrm{~s} / \mathrm{6} / \mathrm{a} / 60 / 1$. 510.5/5b amp. (.e.

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| Noise | Bette | than | 75 dB |
| Supply voltage | 25 | , SA25/ |  |
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| 2 N 22 l | 0.22 |

$\begin{array}{ll}2 N 2 y & 0.29\end{array}$ $\begin{array}{ll}2 \mathrm{NOPLO} & 0.24 \\ 2 \mathrm{~N} 252 & 0.09\end{array}$



 $\begin{array}{llllll}2 N 2411 & 0.261 & 2 N 339 J & 0.181 & 2 N 4287 & 0.181 \\ 0 N 24+1 \% & 0.261 & N 3400 & 0.28 & 2 N 4288 & 0.18\end{array}$

 $\begin{array}{llllll}2 N 2741 & 0.28 & 2 N 3404 & 0.81 & 2 \mathrm{~N} 4290 & 0.18 \\ 2 \mathrm{~N} 2711 & 0.88 & 2 \mathrm{~N} 3405 & 0.46 & \mathrm{~N} 42991 & 0.18\end{array}$ $\begin{array}{llllll}2 \mathrm{~N} 2714 & 0.88 & 2 \mathrm{~N} 3414 & 0.161 & 2 \mathrm{~N} 4292 & 0.18 \\ 2 \mathrm{~N} 2904 & 0.181 & 2 \mathrm{~N} 3415 & 0.161 & -\mathrm{N} \$ 293 & 0.18\end{array}$ | $2 N 2904.4$ | 0.28 | $2 N 3415$ | 0.81 | -N $517 \%$ | 0.13 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $N 290.7$ | 0.28 | $2 N 3417$ | 0.31 | $2 N 5457$ | 0.28 |

 | $2 N 2906.1$ | 0.20 | $2 N 3702$ | 0.11 | 28301 | 0.56 |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | 2 N 2907 | 0.22 | 2 N 3703 | 0.11 | 2830.2 S |
| N .40 .48 |  |  |  |  |  | $\begin{array}{llllll}2 \mathrm{~N} 2923 & 0.151 & 2 \mathrm{~N} 3708 & 0.11 & 28303 & 0.60 \% \\ 2 \mathrm{~N} 2924 & 0.15 & 2 \mathrm{~N} 370 \mathrm{~B} & 0.10 & 28034 & 0.77\end{array}$

 $\begin{array}{ccccc}0.18 & 2 N 3711 & 0.10 & 28322 & 0.61 \\ & 2 \times 3819 & 0.81 & 28322.4 & 0.48\end{array}$

 $\begin{array}{llllll}2 N 3011 & 0.151 & 2 N 3906 & 0.30 & 40361 & 0.44 \\ 2 N 3053 & 0.181 & 2 N 4058 & 0.18 & 40362 & 0.481\end{array}$

DIODES AND RECTIPIERS

| A.1119 | 0.09 | HY133 | 0.28 | 0.410 | 0.88 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AA1:0 | 0.09 | BY164 | 0.85 | 0 A 47 | 07 |
| AA129 | 0.09 | HYX $38 /$ | 130 | 0.40 | 0.071 |
| A. Y 30 | 0.10 |  | 0.48 | 0.79 | 0.07 |
| -A213 | 0.11 | BYZ10 | 0.381 | 0.481 | 07 |
| B. 1100 | 0.11 | YZ11 | 0.38 | 0.885 | 10 |
| 1116 | 0.28 | YZ12 | 0.83 | 0.490 | . |
| 1 | 0.24 | BYZ13 | 0.271 |  | . 06 |
| RA148 | 0.151 | BYZ16 | 0.44 | 0.495 | 0.07 |
| HAlo | 0.13 | HYZ17 | 0.38 | 0.4200 | 0.08 |
| HA155 | 0.151 | BYZ18 | 0.381 | O.420' | 0.07 |
| B.1156 | 0.14 | BYZ19 | 0.81 | 8110 | . 05 |
| 3Y100 | 0.164 | CO62 |  | 8D19 | 0.05 |
| HY10] | 0.18 | (0.491 | Eq.) | 1N34 | 0.07 |
| by 100 | 0.181 |  | 0.054 | 1N34.4 | 0.07 |
| HY114 | 0.18 | Cifisl- |  | 1N914 | - |
| HY1:2 | 0.151 | (OA70 0 | 0.479) | 1N916 |  |
| HY127 | 0.181 |  | 0.081 | $1 \mathrm{~N}+1$ +B | 00 |
| HY 128 | 0.16 | OANo | 0.383 | 18021 | 0.11 |
|  |  |  | 0.88 |  |  |

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100 \& 0.04 \& 0.067 \& $0.05 \frac{1}{2}$ \& $0.14 \frac{1}{4}$ \& $0.17 \frac{1}{2}$ \& 0.25 <br>
-200 \& 0.051 \& 0.10 \& $0.82 \frac{1}{2}$ <br>
\hline

 

200 \& 0.051 \& 0.10 \& $0.06 \frac{1}{2}$ \& 0.151 \& 0.22 \& $0.28 \frac{1}{2}$ <br>
\hline 100 \& 1.061 \& 0.14 \& $0.07 \frac{1}{2}$ \& 0.22 \& 0.30 \& $0.40 \frac{1}{4}$ <br>
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$1 . \mathrm{mb}$ into $50 \mathrm{~K} \Omega$
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OA90, OA91. OA95, 6p exth: OA200, 9p; OA202, 10p.
Other semiconductors: AC128, 17p; AFII7. 35p: BFY51. 19p. Full lists and technical data will be found in Caralogue No. 6.

## SIEMENS' THYRISTORS <br> $0.8 \mathrm{~A} 400 \mathrm{~V} 56 \mathrm{p}, 600 \mathrm{~V} 70 \mathrm{p}$.

$3 \mathrm{~A} 400 \mathrm{~V} 60 \mathrm{p}, 600 \mathrm{~V} 88 \mathrm{p}$
ZENER DIODES full range E24 values: 400 mW $2.7 V$ to 36 V . 14 peach: IW: 68 V to 82 V , 21 p each 15 W rating to 3 wates (rype 266 F ) 4 p .

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by Hishmann, AA rating


2 way L5 -socker 10p, plug 12p
3 way scr.-socket 10p, plug 12p
5 way scr,-socket IIp, plug i5p
TRANSISTOR ACCESSORIES
TO3 cover. ${ }^{2} \mathrm{P}$; Heat sinks $1^{\circ} \mathrm{C} / \mathrm{W}$, type 6 W undrilled, 60p.

## SWITCHES

$\begin{array}{lr}1011 & \text { SPST } \\ \text { 20gile, } 20 \mathrm{p}: & 409\end{array}$ toggle, 20p;
OPDT toggle, 299
209
 (these are chrome
plated, 2.5 A rating): 7201 sub-miniature DPDT 250 V a.c. $/ 2 \mathrm{~A}, 48 \mathrm{p}$.

## ROTARY SWITCHES

Radiospares Miniature Maka-switch (in assembly kis
form). 5haft, 48p. Wafers. MBB-2PSW. IPIIW form). Shaft, 48p. Wafers, MBB-2P5W. IPIIW
BBMIPI2W, $2 P 6 W$, 3 P4W, 4P3W. 6P2W.

## WAVECHANGE SWITCHES

|P12W, 2P6W, 3P4W, 413W, 32p each

60p
25p
42p
40p
3p 26p

27p


1
ELECTROLYTIC CAPACITORS
Raced
Capacity $\mu \mathrm{F}$

POLYCARBONATE-5; TOLERANCE
250 V up to $0.1 \mu \mathrm{~F}: 100 \mathrm{~V}, 0.1 / 1 \mathrm{~F}$ and
0.01: 0.012: 0.015: 0.018: 0022
 $\begin{array}{ll:l:l}0.027: & 0.033 ; & 0.047 ; 0.056 ; 4 p \text { each } \\ 0.068: & 0082: 0.1: 0.12: 0.45: 4 p\end{array}$ $\begin{array}{cccccc}0.068 ; & 0 & 082 ; & 0.1 & 0.12: & 0.15 ; \\ \text { each, } & 0.18 ; & 0.22 ; & 5 p & \text { each. } & 0 \\ 0.33, & 6 p . & 0.397 p . & 0.47 & 8 p . & 0.56\end{array}$ $\begin{array}{lll}0.33, & 6 p & 0.397 p . \\ 10 p . & 0.68 \text { ilp. } 1 \mu \mathrm{~F} 13 \mathrm{p} .\end{array}$
MINITRON DIGITAL
COUNTER
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\& 136 . DIL socket, nert $\& 2$.


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WW = wire wound, Plessey.
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E12 denotes series: $10,12,15,18,22,27,33,39.47,56,68,82$
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$(17 \mathrm{~mm})$ aluminium, 24 p each )


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MT3 $30 \mathrm{~V} / 2 \mathrm{~A}$ plus 4 taps

MTI 103 50V/AA plus 4 taps MT103 SOV/AA plus 4 taps MT $12760 \mathrm{~V} / 2 \mathrm{~A}$ plus 4 taps | $13 T O 513 V / \frac{1}{2} A . C T$ | $C 3.80$ |
| :--- | ---: |
| $2 B T O 512+12 V .2-0-2 V$ | $C 1.25$ |

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No. 6 ( 4 th printing) contains details of 100 's of semiconductors: ICs with circuit diagrams. R's and with accessories, components, kind, 25p materials, etc.. information and
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SINGLE P20 lin. 100 a to
2.2 M : 12D; JP20 Log. 4 K 0 ).

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47 K . IM $\Omega$ only. 42 p : Dual ancilog. 10 K only, 42p. Any type with 2A D.P. mains switeh, $12 p$ exera.
Only decad
Only decades of 10,22 and 47
 available in ranges quoted.
DUAL CONCENTRICDP20 in any combination of $\mathbf{P 2 O}_{20}$
values. $\mathbf{~} 0$ p; with switeh, 72 p . values. ${ }^{\text {80 }}$
SLIDER
Lin. or log. IOK to 1 mes
popular values, each 26 p . popular values, each 26p. yel/gr/blue/dk. grey/lt. grey,
CARBON SKELETON PRE.
SETS
Small hish quality. PR lin.
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[^7]
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## STEREO RADIO WITHOUT TEARS

THE stereo tuner described this month has a number of interesting features which reflect some of the current approaches to domestic receiver design, as practised by set manufacturers.

In the field of domestic radio receivers, the integrated circuit has yet to make its full contribution. Various subsections of the conventional superheterodyne circuit have been designed and produced in monolithic form, but all these devices require additional discrete components in order to function. Thus the apparent labour- and material-saving advantages of i.c.s are largely nullified. The chief problem is one of inductances and capacitances. This real difficulty associated with monolithic circuits has encouraged further investigation into less conventional receiver designs where there is no dependence on LC tuned circuits. For example, the phase-locked-loop or synchronous detector receiver has been much discussed of late, as a likely future substitute for the classic superhet.

The i.c. has however made a noteworthy contribution to stereo receiver design. Single chip phase-locked decoders have been around for some time, and they represent perhaps the most highly developed integrated circuitry, with the highest component density, found at present in a sound receiver. A less exciting but important function performed by the i.c. is as a power supply regulator-a vital role in v.h.f. receivers incorporating varicapacitance diode (truly electronic) tuning.

The completely integrated high quality receiver will emerge eventually; whether as a single chip, or as a set of two or three i.c.s each covering a major portion of the system, only the i.c. and set designers and manufacturers will have a clue at this moment in time. While awaiting the inevitable, the ultimate in integration, set makers have in recent years been employing several methods. One popular approach is a different form of integration-using pre-adjusted circuit modules, containing conventional discretes. Mass production of complex receivers is thus greatly simplified and the need for critical alignment operations on the assembly line eliminated.

This approach has obvious attractions for the home constructor, especially where a complicated and highly sensitive piece of equipment such as a stereo tuner is concerned. This month's design illustrates the use of modules, i.c.s, and discrete components. Thus as a system it is interesting and instructive. It demonstrates how available circuit devices can be judiciously co-ordinated to produce a "state of the art design" for the modestly equipped home constructor--F.E.B.

## Editor

F. E. BENNETT

## Editorial

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UP To recent times the only methods of tuning radios were either the variable capacitor or the variable inductor. Using either system the result was the same. mechanics in the form of pulleys and pointers were needed to physically move either the vanes of the capacitor or the core of the inductor. Any constructor who attempted to build such a radio faced not only these mechanical problems but also the problem of alignment, particularly difficult in v.h.f. radios.
Two new tuner modules recently produced by Mullard go a long way to overcoming all these difficulties; they are pre-aligned and the tuning is electronic, not mechanical, i.e. there are no moving parts.

## VARICAP TUNING

The tuner module uses a "varicap" diode for varying the tuning frequency. A varicap diode is one which takes advantage of the fact that the width of the depletion layer in a reverse biased diode varies with the reverse voltage. Thus one is effectively changing the gap between two plates of a
capacitor. The capacitances involved are small and thus at the moment varicap tuning is restricted to v.h.f. tuners.

In the Mullard LP1186 module the tuning is carried out by applying a voltage between 2 and 17 volts to its input. Because the tuning is electronic this opens up a whole field of possibilities, in particular that of remote tuning.

## THE MODULES

The tuner module type LP 1186 has three stages, a tuned aerial and r.f. stage, giving good image and i.f. rejection, a separate oscillator stage for good signal handling, and a mixer stage with a doubletuned i.f. output circuit. The main characteristics of this module are shown in Table 1.
The LP1 185 is an f.m.-i.f. amplifier module whose main characteristics are summarised in Table 2. Both modules require a supply voltage of 9 V and this is also adequate to cover the broadcast band when applied to the varicap diode.

[^8]Only a few components are needed around the modules for decoupling and de-emphasis. Automatic frequency control (a.f.c.) is available though this may be removed by shorting to ground when tuning weak stations.

## STEREO DECODER

An MC1310P integrated circuit stereo decoder is used to split the output of the LP1 185 into right and left channel signals. The integrated circuit has the advantage over some of the earlier types in that it needs no coils. It has automatic stereo switching and an indicator driver capable of driving a 60 mA bulb. A light emitting diode (l.e.d.) is shown in the circuit together with a resistor necessary to drop the voltage to the 1.5 V needed for an l.e.d.

Table 3 gives some of the data on the i.c. stereo decoder.

## CIRCUIT DIAGRAM

The full circuit diagram excluding the tuning unit and the power supply are shown in Fig. 1. The input from the aerial is fed into pin $B$ of the tuner module. The tuning voltage is applied to pin C. Capacitor Cl is only really necessary if there is a large separation between the tuning unit and the tuner and may be omitted. A.F.C. is taken from pin $F$ of the output module and fed back to pin $D$ of the tuner. Switch $S 1$ removes this a.f.c. by shorting to earth.

The signal is then fed into pin 2 of the stereo decoder. Dl is the stereo indicator lamp. VRI is used to adjust the frequency of voltage controlled oscillator which forms part of the stereo decoder.

Components C9, R4, C10, R5 are de-emphasis components needed to compensate for the preemphasis of the high frequency signals which is introduced at the transmission end.

Output is taken to the DIN output socket via Cll and Cl 2 .

Table 1 :
SUMMARY OF THE CHARACTERISTICS
OF THE LP1186 F.M. TUNER MODULE

| Tuning range | 87.4 to 104.5 MHz |
| :--- | :--- |
| Tuning voltage | 2 to 12 V |
| Bandwidth at -3 dB points | 300 kHz |
| Aerial impedance | $75 \Omega$ |
| Power gain $\left(f_{i n}=95 \mathrm{MHz}\right)$ | 30 dB |
| Noise factor $\left(f_{\text {in }}=95 \mathrm{MHz}\right)$ | 6.5 dB |

Table 2:
SUMMARY OF THE CHARACTERISTICS OF THE LP1185 F.M.-I.F. AMPLIFIER MODULE
$\left.\begin{array}{ll}\hline \begin{array}{l}\text { Centre frequency } \\ \text { I.F. bandwidth at }-3 \mathrm{~dB} \\ \text { points }\end{array} & 10.7 \mathrm{MHz} \pm .50 \mathrm{kHz} \\ \text { Sensitivity for } 40 \mathrm{mV} \text { output } & 250 \mathrm{kHz} \\ & 300 \mu \mathrm{~V}(\mathrm{~min}) 60 \mu \mathrm{~V} \\ (\mathrm{max})\end{array}\right)$

Table 3:
SUMMARY OF THE CHARACTERISTICS OF THE MC1310P STEREO DECODER I.C.

| Maximum input signal | 500 mV r.m.s. |
| :--- | :--- |
| Pilot capture range | $\pm 3 \%$ |
| Distortion | $00.3 \%$ |
| Maximum <br> current |  |

## POWER SUPPLY

In a varicap tuner the power supply is very important as the tuning voltage must be very stable and ripple free. The power supply circuit is shown in Fig. 2.


Fig. 1. Circuit diagram of the stereo tuner. The shaded boxes indicate ready built pre-aligned units
The tuning voltage unit is shown in Fig. 3


Photograph of the complete tuner showing the front panel layout
The low voltage from the transformer is rectified by the diode bridge D2-5, smoothed by the large capacitor C13 and applied to the input of the integrated circuit regulator IC2. VR2 is used to tap off a fraction of the output voltage to feed back into the input of the i.c. Here it is compared with a reference voltage generated within the i.c. and the output is adjusted to make the two equal. Thus VR2 can be used to accurately set the output voltage.

The i.c. used will keep the output voltage to within 0.2 per cent of the nominal voltage for loads up to 100 mA and within 0.03 per cent of nominal for power supply variations, provided that there is more than three volts between input and output. Because this i.c. also supplies the stereo decoder and hence the stereo indicator lamp it is best to keep the lamp current as low as possible hence the use of an l.e.d.

## TUNING UNIT

As mentioned earlier, a tuning voltage of between two and nine volts will adequately cover the normal broadcast band. A suggested switching system is shown in Fig. 3. This system gives two preset stations and one manually variable setting. The number of preset stations may be extended ad infinitum depending only on the number of push buttons in the unit.

The circuit board shown will accommodate six preset potentiometers. Thus a six-button unit or a six-way rotary switch can be used.

Padding resistors are added at either end of the potentiometers so that fine tuning is easier, although this somewhat restricts the tuning range. Fig. 4 shows the relationship between tuning voltage and frequency and this allows calculations to be carried out on the best settings for each station. The padding resistors are mounted with the potentiometers forming small pillars.

## CONSTRUCTION

Construction is simple if the printed circuit board (Fig. 5) or the layout recommended are followed. Note that the orientation of the i.c.s is critical, a small spot indicates pin 1. Assemble the power supply components first (Fig. 6). Set VR2 to midway then switch on and test the output with a voltmeter, adjusting VR2 to give a 9 V output.


Fig. 2. Circuit diagram of the power supply unit. This not only supplies power to the modules but also provides the stabilised voltage necessary for tuning


Fig. 3. A suggested tuning unit. This provides two preset voltages with a third manually variable voltage. The number of preset voltages really only depends on the size of the push button unit. There is also no reason why this tuning unit should not be mounted remote from the tuner itself. S3 is simply used to cancel the other two switches


Fig. 4. Relationship between the tuning voltage and the frequency as measured in the prototype


## COMPONENTS . . .

## Resistors

| R1 | 150S | R4 | $3.9 \mathrm{k} \Omega$ | R7 | 8.2k $\Omega$ | R10, R13 | $8.2 \mathrm{k} \Omega$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R2 | $15 \mathrm{k} \Omega$ | R5 | $3.9 \mathrm{k} \Omega$ | R8 | $5.6 \mathrm{k} \Omega$ | R11, R14 | 5.6 k |
| R3 | $1 \mathrm{k} \Omega$ | R6 | $560 \Omega$ | R9 | $100 \Omega$ | R12 | 100 S |

## Potentiometers

| VR1 |  |  |  |
| :---: | :---: | :---: | :---: |
| VR2 | $5 \mathrm{k} \Omega$ skeleton preset $10 \mathrm{k} \Omega$ skeleton preset |  |  |
| VR3, | $10 \mathrm{k} \Omega$ skeleton preset ( 2 off) |  |  |
| VR5 | 10k! carbon linear |  |  |
| Capacitors |  |  |  |
| C1 | $0.1 \mu \mathrm{~F}$ | C8 | $2.2 \mu \mathrm{~F} 64 \mathrm{~V}$ elect. |
| C2 | $25 \mu \mathrm{~F} 12 \mathrm{~V}$ elect. | C9 | $0.015 \mu \mathrm{~F}$ |
| C3 | 470pF 2\% | C10 | $0.015 \mu \mathrm{~F}$ |
| C4 | $0.22 \mu \mathrm{~F}$ | C11 | $22 \mu \mathrm{~F} 25 \mathrm{~V}$ elect. |
| C5 | $0.47 \mu \mathrm{~F}$ | C12 | $22 \mu \mathrm{~F} 25 \mathrm{~V}$ elect. |
| C6 | $0.22 \mu \mathrm{~F}$ | C13 | $2,000 \mu \mathrm{~F} 25 \mathrm{~V}$ elect. |
| C7 | $0.047 \mu \mathrm{~F}$ | C14 | $10 \mu \mathrm{~F} 16 \mathrm{~V}$ elect. |

## Diodes

D1 Light emitting dio de 1.5 V 20 mA (West Hyde)
D2-5 W005 or any 50 p.i.v. $\frac{\frac{1}{2}}{}$ A bridge rectifier
Integrated Circuits
IC1 Motorola MC1310P
IC2 Motorola MFC4060

Fig. 5. The underside of the printed circuit board. The black areas indicate copper, the white areas being etched away

## Transformer

T1 Mains primary, 12 V 100 mA secondary

## Modules

Tuner Module Mullard Type LP1186
I.F. Module Mullard Type LP1185

## Switches

S1 Miniature rocker or slide on/off switch
S2 Miniature d.p.d.t. toggle switch
S3-5 3 way pushbutton unit, each switch cancelling the other two

Miscellaneous
FS1 100 mA fuse and fuseholder
SK1 Coaxial socket
SK2 5 pin $180^{\circ}$ DIN socket, panel mounting
LP1 Mains neon indicator with integral resistor
PL1 Mains panel mounting plug Bulgin type P360
3 -way tag strip, printed circuit board, case, 6BA and 8BA nuts and bolts

Printed circuit board and modules can be obtained from B \& B Electronics, 64 Manners Road, Balderton, Newark, Notts.

After checking the power supply attach the other components. Note the link between the cases of the two modules. Do not attach C8 at this stage. Push button units vary as to the type of contact arrangement. If you are not sure use a continuity tester, e.g. a battery and bell or lamp to find two contacts which make when the appropriate button is pressed

As mentioned before there is no reason why the push button units should not be mounted remote from the tuner

## SETTING UP AND TESTING

Prior to testing and final setting up. ensure that a good aerial is available and also an amplifier for monitoring. A v.h.f. aerial will be needed for low noise stereo although a v.h.f. television aerial or a length of wire will suffice for initial checks.

Before setting up is explained, some description of the stereo decoder is useful to understand what is going on. Fig. 7 shows a block diagram of the stereo decoder i.c.

The audio input is buffered and separated from the 19 kHz pilot tone which is fed to two modulators which act as phase discriminators; modulator 1 is the input to the phase locking loop and modulator 2 is used as the stereo detector and indicator. Each provide an output which is proportional to the phase difference between the pilot input and the regenerated 19 kHz signal (TP1). The output from modulator 1 controls the frequency of a 76 kHz oscillator which is then divided by two to give a 38 kHz signal necessary for decoding. The regenerated 38 kHz is divided by two to give 19 kHz which is fed back to the modulators, forming part of the phase locked loop.
If this regenerated 19 kHz differs in phase from the 19 kHz pilot then the modulator will correct the 76 kHz oscillator thus locking it to the pilot tone. The resultant output from modulator 2 triggers a Schmitt trigger which switches on the stereo indicator and feeds the regenerated 38 kHz to the decoder. With mono transmissions the audio comes out of the decoder outputs simultaneously, no pilot tone being present

INTERWIRING



Fig. 7. Block diagram of the MC1310P stereo decoder i.r

## OSCILLATOR ADJUSTMENT

There are two ways to set VRI, the object being to set the oscillator to 76 kHz with no pilot or input signal.

Connect the tuner to an aerial and an amplifier with C8 in position on the board, then switch on. It should be possible to tune into a station at least in mono (ignore the indicator lamp if it should come on). Switch off the a.f.c. and tune slightly away from the station, then switch back to a.f.c.; the station should pull in, if the signal is strong. Leave the a.f.c. on and tune to a known stereo broadcast. Rotate VRI until the stereo indicator just lights and a stereo output is heard. There will probably be a good deal of background noise especially with a poor aerial.

If an oscilloscope is available monitor TP1 with the tuner locked onto a station. Remove the input signal and reset the frequency to this measured value.

An atternative method of setting up is to reduce the signal level to the decoder thus reducing the range of VRI. Connect the positive end of C8 to the board but connect a 10 kilohm potentiometer between its negative end and the LP 1185 output (see Fig. la). Switch on and tune to a stereo broadcast then adjust this potentiometer to give maximum audio output. Adjust VRI until the stereo indicator lights then alternately reduce the output with the potentiometer and adjust VR1 until the setting of VR1 is very sharp or critical, this being the correct setting.


Photograph of the internal layout of the tuner


A new Integrated Circuit, the 555, provides the main circuit elements of a timing unit suited to application in the home, darkroom, workshop or factory. Covering delay times from milliseconds to hours, the 555 may in addition be used for pulse modulation or as an oscillator or in other applications. The device in its various guises is discussed in detail so that the constructor may design his own circuits. In addition, this issue includes a constructional feature on a timer using the 555 .

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## PRACTICAL <br> EAECTRONIES

## CONCLUDING ARTICLE



THas final part of the Digi-Cal series describes the rematining logic housed on the underchassis overflow (ovF) board, and attempts to knit together the loose ends which have been left dangling in earlier articles. Testing and troubleshooting information is also given.

## OVERFLOW (OVF) BOARD

The existence of the oVERILow board wals established in Part 2. when it was mentioned that this board is mounted copper side uppermost under the chassis. spaced from it by two 6BA nuts on each of the supporting bolts.

The ove identity was not given to this board in Part 2 but is used here for ease of reference, the majority of the logic housed on this board being concerned with the overfeow circuitry.

The Veroboard panel itself is mounted in the copper up fashion to facilitate the use of this board as an interconnection and power bus medium in
addition to its job of housing logic. This mounting method also permits the easy addition of circuitry without access to the underside of the board, the only compromise necessary being that of neatness, since the solder is "on display" together with the components.

## INTERCONNECTIONS

The ovF board carries the +5 V and ground line power buses, from which the other logic cards are supplied. Any other logic lines which are employed, e.g. the functron code a and bare also allocated a copper strip for bus use to permit a tapping to be made where required.

Programme functions are distributed from the Ove board by means of a series of terminal pins which act as distribution points, the decision as to which functions require this treatment being left to the individual constructor as layouts will undoubtedly vary.

## OVERFLOW LOGIC

The oVERFLOW logic is required to detect and indicate any errors resulting from the incorrect operation of the calculator, indication being provided via the red ovF lamp on the keyboard. If this lamp comes on at all during a calculation then an improper operation has been attempted and the only course open is to depress the clear key which also resets the oVF circuits.

There are several ways in which an error condition can occur, an error being a state which would result in an incorrect answer being given. Detection of these states requires a combination of three separate logic groups whose areas of responsibility are as follows:
(a) ENTRY OVERFLOW. If too many digits are entered into the e register, the most significant data can be destroyed by being shifted out of the end of the register. This condition must be detected.
(b) a register overflow. If during a multiplication sequence, the product exceeds the capacity of the a register then the carry store will stay set at the end of an addition which is an indication of OVERflow.
(c) answer overflow. The Digi-Cal a register has a ten digit capacity although only eight digits are displayed, the other two positions in the register being for transient use during programme execution. Should either of these two positions contain other than zeros at the end of a programme sequence then an overflow has occurred.

This type of OVERFLOW can occur during adDITION, multiplication and when a negative answer is produced in complement form.

## OVF CIRCUITS

The active circuitry of the ovF board is shown in Fig. 11.1, where it can be seen that in addition to the ovF logic proper, IC141 and IC146 perform the functions of constant store buffering and $\mathrm{E}^{2}$ gating respectively.

Bistable BS2 of IC144 acts as the common ovF latch, which is set by an output from any of the three separate overflow detection circuits, and which controls the OVF lamp driver on the KEYBOARD logic board. The ovF latch is cleared when the clear key is depressed in response to an ovf indication.

The NOR section of IC145 which is a four-wide two-input AND-OR-INVERT gate combines the inputs from three detection circuits to drive the BS2 PRESET input, an output from any of the three resulting in a SET Latch signal.

## ENTRY OVERFLOW LOGIC

IC142 and G1 of IC143 are used to detect E REGISTER overflows. The system used here to monitor the B.C.D. outputs of the most significant digit position of the register with IC142, which, in this application, can be considered as a four-input positive NOR gate with a common disable input.

The output of IC142 is gated with the E CLOCK to generate the OVF output when necessary.

Gate IC142 is in fact waiting for one or more of its inputs to go to a logic 1, indicating that the most significant digit of the E REGISTER contains other than decimal zero.

On the arrival of a further clock pulse an error output is generated to set the latch.

A problem arises here since by using the straightforward e clock an error output would be produced one step too early. What is really needed is an E clock "pre-pulse" which comes and goes before the register itself is clocked. At first sight this is an impossible requirement to meet; however, by using the inherent propagation delays of the gates involved, such an arrangement can be achieved.

What happens is that when a B.C.D. output other than zero appears in the most significant position of the register a 1 input to pin 9 of IC 145 results.

Much later, when another number key is pressed the rising e clock on IC 145 , pin 10 will result in an error output to pin 8 , setting the latch. Even before the clock rises on pin 10, the unbuffered e clock operates the common disable input connected to pins 1, 3, 5 and 9 of IC142 removing the 1 input to IC145, pin 9.

The result at the output of IC145 is an extremely narrow pulse which in practice could be too narrow to set the latch BS2. The way to stretch this pulse is to increase the propagation delay through IC142 and G1 of IC143, and this can be conveniently achieved by increasing the capacitive load on the output of IC142.

A capacitor $C_{x}$ is shown on the diagram and can be added if the error output is found to be too short on test; the value used should be between 200 pF and 1.000 pF .

No such capacitor was necessary on the prototype.

## A REGISTER OVERFLOW LOGIC

The operation of the a REGISTER detection logic is quite straightforward; in this case the task is simply to detect the presence of a stored carry at the end of ten clock pulses during a multiplication or addition.

The rising edge of the END OF TEN output from board CB triggers a monostable made up of BSI of IC144 and G2 of IC143. The indication that the clock sequence is at an end is gated with the carry sense output from board AD, in G3.

The output of G3 is gated with an inverted FUNCTION CODE $A$ (which is an indication of the arithmetic operation being performed) in the AND section of IC145 to produce the ERROR output at pin 8.

## ANSWER OVERFLOW LOGIC

Detecting an integer in the two most significant A REGISTER positions seems on the face of it to be quite straightforward, but in practice such considerations as lack of space on the a boards to install i.c. gates, and lack of edge contacts on the a boards to allow external i.c. gates pose some problems.

The only practical solution is to construct a special gate using discrete components which operates as a positive logic Nor. This design requires only the installation of four diodes. and the utilisation of only one edge contact on each a board.

The problem of the low logic 1 levels associated with TTL outputs is overcome by clamping the emitter of TR22 of the gate to about $\frac{1}{2} V_{\text {ce }}$, and using TR23 to regenerate suitable logic levels to interface with IC145 pin 13.

Pin 1 of IC145 gates the ERROR output from the discrete component gate with what is effectively an end of programme signal (display a) so that valid transient outputs from TR23 during programme execution have no effect on the OVF latch.

## OVF BOARD



Fig. 11.1. Circuit diagram of the various units contained on the OVF board

## DIVIDE OVERFLOW

No logic has been included to show that an oVERFLOW during a division operation has occurred.

Logic to fulfil this function would be simple to design and could use pins 4 and 5 of IC145 as an access to the oVf latch, but this was not carried out on the prototype because a divide overflow is very obvious to the operator by virtue of the fact that no answer is produced on the display.

## E SQUARED GATING

It was only after the component location stage of Digi-Cal design that it was realised that the addition of a very few gates could produce an automatic $E^{2}$ facility to complement the basic arithmetic functions.

The gating required is so simple that the incorporation on the OVF board is quite straightforward.

The object of the three gates shown in Fig. 11.1 as part of IC146 is to divert the $A$ to $Z$ transfer command from the programme to the e to $z$ buffer gate when the $\mathrm{E}^{2}$ latch on the programme board is set.

This simple operation causes the multiply programme to multiply the number in the e REGISTER by itself. The normal command to transfer the A REGISTER contents to the $z$ REGISTER is blocked and the $E$ to $Z$ transfer substituted, resulting in the number e being both multiplier and multiplicand.

## CONSTANT STORE BUFFERS

IC141 is an SN7440 buffer gate which is interposed between the keyboard outputs and the constant store to provide the drive and inversion

## OVF LOGIC CONSTRUCTION

Although the $E^{2}$ logic and the constant store buffers will have to be wired up before the testing stage, it is best to leave the ovF detection logic until the calculator is operating correctly. Connecting up these circuits before proper operation is realised could lead to confusion.

Having both the i.c.s and the wiring on the copper side of the board takes a little getting used to when soldering, but there are no special problems to look out for, and circuit tracing is really much easier. The board layout is shown in Fig. 11.2, and mounting position in Fig. 11.3.

## OVERALL TESTING

It would be a very optimistic constructor indeed who wired up the whole Digi-Cal, switched on, and expected it to work perfectly first time.

There will no doubt be wiring errors, perhaps a faulty i.c. (there were three in the prototype), and a dry joint or two.

The policy of piecemeal testing suggested in previous parts will undoubtedly have eliminated most



Fig. 11.2. Construction of the OVF 'board. Note that both the wiring and components are placed on the copper strip side of the Veroboard panel

\section*{COMPOUENTS <br> | Resistors |  |
| :---: | :--- |
| R74 | $4.7 \mathrm{k} \Omega$ |
| R75 | $1.5 \mathrm{k} \Omega$ |
| R76 | $150 \Omega$ |
| R77 | $150 \Omega$ |
| R78 | $4.7 \mathrm{k} \Omega$ |
| R79 | $1.5 \mathrm{k} \Omega$ |}

## OVF BOARD

## Capacitors

C51 $10 \mu \mathrm{~F} 15 \mathrm{~V}$ elect.
C52 $0.047 \mu \mathrm{~F}$
$\mathrm{C}_{\mathrm{x}}$ (see text)

## Diodes <br> D143-150 West Hyde type "red" or any small silicon diode (8 off)

Transistors

Integrated Circuits
IC141 SN7440
IC142 SN7453
IC143 SN7402
IC144 SN7476
IC145 SN7453
IC146 SN7400

## Miscellaneous

11 in $\times 3.6$ in $\times 0.1$ in matrix Veroboard panel
faults, and certainly the constructor who has reached the final testing stage, which basically involves making the programmes work as required, will be sure that all the boards are fundamentally serviceable.

The first hurdle to be cleared is the correct operation of the ADD/subtract programme and when this has been achieved (with a slow clock speed if desired) the bulk of the arithmetic section can be given a clean bill of health.

The multiply and divide programmes can then be tackeld in turn and if any problems are encountered a thorough understanding of the way the calculator should be operating will soon sort these out.

It cannot be stressed enough that after gathering evidence via a multimeter and display, the best strategy in solving a problem is to sit down with a paper and pencil and ponder the possible causes: aimless probing will get you nowhere.

## CLOCK SPEED

The ultimate objective of the testing phase is to increase the clock speed to as high a rate as possible while maintaining correct operation.

In the prototype a speed of over 1 MHz was obtained despite the far from ideal underchassis "bird's nest" wiring resulting from prototype modifications.

Constructors should be able to do better than this easily since all improvements have been incorporated in the published designs and any advance achieved in this respect will be rewarded by a shorter maximum multiplication time, important when operating near to the maximum capacity of the machine.


Fig. 11.3. The OVF board is mounted on the underside of the chassis in the four holes marked " $A$ " in the main chassis plate

Corrections. We apologise for these errors which occurred during the course of Digi-Cal articles.

Part 3, Fig. 3.2. Capacitors C3, C4, C5 and C6 should be connected between +5 V and GND, not as shown. The strobe outputs from IC7 are reversed, i.e. pin 12 should be strobe 8 and pin 4 should be strobe 1.

Part 4, Fig. 4.2. Switch $S 19$ is shown twice, the K switch should be S5. S13 is shown twice, the Decimal Point switch should be S3. Both are shown correctly on Fig. 4.5. The diode labelled D103 on IC26 should be D101.

Part 5, Fig. 5.8. The $K$ switch should be labelled Recall K output.

Part 6, Fig. 6.10. Connection from the $Z 1$ and $Z 2$ sockets to the E1, E2 and E3 boards show the pin numbers incorrectly. Correct destinations can be found by adding 22 to each of the pin numbers associated with the $E$ boards, e.g. $\mathrm{Z} 1 / 1$ should go to E3/31. Also $Z 1 / 19$ should go to $A D / 41$, and $\mathrm{Z} 1 / 20$ to $A D / 42$. $Z 2 / 19$ goes to AD/39; Z2/20 to AD/40, not as shown. Z2/44 should go to Z1/42 and Z2/42.

A1/1 should go to AD/27; A1/10 to AD/31; A1/11 to AD/32.

A2/1 should go to AD/25; A2/10 to $A D / 29 ; A 2 / 11$ to $A D / 30$.

Fig. 6.7. CP in IC 77 and 78 should go to pin 3 not 2.

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| $\pm$ | 5\% | $47 \Omega-1 \mathrm{M} \Omega$ | E12 | Ip | ${ }^{0.8 p}$ |
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$1.5 \mu \mathrm{~F}, 20 \mathrm{p} .22 \mu \mathrm{~F}, 24 \mathrm{p}$. $1.5 \mu \mathrm{~F}, 20 \mathrm{p} .22 \mu \mathrm{~F}, 24 \mathrm{p}$
MYLAR FILM CAPACITORS IOOV $\begin{array}{llll}0.001 \mu \mathrm{~F}, & 0.002 \mu \mathrm{~F}, & 0.005 \mu \mathrm{~F}, & 0.01 \mu \mathrm{~F}, \\ 2 \frac{1}{3} \mathrm{p}, & 0.04 \mu \mathrm{~F}, 0.05 \mu \mathrm{~F}, 0068 \mu \mathrm{~F}, 0.1 \mu \mathrm{~F}, & 3 \frac{1}{3} \mathrm{p} .\end{array}$

CERAMIC DISC CAPACITORS
100pF to 10,000 pF, 2p each

ELECTROLYTIC CAPACITORS—MULLARD OI5/6/7 RANGE REPLACES C426 C457 RANGES
( 1 F/v) $1 \cdot 0 / 63,1.5 / 63,22 / 63,3.3 / 63.4 \cdot 7 / 63,6 \cdot 8 / 40,10 / 25,10 / 63.15 / 16.15 / 40,15 / 63$ $22 / 10.22 / 25,22 / 63,33 / 6 \cdot 3,33 / 40,47 / 4,47 / 10,47 / 25,47 / 40,47 / 63,68 / 6 \cdot 3,68 / 16,100 / 4$ $100 / 10,100 / 25,100 / 40,150 / 6.3,150 / 16$. $150 / 25,220 / 4,220 / 10,220 / 16,330 / 4,330 / 10$ $\begin{array}{lll}470 / 6 \cdot 3.5 p & \text { each. } 68 / 63.150 / 40,220 / 25,330 / 16,470 / 10,680 / 6 \cdot 3,1,000 / 4,9 p & 100 / 63\end{array}$ $150 / 63,220 / 40,470 / 25,680 / 16,1.000 / 10.1,500 / 6 \cdot 3$. $12 p . \quad 220 / 63.470 / 40,680 / 25$ $1,000 / 16,1,500 / 10,12,200 / 6 \cdot 3,15 p .330 / 63,680 / 40,1,000 / 25,1,500 / 16,2,200 / 10$
$3,300 / 6 \cdot 3,4,700 / 4,18 p$.
SOLID TANTALUM BEAD CAPACITORS

| SOLID TANTA 0.1 0.22 0.47 10 | $\begin{aligned} & \text { ALUI } \\ & 1 \mu \mathrm{~F} \\ & 2 \mu \mathrm{~F} \\ & 7 \mu \mathrm{~F} \\ & 0 \mu \mathrm{~F} \\ & \hline \end{aligned}$ |  | APACITORS  <br> $2.2 \mu \mathrm{~F}$ 35 V <br> $4.7 \mu \mathrm{~F}$ 35 V <br> $6.8 \mu \mathrm{~F}$ 25 V <br> $10 \mu \mathrm{~F}$ 25 V |  | $\begin{array}{r} 22 \mu \mathrm{~F} \\ 33 \mu \mathrm{~F} \\ 47 \mu \mathrm{~F} \\ 100 \mu \mathrm{~F} \end{array}$ | $\begin{array}{r} 16 \mathrm{~V} \\ 10 \mathrm{~V} \\ 6.3 \mathrm{~V} \\ 3 \end{array}$ | 12p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| VEROBOARD |  |  | JACK PLUGS AND SOCKETS |  |  |  |  |
|  | 0.1 | 0.15 | Standard screened Standard insulated Stereo screened Standard socket Stereo socket | 18p 2.5 mm insulated |  |  | ${ }^{8 p}$ |
|  | 22p | $16 p$ |  |  | 3.5 mm | insulated |  |
|  | 24p | 24p |  |  | 3.5 mm | screened | 13 p |
|  | 24 p | 24 p |  |  | 2.5 mm | socket | 8 p |
|  | ${ }^{275}$ | 27p |  | $18 p$ | 3.5 mr | socket | 8 p |
| $17 \times 2 \frac{1}{2}$ | 75p | 57 ${ }^{\text {pp }}$ |  |  | , | socket | p |
| $17 \times 3 \frac{1}{4}$ | 100p | 78p | D.I.N. PLUGS A | ID S | CKE |  |  |
| $17 \times 5$ (plain) | . | 82 p | 2 pin, 3 pin, 5 pin | $0^{\circ}, 5$ | pin 240 | , 6 pI |  |
| $17 \times 3$ (plain) | - | 60p | Plug 12p. Socket | 8p. |  |  |  |
| $17 \times 2 \frac{1}{2}$ (plain) | - | 42 p | 4 way screened cab |  |  |  |  |
| $2 \frac{1}{2} \times 5$ (plain) | - | 12p | 6 way screened cab | , 22p | metre |  |  |
| $2 \frac{1}{2} \times 3 \frac{3}{4}$ (plain) | - | $11 p$ |  |  |  |  |  |
| Pin insertion tool | 52p | 52p |  |  |  |  |  |
| Spot face cutter | 42p | 42 p | BATTERY ELIM | NAT | OR |  | 150 |
| Pkt. 50 pins | 20p | 20p | 9 V mains power sup | ply. | Same | as PP9 |  |

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# THE EMI SCANNER <br> BRAIN RAY <br> A NEW COMPUTERISED 

by K. R. HILL

THE EMI-Scanner is a computerised X-ray transverse axial tomography system using new techniques invented in the Central Research Laboratories of EMI Ltd. It has been developed by EMI in conjunction with Department of Health and Social Security after a four year research and development programme.

The equipment is able to produce pictures of cross sectional slices of the human brain. The basic system consists of a number of units:

1. The Scanning Unit which scans the patient with X-rays to produce a series of intensity output readings.
2. The X-ray Control Unit which controls the $X$-rays and the operation of the Scanning Unit.
3. The Computer Unit which stores and processes the data.
4. The Viewing Unit which displays the results on a cathode ray tube screen.
5. The X-ray generating system.

## THE BASIC PROBLEM

The conventional X-ray photograph taken of the human body suffers from a serious drawback in that it is attempting to portray a three-dimensional object on a two-dimensional photographic plate. The X-ray picture indicates the X-ray intensity after it has passed through the object being examined. Typically the X-rays will have passed through bone, tissue, fat, blood. etc. and the resulting picture produced will be confused due to the superimposition of the various materials. Frequently the diagnostician is attempting to detect a small variation in the X-ray absorption of tissue (which may indicate some abnormality such as a tumour) when the area of interest is masked by a nearby bone. This situation is shown in Fig. 1.

The human brain poses a considerable problem for radiologists because it is totally enclosed in the protective bone of the skull. In an attempt to overcome some of the limitations of the conventional skull X-ray, several more sophisticated techniques have been developed such as angiography, ventriculography, and radioactive isotope brain scanning. These techniques, while giving some improvement in diagnoses, can cause considerable discomfort to the patient as well as in some cases requiring a team of highly trained staff to perform them. In addition to this the patient may need to be hospitalised after examination.


THE MACROBERT AWARD
For the invention of a new $X$-ray technique, Mr Godfrey Hounsfield and EMI Limited won the 1972 MacRobert Award.
This Award, often described as the Nobel Prize for engineering, consists of a Gold Medal and $\{25,000$ prize money. It is presented annually, in recognition of the technological innovation contributing most significantly to the prestige and prosperity of the United Kingdom.

It was instituted by the MacRobert Trusts in 1968 and is administered by the council of Engineering Institutes, which is the federal body for 15 chartered engineering institutes.

This is the first time the award has been made in the field of electronics. In his citation for the Award, the Chairman of the MacRobert Award Evaluation Committee said, "One of the medical referees consulted during the evaluation stated that no comparable discovery has been made in this field since Röntgen discovered $X$-rays in 1895, and we agree with him.
"The EMI-Scanner system developed by Mr Hounsfield within the Central Research Laboratories of EMI is epoch-making, because it breaks away from the photographic techniques for recording $X$-ray pictures which in principle have remained unchanged since Röntgen's day
"There is another aspect of EMI-Scanner which is remarkable. In these modern days it is rarely that one finds great developments which are the work of one man. The EMI-Scanner is different: the submission for the MacRobert Award was prepared not by the inventor, but by EMI, who stated, 'Mr Hounsfield has been the guiding expert throughout all aspects of the work. The EMI-Scanner was as much a one-man invention as anything can be these days'.'

## THE NEW TECHNIQUE

The EMI-Scanner offers considerable advantages to both the diagnostician and the patient.

This new system uses X-rays to produce pictures of slices of the head as shown in Fig. 2. The head of the patient rests in a rubber head cap, and a gantry, on which is mounted the X-ray tube and detectors, is able to rotate around the head to perform the scanning sequence shown in Fig. 3. With the gantry in the $0^{\circ}$ start position, the X-ray tube and detectors move so as to make a linear pass of the head. The whole gantry then rotates $1^{\circ}$ and the X-ray tube and detectors move back to make a further linear pass.

The gantry then rotates a further $1^{\circ}$ and this sequence of linear passes and $1^{\circ}$ rotations is repeated until a total rotation of $180^{\circ}$ has been achieved. Each complete scan does in fact yield results for two contiguous slices of the head as shown in Fig. 4. The thickness of each slice can be adjusted to either 0.8 cm or 1.3 cm by means of collimators in the X-ray beam. The two pictures from a single patient scan are achieved by using two detectors each with its own associated data processing channel.

The X-ray detectors used are photomultipliers with sodium iodide scintillating crystals. During each linear pass of the head, 160 readings of X-ray intensity are made by each detector so that for each complete scan of $180^{\circ}$ a total of $180 \times 160=28,800$ readings are taken. The 160 readings are controlled by means of a glass grating consisting of alternately transparent and opaque sections. This grating moves with the X-ray tube and detectors, and passes between a lamp and photodiode. The output from this photodiode controls the operation of electronic circuits which measure the output of each detector.

For each complete scan the scanning system yields a set of 28,800 readings from each of the two detectors plus an additional set of 28,800 reference readings of the X-ray intensity before passing through the patient's head. These three sets of readings are put into digital form by an analogue to digital converter and stored in the buffer section of. a magnetic disc pack. This is illustrated in the block diagram of the system Fig. 5.

## DATA PROCESSING

These readings of X-ray intensity now have to be used to solve many thousands of simultaneous equations so that the X -ray absorption value at each point in the slice can be calculated. This operation is performed by a mini-computer, which, by means of a specially written computer program, is able to call-up these readings from the disc store and process them. The computation, which takes about five minutes for each picture, results in 6,400 output values in digital form which are stored in the main storage section of the magnetic disc pack.

## PICTURE DISPLAY

The 6,400 digital values can be called-up on command and converted into analogue form where they may be used to build up a picture on the cathode ray tube screen of the Viewing Unit. This picture consists of a matrix of $80 \times 80$ picture points, the brightness of each point representing the X -ray absorption of the tissue.



An alternative method of displaying the results is to use a line printer which will print out the numerical values of the X-ray absorption coefficient at each point of the $80 \times 80$ matrix.

The chart shown in Fig. 6 illustrates the range of measurement of the system. The left-hand scale shows the percentage X-ray absorption coefficient greater or less than that of water and the vertical blocks show the coefficients for materials commonly encountered in clinical radiology, i.e. blood, tissue, bone, etc. The right-hand scale on the chart shows the scale actually used on the equipment, with dense bone at +500 , water at 0 and air at -500 . The system is accurate to within $2 \frac{1}{2}$ units on a range 0 to 500 .

In order that the diagnostician can select the information which is displayed on the Viewing Unit there are two very important controls-window width and window level.

The window width control selects the range of X-ray absorption values which yields black to peak white on the cathode ray tube screen.

The window level control enables this selected band to be moved up or down the scale of absorption values. As an example with the window level

control set at +15 (centre of the band) and the window width set at 20 all tissue with X-ray absorption values less than +5 would appear black and all values greater than +25 would appear white. Values between +5 and +25 would appear of different brightness values between black and peak white.
An illustration showing the effect of the window level control is shown in Fig. 8. The top left-hand picture shows the control set at -50 ; all values less than -60 appear black, all values greater than -40 appear white. The dark ring represents air trapped in the hair of the patient. The top centre picture shows the control set at 0 with the saline fluid-filled ventricles just beginning to show. The top rightand lower left-hand pictures show intermediate settings of the control to show detail of brain tissue $\mathrm{at}+10$ to +20 . The lower right-hand picture shows the control set at +50 with the white ring representing the bone of the skuli. These pictures clearly show that the diagnostician can select the displayed picture to suit the material under examination.

By switching the window width control to a "measure" position, which yields 1 digit black to peak white on the display, it is pussible to measure the X -ray absorption at any chosen point in the picture.



The window level control is adjusted until the point under examination is just changing from black to white. The absorption value can then be read off directly from the window level scale.

## PATIENT PREPARATION

As each complete scan of the patient yields results on only two 1.3 cm thick slices of the head it may be necessary to perform three or four such scans to cover the major part of the brain. If, however, it is desired to locate the examination at a certain point this is done very easily. Firstly an adhesive white tape is fixed over the head' of the patient to form a head-band. This is then marked to show the orbitomeatal line, which is an imaginary line drawn between the corner of the eye and the meatus of the ear, used as a reference point. If for example the diagnostician requires to examine a slice 5 cm above the orbito-meatal line, then a mark is made at this position on the head-band. This is illustrated in Fig. 7.

At this point the patient's head is inserted in the machine and the rubber head cap is collapsed onto the skull by means of water pressure to expel the air. The patient's head within the head cap is located

in a plastic cone on which is printed a scale, and the mark denoting the chosen plane of slice is then read off against this scale. This reading is noted and the patient is then moved either into or out of the machine by means of a hand-wheel beneath the diagnostic table until a pointer and scale indicate the same value as the head cone reading. The patient has then been set in the machine such that a slice either side of the marked plane is examined.

A range of different plastic head cones is available in order to accommodate heads of various sizes and also to allow the head to be tilted for certain special examinations.

Each patient is normally allocated an identifying number which the radiographer can enter into the machine store before each scan by means of thumbwheel switches on the X-ray Control Unit. This number appears on the pictures and print-outs for that scan and so gives a positive link between the patient and the result.

The computer normally processes each set of readings in serial order from the buffer store. However, should the diagnostician require the results from a certain patient quickly, then the computer can be instructed to give priority processing to a selected picture.

## APPLICATIONS

As with any X-ray technique the EMI-Scanner system relies on the fact that the various structures found in the brain must have different X-ray absorption values in order that they can be differentiated. Even though the system is extremely sensitive there may be cases where the use of a contrast medium can be an advantage. Typically a small quantity of an X-ray opaque substance such as iodine can be injected intravenously into the patient.

If for instance there is a lesion which takes up the contrast medium more than the surrounding normal tissue then the diseased area will show up clearly on the picture, and, using the EMI-Scanner system, will continue to do so for several hours. The use of contrast media in this way should be compared with the technique used in angiography where the fluid is injected into the arterial system of the body and the effect lasts for only a few seconds.

Fig. 8 (left). Effect of the "window level" control The Viewing Unit




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View of a patient in position on the scanning unit

## TECHNICAL DETAILS

The circuit techniques used are in general of a conventional nature incorporating both discrete components and integrated circuits mounted on printed circuit boards. Both the Scanning Unit control electronics and the viewing Unit contain a large amount of logic circuitry.

The X-ray Control Unit


A feature of the systent is the high degree to which the various controls are interlocked to ensure safe and correct operation by non-technical operators. As an example of this, the scanning sequence cannot be started until four conditions are satisfied :

1. That the scanning gantry is in the start position.
2. That the operator has set the patient's identifying code on the thumbwheel switches.
3. That the computer is ready to receive data into the disc buffer.
4. That the operator has removed the safety key from the Scanning Unit control panel and has inserted it in the X-ray Control Unit.
The status of these interlocks is clearly shown by means of indicating lamps so that the operator can check visually before starting the sequence.
The system for generating the X -rays is designed to give good stability and incorporates regulators for both voltage and current to the X-ray tube. Threephase a.c. mains is converted to 100 V 150 Hz by a power conversion unit, which is then fed to the e.h.t. transformer. The output voltage is full wave rectified and smoothed to give an output of up to $\pm 70 \mathrm{kV}$ w.r.t. earth for the X-ray tube.

The X-ray tube is a fixed anode type, the cathode being aligned to give a line rather than a spot focus.

## CONCLUSION

This system is being confidently predicted by many radiologists as one which will revolutionise the use of X-rays. The significance of this new technique has already been noted in Great Britain where its inventor, Mr G. N. Hounsfield, of the Central Research Laboratories of EMI Ltd., has recently received the MacRobert Award for outstanding innovation in engineering.

## ACKNOWLEDGEMENT

The writer wishes to thank the Directors of EMI Ltd. for permission to publish this article.

## PES Sound Synthasiser 4 BIIMP CEDERDTDRE: MPOI DMPINEES By G.D.Shaw <br> 

THIS month, the operation and construction of the ramp generators and input amplifiers will be described together with guidelines on using the various modules, so far described, in combination.

## RAMP GENERATOR

The ramp generator to be described is effectively a sawtooth oscillator capable of working down to very low frequencies. At the low end of its working range the output of the device may be considered to be slowly changing d.c. and, unlike the v.c.o. which produces an output waveform swinging about zero. the output of the ramp generator is single-ended, that is, swinging from zero to about -3.5 V .

The reason for this arrangement is that the ramp generator is considered essentially as a device for programming other voltage controlled modules all of which require eontrol voltages of one polarity only. This requirement, incidentally, does not mean that alternating voltages cannot be used for programming and, as will be shown, many interesting effects can be obtained when the control voltages vary about zero.

As with the v.c.o. the principle of operation is that of the linear integrator although the circuit shown in Fig. 4.1 is very much simpler.

ICI is the integrator which receives its positive control voltage either from VR1, an external source, or from both in combination. IC 2 is a comparator which, since single ended operation is required, utilises a reference voltage set by R7-R8 and transistor TRI to discharge the integrating capacitor C1. The reference voltage also determines the peak ramp output voltage of the circuit.

## CIRCUIT OPERATION

The operation of the circuit is as follows. The divider R7/R8 provides -3.5 V at the non-inverting input of IC2 and effectively biases TR1 off. Assuming that the R1 input to $I C 1$ is open circuit, a positive voltage derived from VRI is applied to the inverting input of IC1 via R2 and the integrator begins to ramp negatively at a rate determined essentially by R2/C1

When the ramp output voltage applied to the inverting input of IC2 is equal to or greater than
the reference voltage the comparator switches to its positive saturation state, turns on TR1, and discharges C 1 via R6 and R7.

The sawtooth output waveform is taken from the junction of R4 and R 5 via VR4 while a pulse cutput is available from the emitter of TR1. Note that this requires to be a.c. coupled if it is to be used effectively.

## CONSTRUCTING THE RAMP GENERATORS

Construction of the ramp generators is perfectly straightforward, the recommended circuit board layout being shown in Fig. 4.2. Note that both ramp generators (RG1/RG2) are built on one circuit board and that power supply decoupling is not required.

The method of construction should generally follow that employed for the v.c.o. module. Components should be mounted to the front panel and prewirec before the panel is secured to the circuit board support plate. Note, however, that in this case the main wiring harness from the ramp generators should leave the front panel at the top and pass over the top edge of the circuit boards while the wiring to the input amplifiers should be as short as possible and routed direct to the appropriate circuit board.

A detail of the panel component wiring and board layout is shown in Fig. 4.3. The McMurdo plug should now be prewired and mounted into the support plate.

## TESTING

When assembly of one of the ramp generators has been completed make temporary connections to power supply leads and front panel controls and connect a resistor of at least 10 megohms across the integrating capacitor C1. Set VR2 and VR1 to their minimum values, VR3 to its mid-position, and switch on the power supply. Observe the integrator output on the oscilloscope and adjust VR3 for zero offset. Switch off and remove the 10 megohm resistor.

Set VR2 to its mid-position and switch on again. A sawtooth waveform of about 7 Hz should now be observed. Gradually reduce the setting of VR2 until the slope of the ramp begins to show slight rippling.

## RAMP GENERATORS



Fig. 4.1. Circuit of a ramp generator


Fig. 4.2. Component layout and wiring of ramp generators


Fig. 4.3. Control panel wiring and board layout of ramp generator module. A lead should be taken from SK2(2) to PL12/8

## couporizis <br> RAMP GENERATOR (2 OFF) <br> Resistors <br> R1, R2 $270 \mathrm{k} \Omega$ (2 off) <br> R3 24k $\Omega$ <br> $\begin{array}{ll}\text { R4 } & 47 \Omega \\ \text { R5 }\end{array}$ <br> R6 $\quad 82 \Omega$ <br> R7 $560 \Omega$ <br> R8 $\quad 1.5 \mathrm{k} \Omega$ <br> All $2 \% \frac{1}{2}$ watt metal oxide <br> Capacitors <br> C1 $1 \mu \mathrm{~F}$ polyester 25 V <br> C2 1,000 pF polystyrene <br> Integrated Circuits <br> IC1, IC2 741C 8 pin D.I.L. (2 off) <br> Transistor <br> TR1 OC140 <br> Potentiometers <br> VR1 $500 \Omega$ horizontal carbon preset <br> VR2 $10 \mathrm{k} \Omega$ miniature moulded carbon linear potentiometer <br> VR3 $10 \mathrm{k} \Omega$ horizontal carbon preset <br> VR4 $10 \mathrm{k} \Omega$ miniature moulded carbon linear potentiometer <br> Miscellaneous <br> SK1-SK3 2 mm miniature sockets (3 off), 2 Elma knobs, $34 \times 17$ way 0.1 in matrix Veroboard



## IIPUT AMPLIFIER



Fig. 4.4. Circuit of an input amplifier

## COMPONENTS

input amplifiers (2 OFF)

## Resistors

| R1 | $20 \mathrm{k} \Omega$ |
| :--- | :--- |
| R2 | $10 \mathrm{k} \Omega$ |
| R3 | $20 \mathrm{k} \Omega$ |

All $2 \% \frac{1}{2}$ watt metal oxide

## Capacitors

C1, C2 $100 \mu \mathrm{~F}$ elect. 25 V (2 off)

## Potentiometers

VR1 $10 \mathrm{k} \Omega$ horizontal linear preset
VR2 $1 \mathrm{M} \Omega$ linear miniature moulded carbon

## Integrated Circuit

IC1 741C 8 pin D.I.L.

## Miscellaneous

SK4, SK5 2 mm miniature sockets ( 2 off ), $34 \times 17$ way 0.1 in matrix Veroboard, 1 Elma type knob


Fig. 4.5. Circuit board layout of input amplifiers

Increase the setting of VR1 until the rippling disappears and make further reductions in the setting of VR2, adjusting VR1 as necessary to keep the slope ripple free. Note that at the minimum setting of VR2 the ripple effect is at very low frequency and shows itself more as : hesitancy in the motion of the oscilloscope trace.

With careful adjustment, and the component values shown, it is possible to achieve a low frequency of 0.01 Hz but is is almost impossible to remove ripple entirely at this frequency and generally it is best to set the low end of the range to 0.05 Hz to ensure stability. The upper frequency limit with the $1.0 \mu \mathrm{~F}$ integrating capacitor is about 15 Hz .

In the prototype instrument one ramp generator was built as described and the second was built with an integrating capacitor of $0.47 \mu \mathrm{~F}$ thus giving an upper frequency limit of about 30 Hz with very little sacrifice to the v.l.f. end of the range. Such a procedure is recommended since the higher frequency is very useful in the production of rapidly changing. complex sound patterns.
When both ramp generators have been built and tested, mount the circuit board on the support plate in the position remote from the front panel (Fig. 4.3).

## INPUT AMPLIFIERS

The input amplifier theoretical circuit is shown in Fig. 4.4 and the circuit board layout in Fig. 4.5.
Although very simple in design rather more care is required in the component layout if hum pick-up is to be avoided, this latter problem tending to occur more when the gain control VR1 is at its maximum setting. Note that screened wire is used to connect the input sockets and gain controls to the circuit board. These wires should be trimmed as closely as possible to the required length and led directly to the circuit board without being formed into a harness.

The only setting up required is the adjustment of the offsets. VR2 should be set to maximum, the input grounded and, with the power supply on, adjusted to give an output level of precisely zero.

Reference to block diagram in Part One will show that Oscillator 1 is programmed directly by Ramp Generator 1 through the medium of a prewired interconnection. Accordingly tag 4 on the ramp generator McMurdo socket (SK 12) should be connected to tag 1 on the v.c.o. socket (SK8). This direct connection may be over-ridden by inserting either an open circuit or grounded jack plug into the external programming socket of the v.c.o. Alternatively a jack plug coupled to a patch cord may be used to provide programming from another source.
It is recommended that grounded jack plugs are used if precise manual control of v.c.o. frequency is required.

## PROGRAMME DATA SHEET

The completion of this module provides the constructor with greater facilities for the production of programming waveiorms and some quite complex sound structures. With the addition of the v.c.o. module there are now seven separate circuits and 12 controls to manipulate. There is thus a need for a method of logging control settings and interconnections so that any given sound structure may be repeated at a later date.

Details of a data sheet which will prove ideal for the purpose are given in Fig. 4.6. Control settings
would normally be recorded in the circles on the front panel representation while module interconnections would be indicated by a dot in the appropriate square on the grid matrix. Data recorded in the figure relates to the production of a type of bird song which will be described in detail in a later article.

## USING THE CONSTRUCTED MODULES

The provision of the input amplifiers allows waveforms from the oscillators and/or ramp generators to be mixed either additively or subtractively when used in combination with the voltage inverter. The permutation of all the possible settings of amplitude and frequency controls implies that an enormous range of sound structures may be produced and, whereas it is beyond the scope of this article to cover all the possibilities, a number of simple experiments are suggested for guidance.
Starting with the ramp generators, Fig. 4.7a shows the type of relationship which may be observed on the oscilloscope when one ramp generator is running at ten times the frequency of the other. With the output of a v.c.o. coupled to a suitable power amplifier and its frequency control at zero, application of either of the waveforms shown will cause the v.c.o. frequency to be swung from the lowermost end of the range to an upper frequency determined by the amplitude of the ramp generator waveform.

Since the upper frequency limit of the v.c.o. is dictated by the saturation level of the differential stage and since the gain of this stage is 10 then a programming waveform amplitude of about 1.4 V will drive the v.c.o. to its maximum frequency.

Fig. 4.7b shows the effect of mixing the waveforms shown in Fig. 4.7a additively. To achieve this, route the outputs of the ramp generators to separate input amplifiers which have their gain controls set to zero, i.e. unity gain, and then to the inputs of the voltage inverter. Observation of the output of this latter device reveals the composite waveform.

With the ramp generator output levels adjusted so that the maximum combined level is about 1.4 V route the voltage inverter to the input of the v.c.o. The result is an undulating sound the lowermost frequency of which is continuously rising at a rate set by the frequency of the slowest running ramp generator.

## SUBTRACTIVE MIXING

Fig. 4.7 c shows the effect of subtractive mixing of the ramp generator waveforms. Achievement of the staircase form is as follows.

Set the amplitude of the slowest ramp generator output to 1.4 V and route this to the voltage inverter via an input amplifier set to unity gain. Route the second ramp generator to the voltage inverter direct. Since this now sees the inputs from the ramp generators at opposite polarities the result is subtractive mixing which, when the amplitudes are at the correct levels, produces a staircase as shown.

Application of this waveform to the v.c.o. produces a rising, arpeggio-like sound. A falling arpeggio may be produced by reversing the routing of the ramp generators with the slowest direct to the voltage inverter, and fastest to the voltage inverter via the input amplifier. In this latter case the frequency control of the v.c.o. has to be set to its maximum level since the waveform from the voltage inverter is now positive going.

## SYHTHESISER PROGRAMME SHEET



|  |  | Sipnals Inputs |  |  |  |  |  |  |  | Sig or Con |  |  |  | Control Inputs |  |  |  |  |  |  |  |  |  |  | Control <br> Chenges |
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| \% | I/PAmp 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | - |  |  |  |  |  |
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| 8 | OP Ampl |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| \% | O/P Ame R |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Revert output |
| E | Tone $C$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | to Recorder |
|  | Ring Mod |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Reverb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Eny Shaper |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | S8 H |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Diff Amp |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Inverter |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | KBD Signel |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | K BD Syne |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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|  |  | $\square$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| DESCNAFTLON OF SOUND |
| :--- |
| EXTEANAL EQUMPMENT |
|  |
|  |

Fig. 4.6. Example of a programme data sheet

(a)
(b)
(Tc) ${ }^{2}$

Fig. 4.7. (a) Components for additive mixing; (b; resultant tinrough addition of components; (c) :subtractive mixing produces staircase waveform

## FIXING THE V.C.O. LIMITS

In these examples the v.c.o. has been programmed through its maximum working range but it is, of course possible to achieve the same effect within very precise frequency limits. For example, suppose it is wished to provide an arpeggio rising from 130 Hz


Fig. $4.8(a)$. Programmed ramp openerator output (0.) programming wavelorm


Fig. 4.9. Block diagram for ramp generator programming
to 520 Hz , the frequency control of the v.c.o, is set to give the voltage required to produce 130 Hz . The fact that the ramp output will, at times, be zero volts will not affect the l.f. performance limit since the v.c.o.s were originally set up with a link simulating a zerovolt programming input. Thus from Fig. 3.4 in last month's article it will be seen that the initial setting of the v.c.o. will require an input of about 24 mV . Also it wil! be seen that a frequency of 520 Hz . requires an input of about 42 mV and thus the output amplitude of the combined ramp generator signal will have to be $(42-24) \mathrm{mV}$. In a similar manner the manipulation and adjustment of the manual and atutomatic voltage sources can set the programmed sequence almost anywhere in the working range of the v.c.o.

## PROGRAMMING THE RAMP GENERATORS

The monotonous repetition of the ramp generator output can be considerably varied by application of programming voltages to its own external control input. Fig. 4.8 illustrates the effect of applying a steadily rising voltage to the control input.

The voltage has been derived from the output of the other ramp generator running at a fairly low frequency and routed via one of the input amplifiers set to provide a peak ramp output of positive 14 V . The resultant output of the programmed ramp generator consists of a series of ramps gradually increasing in frequency as the programming voltage rises to its peak, the aural effect when used to programme a v.c.o. being a kind of bounce.

For the best effect the programmed ramp generator should be running at about twenty times the frequency of the other

An extension of the above system is shown in the block diagram Fig. 4.9. In this case one of the v.c.o.s is also providing a programming waveform which is first amplified to provide an output swing of $\pm 7 \mathrm{~V}$. This is then combined, in the voltage inverter, with the output of the programming ramp generator set to its maximum output level. The voltage inverter is then routed to the programmed generator which has
been set to run at about 7 Hz , the overall result being a bounce which is changing its rate in a pattern depending on the relative frequencies of the programming sources.

## EXPERIMENTAL COMBINATION

There are many other combinations of the programming devices all of which result in the production of characteristic sounds. The constructor is encouraged to investigate these as widely as possible noting the control settings and interconnections which produce sounds of particular interest.

It should be noted that even quite small adjustments to amplitude and frequency of programming waveforms can cause relatively great changes in the sound structure. This is particularly the case when amplitudes are adjusted in complex programming waveforms such that the waveform changes potential, i.e. crosses zero. In these cases the v.c.o. will cease to oscillate for as long as the programming waveform remains positive and thus, for a fairly rapidly changing waveform, the long term output of the v.c.o. will resemble a series of tone bursts of varying frequency.

The use of positive going programming waveforms to the v.c.o. should be investigated with care, particularly when the manual frequency control is at or near zero. The sudden application of a large positive input will cause an unpleasant click due to the increase in v.c.o. output voltage as it goes into saturation. Similarly a low potential positive input applied for a prolonged period will, on its removal, give rise to a click when the v.c.o. comes out of saturation.

## USING A RECORDER

It is perhaps prudent, at this stage, to mention that a tape recorder is a most necessary adjunct to the Synthesiser if the full potential of the instrument is to be realised. This is essential because, although live performance is possible, it is somewhat limited due to the design of the keyboard which is monophonic. In order to produce complex realisations, it is necessary to employ a recorder in order that multitracking of one form or another may be used to blend or superimpose consecutive series of sound structures into a comprehensive whole.

In a similar manner many sound effects may be enhanced by the addition or superimposition of secondary sounds. This procedure can be particularly useful when complex effects such as storms, battles or woodland birdsong are being synthesised.

Quite apart from the creative aspects of using the tape recorder another important reason for its application with the Synthesiser lies in the establishment of a taped library of sounds.

Many excellent books and articles have been written on this subject but, in the field of creative recording, T. Dwyer's "Composing with Tape Recorders" (Oxford University Press 1971) contains much useful information.

## NOTE:

The power supply transformer in Part 2 has 0-30,0-30V separate secondaries. RI and R6 should be $5 \cdot 6 k \Omega 2 \%$ $\frac{1}{2}$ watt metal oxide resistor. IC2 should be insulated from chassis with a mica washer. In Part 3, VR2 is IOOkS.

ELECTRONIC MUSIC PRODUCTION

By Alan Douglas<br>Published by Sir Isaac Pitman \& Sons Ltd<br>148 pages $5 \frac{1}{2}$ in $\times 8 \frac{1}{2}$ in. Price $£ 2 \cdot 75$

ELECTRONIC MUSIC PRODUCTION presents a very much "up to the minute" look at the use of electronics in the production of music with special reference to the synthesiser and the applications of voltage control. The book is divided into four main sections. 1-Properties of conventional musical instruments. 2-Musical scales, temperament and tuning; concord and discord. 3-Electronic music generators. 4-Electronic music and the composer. Additionally there are two appendices which provide, in the first, a detailed specification of the Synthi 100 , a highly advanced synthesiser designed for interfacing with a computer and, in the second, details of MUSYS documentation standards together with an example drawn from part of a composition programmed on the Synthi 100 . Finally there is a comprehensive bibliography and index.

Electronic Music Production is a lucidly written book packed with data much of which will be new to the reader. There are plenty of clear line illustrations and circuit diagrams and there is little doubt that this book will be "required" reading for all students of electronic music-amateur and professional alike.

> g.D.S.

## LOGIC AND LOGIC DESIGN

## By B. Girling and H. G. Moring <br> Published by International Textbook Company <br> 328 pages, 9 in $\times 6$ in. Price $£ 5.80$

Abasic understanding of logic is essential for anyone interested in the design of computers and associated logic systems. This book, based on a course of lectures given at The City University, provides an excellent introduction to logic, starting from basic number and set theory. It covers the Computer Science requirements for a B.Sc. degree and each chapter concludes with a bibliography and a set of questions with solutions.
${ }^{1}$ This book is very well written and concepts are explained with the aid of copious clearly drawn diagrams. The book does not deal at all with engineering considerations in logic circuit design, concentrating rather on the logical concepts involved. As well as all the standard aids to logic design many up to date references are quoted so that modern concepts can be understood.

With the increasing interest in Computer Science this book will no doubt find its way into many degree courses as the standard reference work. It is well bound and excellently printed and though the price is rather high it is good value for money.
S.R.L.

## Next month: Sample Hold and Noise Generator.



# pochee calculator KIT REVIEW 

Supacal Calculator
Obtainable from S.C.S. Components Ltd., P.O. Box 26, Wembley, Middx HAO TYY.
Price $£ 39$ ( + V.A.T.) with special $£ 4$ discount to P.E. readers.
| Mmediately upon opening the box containing the SUPACAL calculator kit the decision should be made as to whether one is sufficiently equipped in terms of both tools and experience to undertake the construction of the calculator. Should there be any doubt in this respect, it is strongly recommended that the services of a more experienced friend or colleague he recruited for this work. The minimum tools required for building the $k$ it are a good soldering iron of 10 to 25 watts with a bit preferably no more than a sixteenth of an inch diameter, also a pair of side cutters, a pair of long nosed pliers, and a good light.
Many solder joints have to be made in a small area and a certain degree of skill is needed to avoid short circuits and dry joints. Fine solder is provided with the kit and this greatly simplifies the construction.

## COMPONENT PACKING

All components come in plastic bags marked with the value of the components contained, but it is as well to check these values against those required as it is always better to be safe than sorry. Because the printed circuit board has tracks both sides many solder joints have to be made on both sides of the board; this is tedious but it is essential to make good connections.
The display board and the inverter board for the 25 V i.c. supply come as ready made units and this eases the constructor's task enormously. The keyboard is already fitted into the top half of the case and wiring to the main circuit board is simple, though here again solder joints have to be made top and bottom of the board.

## HANDLING PRECAUTIONS

The calculator i.c. comes in a piece of protective conductive foam and the handling precautions in the instructions should be carefully followed. A socket is provided for the i.c. so the usual problems of soldering to an m.o.s. integrated circuit are overcome.

Instructions for the insertion of all components are given and these are easy to follow. A circuit diagram

and point-to-point wiring diagram are also supplied. Total construction time for the SUPACAL was three and a half hours in this reviewer's case. Any difficulties will probably be caused by poor soldering and a good light is useful for checking.

The kit suppliers offer a back-up service in the form of a fixed price repair facility and this ensures a fully working calculator no matter how much of a mess you made of the construction. Once the calculator is working then all parts are guaranteed for one year.

## CALCULATOR CONSTRUCTION

Now something about the calculator itself. It is housed in a strong plastics case and uses two rechargeable batteries for its power source. A ready built charger is provided with the kit; fully charged batteries give about eight hours working. There is an automatic fadeout facility which switches off the display (which consumes about half the total power) approximately ten seconds after a key has been pressed.

The keyboard uses conductive rubber contacts which give the machine an extremely light touch; in fact the switches are almost too sensitive, some care being needed not to enter a digit unintentionally.

## CAPABILITY

The calculator can handle all four arithmetic operations with all calculations being in floating point, with eight digits being displayed. There is a stored constant facility which, unlike most other calculators, can be used with all four functions. Another advantage of this calculator is that it will not overflow. Other calculators will ignore any entries over eight digits long; the SUPACAL stores not only the eight digits entered but also stores an exponent up to $10^{79}$; the true decimal point position is found by dividing by powers of ten until the point appears on the display. This enables more accurate answers to be found.

## INSIDE THE POCKET CALCULATOR

How does the pocket calculator work? The "heart" is the second generation single chip MOS LSI circuit type C500 manufactured by General Instruments Microelectronics. It contains within its 4,000 active devices all the logic necessary for performing eight digit, four function plus constant and floating decimal point, calculations.

The chip contains a read-only-memory (ROM) of 2,000 bits, a random-access-memory (RAM) of 100 bits and associated control logic, dividers and timing circuits for clocking and multiplexing. The chip simply requires a 25 V supply and a clock input of 50 kHz to 100 kHz , a keyboard, display, and circuits to drive the display and it becomes a fully operational calculator.
The display interface is by means of discrete buffer/driver transistors for segment and digit driving. The display is multiplexed, i.e. each digit is only driven for one-ninth of the time, there being nine l.e.d. digits with seven segment format.


BY FRANK W, HYDE

## SKYLAB EXPERIMENTS

The number of activities that have been planned for the Skylah project are extensive. The work periods are 28 days for the first crew and up to 56 days for the next two crews.

In some experiments the astronauts will be used to study the effect of prolonged weightlessness. So far the longest time in the weightless state has been 18 days. This was by three Russian astronauts during the Soyus 9 flight.

One of the after effects that became noticeable after the Soyus flight was a curious random stumbling which each astronaut suffered but for varying times. All had returned to normal within three weeks.

As the Russians always operate the "shirt sleeve" mode as it were, the Skylah experiments will be comparable though, of course, the available area for movement will be greater.

There will be specific exercises which each member of Sky/ah crew will do. These, together with studies of the changes induced in muscles, bones and the blood chemistry will enable a better assessment to be made of the space-induced effects.

Each man will have a special standardised diet to follow. With a special spring balance designed for zero gravity use, the astronauts will measure and record the mass of food they eat.

The spring balance is a coil spring to which is attached the item to be measured. The oscillation of the spring is measured electronically. The period of the oscillation depends upon the mass and on the known properties of the spring. In a similar way the astronauts will check their body weight using a spring chair.

Other experiments to be carried out are the study of crystal growth
of metals and alloys together with solidification properties by using an electric furnace. One special study will be that of the possibility of producing doped semiconductors of high chemical uniformity. It is thought that in zero gravity the effects of thermal convection in a gravity field will be avoided.

The changes in flammability which have been noticed in short periods of weightlessness in aircraft will also be studied. On many occasions it has been noted that flames tend to go out when the weightless condition has been reached.

## EARTH RESOURCES STUDY

Because the orbit of the space station will be inclined by $50^{\circ}$ to the equator something like 75 per cent of the earth's surface will be covered and the station will return every five days over a given area. This provides a unique opportunity to study earth resources. Some 132 experiments originating from about 24 countries will be undertaken.

Observations will be made with cameras both in the visible and the infra-red part of the spectrum, together with the micronave sweeps. The moisture in the soil, the vegetation type and its condition will be determined by comparing the photographs from different spectral areas.

The experiments are varied and the chart below gives some details.

These are but a few of the experiments agreed by NASA and there are many more suggestions involving, in some cases, on-board equipment and in others the use of data collected. NASA accepted 19 experiments from the total of 3,400 proposals sifted by the Science Teachers Association.

The results of the first period will undoubtedly influence the later programmes particularly on the effects of weightlessness.

## SOLAR OBSERVATION

The experiments involving solar observation are designed to both add to existing data and check the present thinking. Several of the station's telescopes are under automatic control from Earth. This has many advantages since there will be intervals between the change of crews when the station will be unmanned: continuous operation of the selected instruments is important.

The white light coronograph will measure the brightness of the corona and the polarisation. This will be done at distances varying between 1.5 and 6.0 solar radii from the Sun. The instrument has a number of sizes of occulting discs which are controllable and prevent the direct light from the Sun from reaching the objective lens. The scattered light is reduced to $10^{-10}$ of the mean solar radiance.

|  |  | CHART 1 |
| :--- | :--- | :--- |
| Experiment | Originator | Observation |
| Ecological | Joseph Otterman | Indentifcation of land <br> in Israel suitable for <br> wheat and date palms. |
| Ecological | US Department of <br> Agriculture | Seek infestation areas by <br> pine beetles in South |
| Dakota. |  |  |

T0 many, the fundamental principles invoived in computing are a foreign language. In this article the construction of a comprehensive Logic Tutor is described. Elsewhere in this issue is the first article on using the Tutor providing an introduction to digital logic theory with practical exercises so that at the end of the series a full understanding of computing should be gained

## TUTOR FUNCTIONS

The Logic Tutor is designed to demonstrate the and, NAND, nor and or gates in nand logic form. Other circuit functions demonstrated are flip-flops, counters and shift registers.

To demonstrate logic theory it is necessary 10 construct a basic bread board on which exercises can be carried out. This panel can be seen in the photograph with the various symbolic functions marked upon it.

The complete tutor can be made, using entirely bought parts. for about $£ 9$. This can, of course, be reduced by judicious shopping.

## LOGIC BOARD

In the prototype a $13 \mathrm{in} \times 10 \mathrm{in} \times 4 \mathrm{in}$ wooden box was used for housing the Tutor electronics, the logic board forming the lid

The latter is drilled as in Fig. 1 using a 1.2 mm drill for the terminal pin holes. Other holes should be shaped to suit the switches, lamps and digital indicator purchased but at this stage none of these components should be mounted The logic symbok

## COMPONENTS . . .

## DISPLAY CIRCUITS

Resistors
R1-R11 10CS! (see text) (11 off)
R12-R17 tko ( 6 of )
R18 47hs!
R19-R28 47cs (10 off)
All $10 \% \frac{1}{2}$ watt carbon
Transistors
TR1-TR32 EC102 or any 330 mW n.p.n. silicon planar switching transistor (32 off)

## Lamps

LP1-LP10 RDund M.E.S. bulbs 1-5V, 0.2A
Cold cathode fube
V1 Hivac GF2W or Mullard IM1026
LOGIC CIRCUITS integrated Circuits
IC1-IC6 945 D.I.L. (6 off)
IC7-IC10 946 D.I.L. (4 off)
IC11-IC12 930 D.I.L. (? off)
IC13 952 [IIL.
IC14 933 [.I.L.
IC15 945 D.I.L.

## Diodes

D1-D2 OA91 (2 off)

## Capacitors

C1-C2 $100 \mu \mathrm{~F}$ elest. $6 \mathrm{~V}^{\prime}$ (2 off)

## Switches

S1 Mains on/off taggle
S2-S5 Singlefcle, changeover taggle (4 off)
S6-S7 Miniature push button switches
LP11 Round M.E.S. kulb $1.5 \mathrm{~V}, 0.2 \mathrm{~A}$
D.I.P. Verobjare Ginこ31 in


The completed Logic Tutor showing the front panel layout
$\begin{array}{ccccccccccccccccccc}0 & 0 & O & O & O & O & O & O & O & O & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 2 & 3 & 4 & 5 & 6 & 7 & 8 & 9 & & & 0 & & & 0 & 0 & & 0\end{array}$



$\bigcirc$


RESET





NAND




EXTENDER

Fig. 1. Layout of logic board showing drillings and symbols



Fig. 3. Component layout and wiring for the power supply unit

Fig. 2. Circuit diagram of power supply

## COMPONENTS . . .

## POWER SUPPLY UNIT

Capacitors
C1 $100 \mu \mathrm{~F}$ elect. 350 V
C2 $5,000 \mu \mathrm{~F}$ elect. 15 V
C3 $10 \mu \mathrm{~F}$ elect. 15 V
C4 $100 \mu \mathrm{~F}$ elect. 15 V

## Rectifiers

D1-D4 REC41A Silicon Bridge Rectifier D5-D6 BY100 (2 off)

## Regulator

IC1 $5 \mathrm{~V}-600 \mathrm{~mA}$ monolithic voltage regulator (R.S. type MVR-5V or similar)

## Transformers

T1 240 V primary; $150 \mathrm{~V}, 10 \mathrm{~mA}$ secondary
T2 240 V primary; $9 \mathrm{~V}, 1 \mathrm{~A}$ secondary

## Miscellaneous

$18 \mathrm{~s} . \mathrm{w} . g$. aluminium as required, 12 way tag strip, double-sided terminal pins and pick-up tags 1.2 mm diameter (R.S. types)
on the board indicate six RS/JK flip-flops, fourteen two-input Nand gates, four four-input nand gates, two three-input NAND gates and two fourinput extenders (and). Most logic functions can be demonstrated with these.
The logic symbols are marked on the drilled board with paint or Letraset. These should be lacquered for permanent fixing after the doublesided terminal pins are pressed into the 1.2 mm holes. These pins have a shoulder to facilitate insertion without risk of pushing the pin right through the board.

## POWER SUPPLY

The next item to be tackled is the power supply which feeds the integrated circuits with a stabilised 5 volt, and the output displays.

To observe the logic outputs two alternative displays can be used; lamps to indicate outputs singly or a cold cathode numerical indicator. Although included this item can be dispensed with if costs are to be kept down.

The display supply requirements are 12 V for the lamps and 180 V for the neon indicator. The circuit diagram in Fig. 2 show how these outputs are derived.

The power supply unit is mounted on an 18 s.w.g. aluminium sub-frame as in Fig. 3, which also gives the interwiring details.
When the wiring is complete the output voltages should be checked with a meter before any loads are connected. If everything is functioning satisfactorily the sub-frame can be screwed to the base of the box.

## D.I.P. MOUNTING AND WIRING

The fifteen D.I.P. integrated circuits are mounted on a D.I.P. Veroboard (Fig. 4) in the orientation shown. Pin numberings for the i.c.s are identical as indicated on the key. When the i.c.s are soldered the wire links are added.

The next job is to connect the i.c.s to the logic board. In Fig. 5 the board symbol input and output pins are related directly to the numbered i.c. pins on the Veroboard so that point-to-point wiring can be made. To illustrate this; to wire ICI to its corresponding logic board symbol, ICI pins are connected to the underside of the logic board at the corresponding pin numbers (Fig. 5(a)).

Next the two-input NAND gates are wired (IC7IC10), the four-input (IC1I-IC12), the three-input


Fig. 4. Wiring and layout of the fifteen D.I.P. integrated circuits on the D.I.P. Veroboard

(b)



IC13
(d)

$167-1010$
$(946)$





ICn-10 10
(e)
(c)




Fig. 5. Identrying the logic symbol Verojins witt the i.c. pin numbering
(IC13), and finally the four-input gates (IC14) all being wired according to the relevant gate symbol of Fig. 5. The Veroboard can be fixed finally to the underside of the front panel with nuts, screws and stand off bushes.

## LOGIC SWITCHES

Four switches are provided ( $\mathrm{S} 2-\$ 5$ ) for logic 0 or 1 inputs to the gates. Here, 0 corresponds to 0 volts and 1 to 5 volts as indicated in Fig. 6. A switch output is taken from either of two Veropins at the switch pole. Wiring for all four switches is given later in Fig. 10.

## CLOCK GENERATOR

Most counting circuits can best be demonstrated by applying a clock input of about 2 to 4 Hz . This function is provided on the logic board by a 946 i.c. connected as a free running multivibrator (Fig. 7). The timing elements include two $100 \mu \mathrm{~F}$ capacitors.

Two outputs are available from this circuit, positive and negative square wave clock pulses. The pins for these are adjacent to the JK flip-flops (Fig. 1). It should be noted that the adjacent "bus-bars" alternatively marked " B " are earth returns to complete signal paths when patching leads. Wiring for the clock generator IC15 is included in Fig. 4.


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| $2 \mu \mathrm{~F}$ | 450 V | 22p | $2000 \mu \mathrm{~F}$ | $25 \vee$ | 43p |
| $4 ı \mathrm{~F}$ | 350 V | 151p | 2000 $\mu \mathrm{F}$ | 50 V | 58 |
| $8 \mu \mathrm{~F}$ | 450 V | $18 \frac{1}{6}$ | 2500 $\mu \mathrm{F}$ | 25 V | 30 p |
| $16 \mu \mathrm{~F}$ | 450 V | 20p | $2500 \mu \mathrm{~F}$ | 50 V | 66 |
| $25 \mu \mathrm{~F}$ | 25 V | $7 \frac{1}{1} \mathrm{p}$ | $3000 \mu \mathrm{~F}$ | 25 V | 33 |
| $25 \mu \mathrm{~F}$ | 50 V | $11 p$ | 5000 $/ \mathrm{F}$ | 25 V | 66p |
| $32 \mu \mathrm{~F}$ | 450 V | 30p | $5000 \mu \mathrm{~F}$ | 50 V | 4.21 |
| $50 \mu \mathrm{~F}$ | 50 V | $11 p$ | 8-8 $\mu \mathrm{F}$ | 450 V | 20p |
| $100 \mu \mathrm{~F}$ | 50 V | 12p | 8-16 $\mu \mathrm{F}$ | 450V | 22p |
| $250 \mu \mathrm{~F}$ | 25 V | 15¢p | 16-16 4 F | 450 V | 10p |
| $250 \mu \mathrm{~F}$ | 50 V | 19p | $16-32 \mu \mathrm{~F}$ | 450 V | 9p |
| $500 \mu \mathrm{~F}$ | 25 V | 20p | 32-32 $\mu \mathrm{F}$ | 450 V | 54 p |
| $500 \mu \mathrm{~F}$ | 50 V | 27 to | 50-50 $\mu \mathrm{F}$ | 350 V | 41 |
| $1000 \mu \mathrm{~F}$ | 25 V | 30p |  |  |  |



## WIRING THE INDICATORS

If the lamp bulbs are screw types these can be screwed into the holes provided. The cold cathode tube should be a press fit and glued finally into position.
The lamp driving circuits consist of two transistors and a resistor (Fig. 8) with the inputs connected to adjacent Veropins ( $0-9$ ). The value of the series resistor may have to be tailored so that the appropriate lamp gives the required light output. The limits to be expected here are 27 ohms to 220 ohms. All drive circuitry is mounted close to each lamp base.

Each cathode of the indicator tube is switched by a transistor (Fig. 9) the emitter of each being connected to board Veropins numbered $1-0$. A wiring detail of the transistor drive circuits indicators and switches is given in Fig. 10.

## DISPLAY CHECKS

Connections to the indicator tube can be made with the same tags as used for terminating the patching leads, this saves the cost of a special valve base. For a rigid transistor assembly the supply lines and earth returns should be of stiff copper wire.

The first test is with the indicator which should glow as soon as its 180 V supply is connected. All the numbers will glow until a particular cathode is grounded when all the current passes via one number which cancels off the others.
If this test is satisfactory connect the 5 V supply to the panel and check that the indicator lamps light when the logic inputs are applied to their terminals, remembering that "off" corresponds to 0 and "on" corresponds to 1 .

## PATCHING LEADS

Some leads can now be terminated with tags for patching exercises. These should be of 12 in , $8 \mathrm{in}, 4$ in and 2 in lengths. More short leads will be required than long leads and it facilitates easy location of a particular length if the lengths are of one given colour.
The Logic Tutor should now be functioning and simple exercises can be performed to get the feel of the instrument. See page 438.


# LOGIC TUTOR EXPPERTIMENTS <br>  

AND and OR GATES

N DIGITAL LOGIC there are two states, these are low and high or off and on states. In positive logic, which is the type used in the Logic Tutor, the off or low state is 0 V and the on or high state 5 V . These two conditions we also know as logical 0 and logical I respectively.

The simplest gate which allows or stops a 0 or 1 input is the AND gate formed by an arrangement of diodes as in Fig. I.I.

## TRUTH TABLES

If there is no connection to either input the output will rise to 5 V since no current flows through the resistor but if either input is grounded current flows to ground thereby reducing the output to zero volts.
This is logically expressed in logic truth tables and the output sequence is expressed as A.B which is the Boolean Algebra way of representing A AND B. So in the circuit both A AND B must be $!$ in order that the output is $I$.

## PROVING IT

To electrically check the truth table connect the four logic input switches to the inputs of EXTENDER I and the output
of this to the CHECK lamp. Operating the switches will show that the lamp lights only when all inputs are logical 1 .

## OR GATE

If the diodes of the AND gate are reversed and the supply is changed to OV an OR gate is formed as in Fig. 1.2. In this gate the output is always I if any input is 1 , that is, the diodes will conduct if the input goes to 5 V but the output return to zero if no input is connected or the inputs are grounded.

It is not possible to demonstrate an OR gate on the tutor since it is seldom used on its own.

The OR function is normally expressed as a combination of NAND functions known as a wired OR functions which will be demonstrated in a later exercise. The $O R$ function is written as $A O R B$; symbolically this is $A+B$.

by M. Hughes



Flg. 1.1. AND gate and truth table



## POInIS Gilsing

HI FI TAPE LINK (March, April 1973)
In Components List, Page 213, R121, 22012 was omitted. In Fig. 6 page 328, R13 adjacent to C12 should be R12. TR9 and TR109 base diagram, drain and gate connections reversed. On underside wiring collector of TR103 should go directly to R102 not via point marked TO SK2 PIN. In Table 3 TR10 collector voltage is dependent on VR5. First paragraph page 332 should read "collectors of TR10 and TR110 is 12 volts".

## P.E. SYNTHESISER

See note on page 427

## P.E. TRIFFID I.C. RADIO (February 1973)

R7 should be $4.7 \mathrm{k} \Omega 2$ not $10 \mathrm{k} \Omega$ as specified. R17 should be $10 \Omega 2$ not $10 \mathrm{k} \Omega$ as in the components list. High gain transistors must be used for TR2 and TR3. Fiq. 7. Transistor TR4 should read c.b.e. not as shown.

## A.F. SIGNAL GENERATOR (November 1972)

VR2 should be $10 \mathrm{k} \Omega 2$ not $1 \mathrm{k} \Omega$ as shown in Fig. 1 and components list. In Fig. 3 C5 and C7 to S1 have been reversed, i.e. C5 should be where C7 is shown.

## 10 Action Packed Instrument kits from Heath



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BN 7427 SN7428
GN7430 8N7433
 SN7437 0 EN7440 0
SNTHALAN 0.76 0. 18 o. 16
8N7442 $\quad 0.75 \quad 0.72 \quad 0.70$
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$\begin{array}{llll}8 N 7445 & 2.001 .75 & 1.60\end{array}$
$\begin{array}{lllll}\text { SN } 7447 & 2.00 & 1.75 & 1.60 \\ 1.75 & 1.60 & 1.45\end{array}$
$\begin{array}{lllll}8 N 7448 & 1.75 & 1.80 & 1.45\end{array}$
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A


#### Abstract




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## Gerry Brown ON|WETHNGGE



## SHEER CUSSEDNESS

The number of times I have heard people justifiably complain about having put a screwdriver down on the floor while adjusting some piece of equipment, only to find, on going to pick it up, that the darned thing had surreptitiously "hopped it'". If that didn't happen, one could lay even odds that the four screws, previously lying on your left-hand side, had somehow learned to interpret the structure of the DNA molecule enabling them to grow legs of their own.

Screwdrivers are not, however, exclusive in possessing a mind of their own, oh no. Indeed, the effect is not entirely foreign to the wrong side of hot buttered crumpets, marmalade toast, and (on occasion) the resistor that you've just soldered into position (and for which you are enduring agonies in order to prove that you just don't make dry joints) flying off at one end and treating both you and your starboard eye to a good "dollup" of molten solder! Soad's Law, for that is the nice way of putting what this effect has come to be known as, is almost certainly


Fig. 1
the one which equates with the belief that "lf something can go wrong, then it will''.

My old friend Denis has an interesting theory about the effect (also, in ancient literature, referred to as the 4th Law) and has recently put it to the test. He believes, you see, that Soad still exists somewhere, and further that he controls his meddling from either the Moon, or that other satellite which the earth is supposed to have.

The test, which you may have already proved unwittingly, is accomplished by employing a "sacrificial" circuit like the one l've shown in Fig. 1. With such an arrangement one can easily establish how far away this bloody-minded individual is.

First set switch S1 to position "a", then select the most expensive transistor you have, and connect it into circuit. Spin the flywheel-driven
rotary switch (the normal wafer type, but with mechanical "click" and "end stops" removed). When it has come to a standstill, decide quite deliberately to yourself whether to operate switch S2 to "b" or "c". This done, now operate the switch quickly to the opposite position of your choice; but do it within 2.68 seconds, I implore you.

Provided the decision is made within this time, I'm told it has never been known to "do-in" a transistor. This being so, it looks certain that this ubiquitous enemy of mankind must inhabit a world about a quarter of a million miles from here, composed, for the most part, of dud transistors, brand-new screwdrivers, and fluff-covered "jam-butties".

Judging from his discussion a couple of months back, I have a shrewd suspicion that Frank Hyde knows something of the fella's co-ordinates but is not letting-on!

## NEWS BRIEFS

## 1973 Design Council Awards

Two electronics companies feature prominently among this year's Design Council Awards for consumer goods. Sinclair Radionics win an award for the Sinclair Executive calculator and Rank Radio International win an award for the Wharfedale "Isodynamic" headphones.

The Sinclair Executive pocket calculator was launched in June 1972 and now, nine months latéf, sales are running at nearly $£ 100,000$ per month and profits of $£ 300,000$ are forecast for the financial year ending in April this year.

The Wharfedale Isodynamic headphones also introduce some technological advances to achieve a quality of sound previously only reached in headphones costing well over twice as much.

The Wharfedale system combines the best of the
electrostatic method with the simplicity and price advantage of the electromagnetic method by using a lightweight diaphragm driven evenly all over its surface by magnetic means.

Launched in London last year, sales for the first year are expected to reach 100,000 units and in fact Wharfedale are having difficulty meeting the demand.

## New Electronics Course at Keele University

AmONG nine new courses announced by Keele University is a new degree course in Electronics. There is great demand for honours Electronics, it being one of the major growth areas in scientific studies. There is particular interest in Electronics where it overlaps with such areas as cybernetics, information theory and "bioelectronics".

Three and four year courses will be on offer, and amongst the permissible combinations of courses over three years will be Electronics and Music.

For further information please contact the Director of Information Services or Professor D. J. E. Ingram, Department of Physics, University of Keele, Keele, Staffordshire ST5 5BG.


## PRICE WAR CONTINUES

A phenomenon of the electronics industry is that while everything else seems to be shooting up in price, many electronic products persist in going down. This is mainly due to the nature of the beast. High technology demands big investment in $R$ and $D$ and, more often than not, a further major investment in production equipment. So new products tend to start their life as high cost items capitalising on improved performance. Then, as production increases, there , is the so-called "learning curve" which, when mastered, gives fewer rejects and higher production rates. By this time, other firms are getting into the same market and any monopoly position that may have been attained is soon eroded. Add these factors together and you can see the reason why prices tumble.

No less an authority than Dr lan Mackintosh, 20 years in the semiconductor business and now a leading consultant, goes as far as to suggest in a recent press interview that aggressive pricing is the key to success. Essentially, he maintains, semiconductors is a volume industry and nobody gets volume without competitive prices. He cites the 1971 price war in TTL devices as nothing new and forecasts a similar war in MOS devices.

Certainly, ready availability of devices and lowered prices are working their way through into products. Look at digital multimeters. The Solartron 4440 is billed in the advertisements as low-cost at $£ 115$. Along comes Sinclair with the DM1 at £49. Not to be left out of the act, Advance Electronics introduce the Alpha DMM8 at $£ 55$.
It wasn't all that long ago that a digital panel meter was listed at
£99. Today you can get one for well under $£ 50$. Of course, the products I have mentioned are not all to the same specifications and therefore not directly comparable but the trend is there-downwards in price.

The trend is most obvious in consumer products-in radio, TV, tape recorders, pocket calculators. Look around and shop aroundyou can see it happening. I find it intriguing that some of my friends in manufacturing industry claim it is often cheaper to buy their employers' products through cut-price retail outlets than through their own staff shops.

The biggest shock, however, comes not through price competition between existing technologies and derivatives thereof, but when a completely new technology threatens to displace the old. Semiconductor memory manufacturers may well spend restless nights following the disclosures that IBM researchers have developed amorphous film bubble memories and got them into experimental use. Moreover, IBM say the new process cuts bubble memory costs ten-fold as well as conferring advantages such as extremenly high density packaging.

## EUROCONTROL

It was quite an experience attending the signing of Eurocontrol's latest commercial contracts for the new KARLDAP air traffic control centre at Karlsruhe. The signing was between Plessey Radar, Thomson-CSF and AEG-Telefunken on the one hand, and Eurocontrol officials on the other, and covered the supply of electronic equipment to the value of over $£ 5$ million. We had full simultaneous translations of the proceedings which took place in the Eurocontrol Brussels HQ beneath the flags of the member nations.

Plessey Radar's share was worth $£ 1.25$ million. Good for Britain, of course, but what was most pleasing was to be in at a ceremony where nations and companies were working amiably together towards a common good.

## ERNIE Mk. II

Having never won a penny on Premium Bonds it was interesting to visit the newly installed ERNIE Mk II at Lytham St Annes and see for myself that everything was fair and above board and that my lack of success was nothing more than bad luck.

The original ERNIE, now honourably retired, was built by the Post Office and did a marvellous job. The success of Premium Bonds has been so staggering that Old ERNIE was too sluggish to cope
with the draw. It was taking ten working days to generate the prize list. New ERNIE picks out the winners of over 90,000 prizes each month in just three hours. This is remarkable when you remember that each random number generated has to be checked against a master file to see if it has been sold or not.

New ERNIE was designed by Dr Roger Harding of Plessey Telecommunications under a contract worth $£ 250,000$. Plessey has also supplied a smaller system to New Zealand who run a similar Bonds scheme. Plessey now have ERNIE on offer world-wide and could secure more orders from governments who wish to run similar savings schemes.

To-date, ERNIE has paid out 10 million winners with nearly $£ 350$ million of prizes. Average odds of winning are 10,350 to 1 . Don't despair-there will be even more prizes in future.

## GROWTH

Several sectors of electronics are now showing good growth. VAT has helped Pitney-Bowes in selling electronic cash registers which have calculating power and produce cash receipts showing the amount of VAT paid. Sales are well up on the forecasts. NCR is another company gearing up to get in on the electronic point-ofsale business.

Over $£ 3.5$ million is said to have been invested in getting a production line going at Dundee for the NCR 280 retail terminal and first orders have been taken in the UK. In the United States the order book is reported as being 20,000 units of which 4,500 have been installed. Dundee output is planned to match a sales forecast of over 1,000 units this year rising to over 4,000 units by 1975.

Finally, MDS Data Processing Ltd. report big European sales for the 2400 Key Display System, a key-to-disc data entry system for computers. In 14 months more than 500 systems have been ordered which, together, use 6,000 key-stations.

## AEROSPACE EXPORT DRIVE

More than 100 British aerospace companies will be at Paris for this year's air show in June. Electronics companies will be well represented during what promises to be a boom exhibition despite setbacks on the Concorde programme. Last year's exports were in the region of $£ 400$ million for the industry as a whole with electronic navaids and quided missiles accounting for a big chunk.

## Build yourselfa TBANSISTOR RADID <br> WITH AFTER SALES SERVICE

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Lasy to follow instructions and diagrams．Parts pricelist and easy build plans 30 p （FREF with parts）．Earpiece with ghy and awitehed socket for pritate listening 330 ext

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ROAMER SIX


WAVEBANDS：
MW．LW，
SWi．SW2．
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## POCKET FIVE

## TRANSONA FIVE <br> 5 TRANSISTORS AND 2 DIODES

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TOTAL－EP．P．\＆INS． $25 p$ BUILDING COSTS 2$]^{\circ} \rightarrow$（OVERSEAS



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| 8N7400 | 18p | 15p | 8N7403 | 55p | 50 p | 8N7450 | 16p | 15p | SN7489 | $6 \cdot 05 p$ | 5.85p |
| 8N7401 | 16 p | 15p | SN7425 | 55 p | 50p | SN7451 | $16 p$ | 15p | 8N:490 | 74p | 72 p |
| 8N7402 | 16 p | 15 p | 8N7427 | 49p | 46p | 8N7453 | 18p | 15p | 8N7491 | 1.10p | 1.04 p |
| 8N7403 | 18D | 15p | 8N7428 | 77 p | 72 p | 8N:454 | 16p | 15 p | SN7492 | 74p | 72 p |
| $8 \times 7404$ | 18 p | $15 p$ | SN7430 | 16p | 15p | SN 7460 | 16p | 15p | 827 7403 | 74 p | 72p |
| 8N7405 | 16p | 15p | 8N7432 | 90p | 46p | 8 8N740 | 33p | 29p | 8N7494 | 85p | 72 p |
| 8N740 | 38p | 35p | SN7433 | 94. | 82 p | 8N7472 | 33 D | 29p | SN7495 | $85 p$ | 72 p |
| SN7407 | 38 p | 35p | $8 \mathrm{BN7437}$ | 72p | 68p | 8N7473 | 41 p | 39 p | 8 N 749 t | 95p | 92 p |
| 8N7408 | 20p | 18p | EN7438 | 720 | 690 | 8N7474 | $41 p$ | 38p | 8N74100 | 1.80 p | 1.75p |
| 8NT409 | 20p | 18 p | 8N7440 | 18p | 15p | 8N7475 | 50p | 47p | SN74104 | 1.09 p | 1.08 p |
| 8N7410 | 17p | 15 p | SN7441 | 74 p | 70 p | 8 SN 776 | 44 p | 43p | gN 74105 | $1.09 p$ | $1 \cdot 66 \mathrm{p}$ |
| EN7411 | 27 p | 25p | 8N7442 | 74 p | 70p | 8N7480 | 73 p | 70 p | SN74107 | 44p | 42 p |
| 8 S 7412 | 88p | 35p | SN744, | 1-43p | 137p | SNT481 | $1 \cdot 32 \mathrm{p}$ | 1.26p | SN74110 | 61p | 58p |
| 8N7413 | 32p | 29p | AN7444 | 1-43p | 137 p | AN748\% |  | 959 | AN74111 | $1 \cdot 37 \mathrm{p}$ | $1 \cdot 27 \mathrm{p}$ |
| SN7416 | 47p | 43 p | 8N7445 | 2.00p | 1-92p | gN7403 | 1.20 p | -15p | SN7418 | $1 \cdot 100$ |  |
| SN7417 | 475 | 43 p | SN 7446 | 1.07p | 1-02p | 8N7484 | 1.10 p | 05p | 8N7419 | 1 -47p | 37p |
| SN7420 | 18p | 15p | AN7447 | 1-10p | 1.03 p | gN7485 | 3.98p | $3 \cdot 85 p$ | 8N74121 | 44p | 41p |
| 3N:422 | 65p | 50p | SN7448 | 1.10p | 1-03p | SNT486 | 36p | 35p | 8N74129 | 1.64 p | 43 p |

## Electrolytic Capacitors

| 4 VOLT |  | 16 VOLT |  |
| :---: | :---: | :---: | :---: |
| $47 \mu \mathrm{~F}$ | $6 \frac{1}{2} \mathrm{p}$ | $15 \mu \mathrm{~F}$ | $6 \frac{1}{2}$ |
| $100 \mu \mathrm{~F}$ | $6 \frac{1}{2} p$ | $33 \mu \mathrm{~F}$ | $6 \frac{1}{2} \mathrm{P}$ |
| $220 \mu \mathrm{~F}$ | $6 \frac{1}{2} p$ | $68 \mu \mathrm{~F}$ | $6 \frac{1}{2} \mathrm{p}$ |
| 330 uF | $6 \frac{1}{3} \mathrm{p}$ | $150 \mu \mathrm{~F}$ | 8p |
| $1000 \mu \mathrm{~F}$ | 13 p | $220 \mu \mathrm{~F}$ | 9 p |
| $4700 \mu \mathrm{~F}$ | 29p | $680 \mu \mathrm{~F}$ | 17 p |
|  |  | $1000 \mu \mathrm{~F}$ | 17 p |
|  |  | $1500 \mu \mathrm{~F}$ | 25p |
|  |  | $2000 \mu \mathrm{~F}$ | 43p |


| 63 VOLT |  |
| :---: | :---: |
| $33 \mu \mathrm{~F}$ | $6 \frac{1}{2} \mathrm{p}$ |
| $68 \mu \mathrm{~F}$ | $6 \frac{1}{2} \mathrm{p}$ |
| $150 \mu \mathrm{~F}$ | $6 \frac{1}{2} \mathrm{p}$ |
| $470 \mu \mathrm{~F}$ | 11 p |
| $680 \mu \mathrm{~F}$ | 13 p |
| $1500 \mu \mathrm{~F}$ | 18 p |
| $2200 \mu \mathrm{~F}$ | 18 p |
| $3300 \mu \mathrm{~F}$ | 26 p |

## Linear Integrated Circuits

\author{

301 DIL | 301 |  |
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## Transistors

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# PRATENTE RETCETM 

## CAR WARNIIHE CIRCUIT

A Company which is very active in the field of patents for car satety devices is Joseph Lucas (Industries). Their latest device, BP 1297 385, triggers an alarm if a driver attempts to leave his vehicle without removing the ignition key.

In the patent circuit, Fig. 1, the car battery has its negative terminal earthed to chassis and its positive terminal connected to one side of a car internal rooflight LP1.

The other side of the light is earthed to chassis via three separate parallel paths. One of these paths contains switch S1 which is operated by the passenger door of the vehicle and closes when the door is open. The second path contains a switch S2 which is manually controlled from within the vehicle.

The third parallel path contains a diode D1 and switch S3 in series. Switch S3 is operated by the driver's door and closes when the door is opened. Closure of any one of the switches S1, S2, S3 energises LP1.

The "live" side of switch S3 is connected to the positive battery terminal via an alarm buzzer or bell in series with a resistor R1.

An npn transistor TR1 has its collector-emitter path connected across the alarm and its base connected to the positive battery terminal through resistor R2 and to earth via switch S4. The switch S4 is ganged to the ignition switch and closes when the ignition key is in position.

When the car is being driven, S4 is closed and current flows through R2; no current flows through the alarm or the transistor. When the driver stops the vehicle and removes the ignition key, S4


Fig. 1
opens. As the driver gets out of the car the act of opening his door closes S3 and TR1 is turned on by current flow through resistor R1. This short circuits the alarm, which thus cannot sound.

In the event that the driver forgets to remove his ignition key, S4 stays closed and no base current reaches the transistor when S3 closes (as the driver opens his door). In this case the alarm receives current via R1 and sounds the alarm.

The presence of the diode D1 ensures that the alarm cannot be operated when one or both of the switches S1 and S2 are operated.

## BUTLER-TYPE OSCILLATOR CIRCUIT

BP 1282853


Fig. 1

International Standard Electric Corporation in BP 1282853 discloses a Butler-type oscillator circuit of the generally known type in which a first and second transistor have their emitters coupled by a series resonant circuit.

The first transistor has its base biased to a fixed potential and its collector coupled to the base of the second transistor to limit feedback amplitude. The output signal is in the form of a clipped sine wave so in some uses, e.g. in telephony where distortion may cause the faulty operation of receiving equipment, the clipped signal must be corrected by filtering. The filterers necessary can, however, be bulky and costly in comparison with other miniaturised components.

What ISEC suggest is a modified Butler-oscillator with three npn transistors TR1, TR2 and TR3 and a buffer output stage formed from an npn transistor TR4 mounted in emitter follower configuration.

## CIRCUIT PROTECTION

Connecting a car battery into circuit the wrong way round can cause damage, e.g., in the generating and regulating circuits of the vehicle. A diode can be used to block wrong polarity currents but where the circuit carries heavy surges, the diode is at risk.

In BP 1293046 Pal-Magneton Narodni Podnik of Czechoslovakia describe three closely related simple ways of connecting circuits which must carry heavy currents and are sensitive to polarity.

The circuit, Fig. 1, shows a relay with its contacts RLA1 in series with a battery and the coil in series with diode D1 and switch S1. The coil, D1 and S1 are connected in parallel with the baftery.

The contacts RLA1 are normally open and the diode D1 ensures that current will flow through the relay coil (when $S 1$ is closed) only if the battery is connected with the correct polarity. Incorrect polarity will cause the diode to block current flow through the coil with the result that the contacts stay open and the polarity sensitive load is safeguarded.

The circuit in Fig. 2 shows RLA1 contacts connected as in Fig. 1 but diode D1 is used in parallel with the coil. A resistor R1 is connected in series with the coil and S1.

Again, current flows through the relay coil only if the battery is correctly connected, but in this case if the polarity is wrong the diode D1 will conduct and, in effect, put a short across the relay coil stopping it operating. The resistor R1 prevents the full short circuit current from passing through the diode when the battery is connected incorrectly.

BP 1293046


Fig. 2

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THE RADIO AND ELECTRONIC ENGINEER
(The Journal of the Institution of Electronic and Radio Engineers)
VOL. 43 No. 1/2 January/February 1973.
T is unusual to review a Journal, but this particular publication is of especial and topical interest to all who are involved in any way with semiconductors. The January/February issue of the Radio and Electronic Engineer is almost entirely devoted to special contributions from leading British scientists and engineers who have been associated with semiconductor developments during the past 25 years. Collected together are 18 papers, each written with authority based upon intimate involvement and covering some particular aspect of the design, development, manufacture or application of discrete active devices and integrated circuits.

As a technical record of the first twenty-five years of semiconductors, including their impact and influence upon different specialised fields of application, this issue of the Radio and Electronic Engineer warrants a place on the bookshelf of any electronics enthusiast.

Copies may be obtained from the IERE Publications Sales Department, 9 Bedford Square, London, WC1B, price $£ 2.00$ per'copy, post free.

HANDBOOK OF BASIC ELECTRONIC EQUIPMENT By W. Oliver
Published by Foulsham Technical
102 pages, $5 \frac{1}{2}$ in $\times$ 9in. Price $£ 1.75$

THE AUTHOR of this book will be known to all readers of Foulsham-Sams books as the man who translates American into English. The main idea behind this book seems to be that of giving readers some technical background on basic equipment but mainly information on suppliers.

However, if one is going to give technical information it is essential not to give wrong information. The note inside the front cover states that "mathematics . . . have been minimised so that the book will be easily understood by even beginners". After reading the book it makes me wonder whether Mr Oliver knows any maths! For instance, on capacitors: "the total effective capacity of capacitors in series is the sum of the individual capacitors"; or on resistors: " 2 K and 4 K in parallel, then in series with the 3 K , gives you roughly 1,333 ohms" (yes, very roughly, in actual fact 4,333 ohms); the term EMF is used where potential drop is meant; a varactor is described as a "very special kind of diode" whereas all diodes exhibit varactor action.

If one is going to present technical information, especially for beginners then one has got to be a little more accurate than this. No, I am afraid I would not recommend this book to any beginner; the suppliers addresses may be useful but as a technical work it leaves very much to be desired.
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No. 12 V 24 V to oz
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| Amps. | Weight | 30 VOLT RANGE <br> Size cm. <br> Secondary Taps |  |  | $P^{\prime}$ \& $P$ |  |
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| 1.0 | 20 | $8.0 \times 6.4 \times 6.0$ |  |  | 1.48 | 36 |
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| 3.0 | 46 | $10.2 \times 8.9 \times 8.6$ |  |  | 2.72 | 42 |
| 4.0 | 60 | $10.2 \times 10.0 \times 8.6$ |  |  | 3.23 | 52 |
| 5.0 | 68 | $12.1 \times 10.0 \times 8.6$ |  |  | 4.02 | 52 |
| 6.0 | 78 | $12.1 \times 10.0 \times 10.2$ |  |  | 4.80 | 52 |
| 8.0 | 100 | $14.0 \times 11.7 \times 10.0$ |  |  | 6.20 | 67 |
| 10.0 | 122 | $14.0 \times 10.2 \times 11.4$ |  |  | 7.85 | 67 |


| Ref. | Amps. | Weight | Size cm. ${ }^{50}$ | VOLT RANGE Secondory Tops |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| No. |  | 16 oz |  |  |  |
| 102 | 0.5 | 111 | $7.0 \times 7.0 \times 5.7$ | 0-19-25-33-40-50V | 1.46 |
| 103 | 1.0 | 210 | $8.3 \times 7.3 \times 7.0$ | , , , | $2 \cdot 13$ |
| 104 | 2.0 | 50 | $10.2 \times 8.9 \times 8.6$ |  | 2.96 |
| 105 | 3.0 | 60 | $10.2 \times 10.2 \times 8.3$ | .. .. | 4.01 |
| 106 | 4.0 | 94 | $12.1 \times 11.4 \times 10.2$ | .. | 5.31 |
| 107 | 6.0 | 12 | $12.1 \times 11.1 \times 13.3$ | ., .. | 7.85 |
| 118 | 8.0 | 189 | $13.3 \times 13.3 \times 12.1$ | ., .. | 10.25 |
| 119 | 10.0 | 1912 | $16.5 \times 11.4 \times 15.9$ | "., ". | 12.85 |
| Ref. | Amps. | Weight | Size cm. ${ }^{60}$ | VOLT RANGE Secondory Tops | P |
| No. 124 |  | 16 oz |  |  |  |
| 124 | 0.5 | 24 | $8.3 \times 9.5 \times 6.7$ | 0-24-30-40-48-60V | $1.48 \quad 36$ |
| 26 | 1.0 | 30 | $8.9 \times 7.6 \times 7.6$ | ., .. | 2.0636 |
| 127 | 20 | 56 | $10.2 \times 8.9 \times 8.6$ | ". | 3.2342 |
| 125 | 3.0 | 88 | $11.9 \times 9.5 \times 10.0$ |  | 4.9252 |
| 123 | 40 | 106 | $11.4 \times 9.5 \times 11.4$ |  | 6.3567 |
| 120 | 6.0 | 1612 | $13.3 \times 12.1 \times 12.1$ |  | 9.2082 |
| 122 | 10.0 | 232 | $165 \times 12.7 \times 16.5$ |  | 15.23 |

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25
25
BCY $\begin{aligned} \text { 25p } & \text { BCY } \\ \mathbf{4 4} & \text { BD } 124 \\ 76 & \text { BD } 131 \\ 44 \mathrm{p} & \text { BD } 132\end{aligned}$
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25p BDY 20 $\mathbf{2 5 p}$ RDY 20
$\mathbf{2 6 p}$ BF 115 20p BF103 K 62 17
23


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20p BF 196
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BFY 25p
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| :---: | :---: | :---: | :---: | :---: | :---: |
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| 1.0 | 100 v | 5p | 100 | $25 v$ | 6 p |
| $2 \cdot 2$ | 25v | 7p | 100 | 40 V | 7p |
| 22 | 63 v | 5 p | 100 | 53 v | 10p |
| 47 | 40 v | 5p | 220 | 25 v | 8 p |
| 10 | 25 v | 5p | 220 | 40 v | 9p |
| 10 | 63v | 6 p | 470 | 25 | 12p |
| 22 | $25 v$ | 6p | 1000 | 25 v | 16p |
| 22 | 40 V | 6 p | 2200 | $25 v$ | 30 p |
| 47 | 25v | 6p | 4700 | 16 v | 33p |
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