OS250 10MHz DUAL TRACE OSCILLOSCOPE

Instruction Manual

ADVANCE INSTRUMENTS

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Telex 263785

Division of ADVANCE ELECTRONICS LIMITED

Specification

DISPLAY

5 in flat faced c.r.t. giving 10 cm × 8 cm display E.H.T.– 3.6 kV overall.

Phosphor–P31. Long persistence (P7) available as an option.

VERTICAL DEFLECTION

Two identical input channels. Y1 and Y2
Bandwidth (–3dB) DC–10MHz. (2Hz– 10MHz on AC)
Sensitivity 5mV/cm to 20V/cm in 1-2-5 sequence.
Accuracy ±5%.
Input Impedance 1 MΩ/approx. 28 pF.
Input coupling DC–GND–AC.
Protection 400V DC or pk AC.

DISPLAY MODES

Single Trace Y1 or Y2.
Dual Trace chopped or alternate modes, automatically selected on timebase switch. Chop rate approx. 250kHz.
X-Y mode with Y1 input giving X deflection and Y2 input giving Y deflection.
Bandwidth DC to 500kHz <3° phase shift at 20kHz.

HORIZONTAL DEFLECTION

Timebase–1 μs/cm to 0.5s/cm in 18 ranges (1-2-5) sequences.
Accuracy ±5%.
X Expansion–X10 pull switch gives fastest speed of 100 ns/cm. Accuracy ± 5%
Variable control gives >2.5:1 reduction in sweep speed.

TRIGGER

Variable level control with option of bright line in absence of signal.

Trigger level control range

INTERNAL > 8cm
EXTERNAL > 20V

Source
Internal Y1 + or –
Y2 + or –
External + or –
External trigger input impedance, approx 100kΩ/10pF.

Coupling AC, AC fast, TV Frame.
Sensitivity

Internal	2mm approx. 40Hz–2MHz.	bright line on or off.
External	1V approx. 40Hz–2MHz.	
Internal	1cm approx. 8Hz–10MHz.	bright line off.
External	5V approx. 8Hz–10MHz.	

Internal 2cm pk/pk video on TVF

ADDITIONAL FACILITIES

Calibrator 1 V ± 2% square wave at supply frequency.
Ramp output 0-10V.
Z mod input AC coupled. 10V gives visible modulation (2 Hz to 10MHz). 70V gives full blanking.

SUPPLY

95-111V, 103-121V, 111-130V.
190-222V, 206-242V, 222-260V. } 45-440Hz
Approx. 25VA.

OPERATING TEMPERATURE RANGE

0-50°C (15°C to 35°C for full accuracy, approx 2% degradation at 0°C and 50°C)

DIMENSIONS

18cm (7″) × 29cm (11⅜″) × 42cm (16½″)
Approx. 7 kg (15 lbs.).

ACCESSORIES

Connector BNC–BNC PL43
Connector BNC–clips PL44

OPTIONAL ACCESSORIES

Probe Kit PN 32824. A passive probe kit with X1 and X10 attenuations. With X10 attenuation input impedance is 10MΩ/13.5pF.
Viewing Hood PN A1/32264.
Trolley Type TR4 A general purpose oscilloscope trolley.
Protective Carrying Case PN 3247.
A strong carrying case which completely encloses the oscilloscope with three thicknesses of padded material covering the front panel.
Tube Option The OS250 may be ordered with a long persistence c.r.t. (P7 phosphor).

Rack Mount Kit PN 33389
Adaptor BNC–binding post PN 26234

The OS250 block diagram is shown in Fig. 1. Inter connection of the printed circuit boards, controls, tube and associated components is shown in Fig. 6. Circuit diagrams are as follows:-

Fig. 3 Y1 and Y2 attenuators, pre-amplifiers, the main Y amplifier, beam switch and drive circuits.
Fig. 4 Timebase, X amplifier and trigger circuits.
Fig. 5 The power supply and tube network.

4.1 GENERAL

Referring to the block diagram (Fig.1) signals applied to the Y1 and Y2 input sockets pass into their respective attenuators and amplifiers. The VOLTS/CM switch controls the gain of the amplifier in the necessary 1 . 2. 5 sequence to cover the ranges from 5mV/cm to 0.2V/cm. Above this a ÷ 100 attenuator is introduced before the amplifier.

The fast electronic beam switch selects either the Y1 or the Y2 signal to be amplified further and passed to the Y deflection plates of the c.r.t.

A sample of each signal is taken and passed to the trigger switch, where slection of Y1, Y2 or Ext trig source is made. The selected signal is amplified and passed to the Schmitt trigger, where it is converted into fast negative-going pulses. The hold off circuit acts as a gate which is normally open to allow a trigger pulse to set the timebase bistable. The bootstrap ramp generator then begins to generate its linear ramp, which after passing through the X amplifier is applied to the cathode ray tube and drives the electron beam linearly across the tube face. A small portion of the signal from the ramp generator is fed back to the hold off circuit, shutting the gate to prevent any further pulses from the Schmitt trigger from reaching the timebase bistable during the ramp period. When the ramp has reached the necessary maximum level, the timebase bistable is reset, and the ramp is quickly returned to it's quiescent state. A time constant in the hold off circuit now holds the gate closed to inhibit another ramp from being initiated for a short period, until the ramp timing capacitor is discharged fully. Thus a ramp is generated at a rate set by the TIME/CM switch when the trigger signal reaches a predetermined level. This ramp sweeps the beam across the c.r.t. face, returns and waits for the next trigger point to be reached. The timebase bistable is connected to a blanking amplifier whose function is to turn on the electron beam during the sweep and blank it off during the fly back and subsequent waiting period.

At fast sweep rates for a dual trace display, the TIME/CM switch automatically selects the alternate sweep mode of control for the beam switch. At the end of each sweep the signal from the time-base bistable reverses the state of the beam switch bistable, causing alternate displays of the Y1 and Y2 signal on successive sweeps of the timebase. At slow sweep rates, the chop mode is selected, when the chop

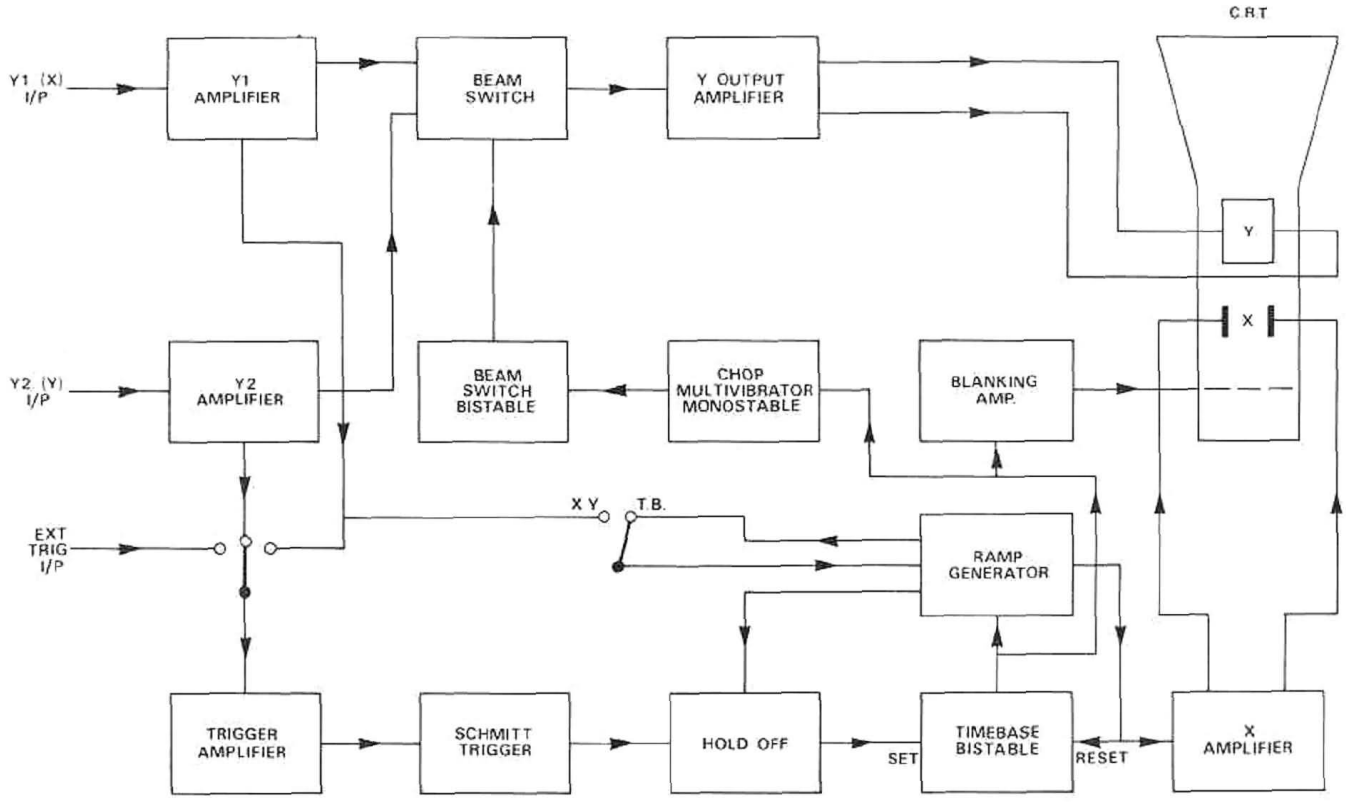

Fig. 1 Block diagram

multivibrator free runs independently, causing the beam to switch between Y1 and Y2 levels during the sweep. A signal from the multivibrator also blanks the trace during each switching transition. With Y1 or Y2 switched to the OFF position the beam switch bistable is locked to switch on the other channel.

In the X–Y mode, the signal from the Y1 amplifier, normally used for trigger, is passed via the ramp generator, which acts as a voltage follower, to drive the X plates while the beam switch selects Y2 to drive the Y plates. The beam blanking signal is not used.

4.2 THE Y AMPLIFIERS

The attenuator and pre-amplifier in the Y1 channel are identical to those in the Y2 channel. Accordingly, only the Y1 channel is described.

The input signal is applied to the front panel socket SKA and then to the 3 position slide switch S20, via R26. The switch selects AC or DC input coupling by including or by-passing C21 in the signal path. In the middle position of the switch, the input socket is disconnected, and the input of the attenuator is connected to ground through R27. The attenuator feeds into an impedance of 1MΩ (R29). The ÷ 100 attenuation is determined by the potential divider action of R20 in series with the parallel combination of R29 and R201. High frequency compensation of the attenuator is achieved by the a.c. potential divider C202 and C203; C202 is set for the correct ratio. C201 is adjusted to maintain constant input capacitance between divided and undivided ranges. This attenuator is used on the six higher voltage ranges i.e. 0.5V/cm – 20V/cm, dividing them down to 5–200mV/cm. Further selection of input sensitivity is carried out by gain switching within the amplifier, and is described later. Diodes D201 and D202 in conjunction with R28 protect the input up to 400 volts peak.

The input stage consists of TR201 and TR202, a matched pair of field effect transistors. The current in TR202 is self biased such that the potential drop across R205 equals the gate/source potential. This same current flows in TR201, which operates as a source follower on the input signal. As R207 equals R205 the base potential of TR203 always equals the input voltage on the gate of TR201. The signal is passed via emitter follower TR203 to the gain switching stage.

The grounded emitter transistor TR204 forms a shunt feedback amplifier with gain determined by the ratio of the feedback resistor R211 to the input resistor R40 in parallel with the resistor selected by the range switch as shown in Table 1. R202 (BALance) sets the base of TR203 to null the potential across R40 etc.

The signal from the collector of TR204 is passed via R214 to the base of TR205 which in conjunction with TR206 forms a long tail pair amplifier, the gain of which

Table 1.

Switch Setting	Attenuation	Resistor Used	Amplifier Gain
5mV	÷1	R40+R45	5
10mV	÷1	R40+R44	2.5
20mV	÷1	R40+R43	1.25
50mV	÷1	R40+R42	0.5
100mV	÷1	R40+R41	0.25
200mV	÷1	R40 only	0.125
500mV	÷100	R40+R45	5
1V	÷100	R40+R44	2.5
2V	÷100	R40+R43	1.25
5V	÷100	R40+R42	0.5
10V	÷100	R40+R41	0.25
20V	÷100	R40+ only	0.125

is set by R217 and R223. The collector current of TR205 feeds into the trigger section of the timebase and 'X' amplifier circuit (fig.4). Potentiometer R52 provides a variable current via R219 into the collector circuit of TR206, to produce 'Y' shift. The bases of TR206 (Y1) and TR216 (Y2) are driven from the collector circuit of TR217 which being connected in a similar manner to TR204 and TR214 provides the correct bias and compensation for supply and temperature variations.

The beam switch, consists of diodes D203, D204, D206 and D207, with their associated drive circuitry and is described in detail in section 4.3. It selects the collector current of TR206 or of TR216 to pass through D205 and R223. The voltage developed across R223 consists of a fixed d.c. component, a variable d.c. component (Y shift) and the signal and is applied to the base of TR207, a common emitter amplifier. The emitter circuit includes potentiometer R222, to set the gain of the stage and hence the overall gain of the amplifier. The signal from the collector of TR207 is passed to the base of TR208, which with TR209, TR210 and TR211 forms the output cascode stage. TR208 and TR209, is a long-tail pair, which converts the input signal voltage to differential output current; its gain is determined by emitter resistors R234 and R236, with high frequency gain set by networks R232/C211/C212, R233/C213 and R236/C236. The collector currents of TR208 and TR209 flow into the emitters of the grounded base transistors TR210 and TR211 to develop the differential output voltage across the load resistors R230/R240 to drive the c.r.t. deflection plates. Inductors L201 and L202 are included to improve the high frequency response.

4.3 THE BEAM SWITCH

The cathode of D203 is supplied with a 6 volt positive-going square wave from the bistable TR218/TR219. When the waveform is "high", D203 is biased off and the collector current of TR206 passes through D204 into the output amplifier. During the low state of the waveform D203 conducts, passing this current to ground through TR219. As diodes D203 and D207 are fed with complimentary waveforms, when the current from TR206 passes to the output amplifier, that from TR216 is shunted to ground and vice-versa.

Bistable TR218/TR219 is switched with pulses from TR220/TR221, the chop multivibrator.

This emitter coupled circuit free runs at approx. 500kHz on TIME/CM settings from 0.5s to 1 ms,† causing the bistable to operate the beam switch at 250kHz. In addition to driving the bistable, an output from the collector of TR221 is fed to the cathode of the c.r.t. to blank the trace during the beam switching transitions. The mark/space ratio of the multibrator is approx. 1:4, causing the trace to be blanked for one fifth of each switching period.

At faster TIME/CM settings of 0.5 ms†† to 1μs, the lower end of R292 is taken to −20V by a contact on the timebase switch biasing off TR221, and preventing oscillation. The circuit now acts as a monostable, triggered via C220 at the end of each sweep by pulses from the timebase bistable, each output pulse reversing the beam switch bistable and rapidly blanking the trace.

For single trace operation, the Y shift control on the channel not required is rotated fully anti-clockwise to operate the OFF switch. In this position, the switch S27 or S28 is closed, connecting the cathode of its associated diode to the negative line. This biases off the relevant transistor in the bistable. Thus when Y1 is turned off, S27 closes, biasing off TR218; TR219 turns on and sinks the current from Y1 channel to ground through D203. A reversal occurs when Y2 is turned off. In the X-Y mode, both shift controls are set to the on position; a contact on the TIME/CM switch in parallel with S27 is used to bias TR218 off, allowing Y2 signals only to reach the Y output stage.

* 4.4 THE TRIGGER CIRCUITS (Fig. 4)

The collector currents from TR205 and TR215 in the Y amplifier pass to the timebase printed circuit board into R108 and R109 respectively. In series with R108 is R110 shunted by C101, a collector load network used when X-Y mode is selected. External trigger signals appear across R107, and these, together with those across R108 and R109 pass to the trigger selector switch. The selected trigger signal is amplified by TR107 and passed to the coupling switch. Here, high pass, direct and low pass networks provide the required ACF—AC—TV filtering. Trigger level and slope selection operations are performed by long-tail pair amplifier TR101/TR102. The signal is applied to either input as determined by the slope selector switch, the other input being grounded via C121. The Trigger Level control, R10, provides a variable d.c. bias at both inputs, which the amplifier sums with the signal. The output at the collector of TR102, consisting of an alternating signal voltage superimposed on a d.c. level, passes to the Schmitt Trigger TR103/TR104, where fast negative edges are generated as the input signal crosses the circuit threshold.

4.5 THE TIMEBASE BISTABLE AND RAMP GENERATOR

The ramp generator comprises TR111, TR112 and TR113 as cascaded emitter follower stages, with bootstrap feedback action provided from the cathode of Zener diode D104. This feedback maintains constant voltage across the VARIABLE TIME control R11, R148, R147 and the timing resistor selected by the TIME/CM switch. This constant voltage drop, independant of actual voltage level produces a constant current to linearly charge the timing capacitor, also selected by the TIME/CM switch. The VARIABLE TIME control provides fine adjustment of the timing current, and hence sweep time, by varying the feedback voltage applied to the timing resistor.

In the quiescent condition of the timebase bistable, TR108 is on, TR109 is off and clamp transistor TR110, which shunts the timing capacitor, is saturated. A negative-going pulse from the Schmitt Trigger is coupled via C111 and D102 to turn off TR108. TR109 turns on, thus turning off TR110. The clamp is removed, allowing the timing capacitor to charge, producing the linear ramp. As the emitter of TR113 rises, a feedback voltage, via D105, R143 and R133 biases off D102 to prevent any further pulses reaching the bistable. Connected to the junction of R133/R143 is the HOLD OFF capacitor which now charges positive. When the ramp reaches its final amplitude, a rise of approximately 10V, feedback from the junction of R151/R149 is applied to the base of TR108, turning it on. The bistable reverts to its initial state allowing TR110 to turn on, rapidly discharging the timing capacitor and returning the ramp to its quiescent level. The hold off capacitor, which was charged to a positive voltage during the ramp, now slowly discharges through R143 and R153, until it is caught by D105. Only then is D102 biased for the next trigger pulse to initiate the next sweep.

An output is taken from the ramp generator via R155 to SKE, the RAMP OUT socket, on the front panel.

† 2ms. on OS250TV.

†† 1 ms. on OS250TV.

* See OS250TV Supplement.

4.6 BRIGHT LINE CIRCUIT

When sufficient trigger signal is available, the square wave from the collector of TR104 passes through R127/C104, where restoration by D101 produces a negative going signal with respect to the negative rail. This negative signal on the base of TR105 is integrated by R124/C107 to produce a d.c. bias sufficient to hold off TR106. In this condition the circuit has no effect on timebase operation. However, when the triggering signal falls below the required level, the Schmitt trigger ceases to operate, removing the signal from D101. The voltage on the emitter of TR105 rises to approximately one volt above the negative line, turning on TR106. R177 is now effectively connected between the negative rail and the cathode of D102. It rapidly discharges the hold off capacitor below the normal quiescent level to a point where D102 conducts, turning TR108 off and initiating a sweep. At the end of the ramp, the charge on the hold off capacitor is again removed by R177/R143 and another ramp begins. These consecutive sweeps produce the bright line display. When the "PULL BRIGHT LINE OFF" control is operated, switch S10 closes, effectively shorting the base and emitter of TR106, holding it off; in this condition a ramp is only generated after the arrival of a trigger pulse.

4.7 THE X OUTPUT AMPLIFIER

The ramp or X-Y signal at the emitter of TR113 passes through R156 to the base of TR114, which with TR117 forms a long tail pair. Gain switching is carried out in the emitter circuit by selection of one of two resistance paths, with gains set by R169(X1) and R16 R162(X10). In timebase mode, the PULL X10 switch S11 can be operated in order to expand the trace length ten times. In the X-Y mode contacts on the TIME/CM switch, in parallel with S11, close to select this higher gain setting automatically. An X SHIFT voltage is produced at the base of TR117 by R12. The signals on the collectors of TR111 and TR117 are applied to the differential output amplifier, TR115 and TR116. Signals from the collectors of these two transistors drive the horizontal deflection plates of the c.r.t.

4.8 X-Y Mode

In this mode, signals are applied to both Y1 and Y2 input sockets; Y2 is routed through the beam switch to the Y deflection plates in the normal manner. Y1 is routed through the ramp generator, now acting as a high impedance unity gain buffer, and into the X output stage.

Signals entering Y1 channel pass through the attenuator and gain switching stage, as described previously. Current from TR105 passes to the X board, while that in TR206 is shunted to ground through D203. The current from TR205 develops a voltage across the series connection of R110,R108. This voltage is level-shifted by R144/R146 to the base of TR111. In the X-Y mode, both timing resistors and capacitors are switched out of circuit, consequently TR111, TR112 and TR113 merely act as emitter followers which provide buffering between the level-shift resistors and the X output amplifier.

When this mode is selected, a contact on the TIME/CM S14(a) switch connects the cathodes of D106 and D107 to the negative line. The current drawn through D106 and R138 turns off TR108 and consequently TR110, and removes blanking. (See section 4.11)

Current through D107 controls the state of the beam switch bistable. (See section 4.3)

4.9 POWER SUPPLIES (Fig. 5)

All power supplies are derived from transformer T1. The primary winding can be connected to accept six supply voltage ranges, as shown in fig. 2, on the inside of the top cover.

The transformer secondary has four windings developing the following r.m.s. voltages; 6.3V, 44V (centre tapped), 140V and 1000V.

The 6.3V winding supplies the c.r.t. heater.

The 44V a.c. is rectified by MR32 and smoothed by C33/C34 to form the unstabilised +26V and −26V d.c. lines. These voltages are fed to series regulators to provide the stabilised +20V and −20V lines. As both regulators operate in an identical manner, only one will be described.

The base of series pass transistor, TR32, is fed from the output of the high gain error amplifier formed by TR305/TR306. This amplifier compares the zener reference voltage from D316 with the voltage at the junction of R310/311, a potential divider connected between the emitter of TR32 and ground. As this emitter supplies the +20V line, any fluctuations in the line voltage appear at the base of TR306 where they are amplified and inverted. This signal is then fed to the base of TR32 to correct the error, thus maintaining a constant output voltage. Resistor R309, in series with the collector of TR32, drops a voltage which is proportional to the output current. Under normal conditions, this voltage drop is less than that across R307, biasing off D310. As the output current rises above the safe maximum, D310 turns on, taking the current in R307 away from the emitter of TR305. This causes a drop in voltage at the collector of TR306 and hence on the base and emitter of TR32, limiting the current to a safe value.

The voltage from the 140V winding is rectified by MR31 and smoothed by C31 to form the unstabilised 170V line.

The 1000V winding energises both the −1.2kV and +2.4kV supplies. Half wave rectification of the negative half cycle by D301 produces the negative line, while voltage doubling by D302/D303 produces the positive. Stabilisation of both lines against supply variation is achieved as follows. One end of the 1000V winding feeds the diodes mentioned above. The other end passes to ground through bridge rectifier MR301. The alternating current in the winding passes through the rectifier as direct current via R338 and TR301, developing a smooth direct voltage across C315. This voltage, controlled by the conduction of TR301, forms a threshold above which the alternating voltage applied to the bridge must rise before current can flow. As this threshold must be reached on both positive and negative excursions of the supply waveform, the overall effect is to take the middle out of the sine wave, thus reducing its voltage. This controlled voltage is rectified to produce the E.H.T. supplies. R322 feeds a negative current into the base of TR302, proportion to the peak value of the regulated waveform. This current is balanced by a reference current from the + line fed via R319 and SET E.H.T. potentiometer R320. The voltage at the summing point of the two currents appears at the emitter of TR302 and controls the current flow through D304, which in turn controls the conduction of TR301. As it is this conduction which controls the alternating voltage from which the feedback is derived, a closed loop circuit is formed. Variations in the magnitude of voltage across the 1000V winding either increases or decreases the voltage on the −1.2kV line. Feedback from this line is compared with a reference and the conduction of TR301 is varied accordingly to bring the line back to its correct voltage. As the +2.4kV line is derived from the same stabilised source as the −1.2kV, it also remains constant.

4.10 CALIBRATOR (Fig. 5)

The 1V ±2% square wave at the CAL 1V socket, SKD, is produced by TR307, on the power supply board. Current for the base of this transistor is supplied via R305 and D311. The anode of D312, is connected to the junction of these two components, its cathode being taken to one of the 22V windings. On positive excursions of the winding, D312 is biased off, and the current through R305, D311 saturates TR307. During negative excursions, D312 conducts, and the current in R305 passes through the transformer winding. In this condition D311 and TR307 are turned off. The result is a square wave on the collector of TR307, at line frequency, with amplitude set by adjustment of R304.

4.11 BLANKING

The signal which blanks the c.r.t. when a sweep is not occurring is produced by TR308. The base of this transistor is fed via R135/C118 from the collector of TR108 in the timebase bistable. When TR108 is on, no current flows in R135, thus TR308 is off and its collector is at approximately 70V, as determined by R335, R336 and R337. This voltage is fed to the beam blanking plates of the c.r.t., pin 5, and blanks the trace. As TR108 turns off to initiate a sweep, the current in R135 turns TR308 on; its collector voltage falls to about 3V, where it is held by the action of the forward biased diode, D313. Under this condition c.r.t. blanking is removed. Blanking is not effected in the X-Y mode as TR108 in the timebase bistable is permanently off.

When dual trace operation is selected, a pulse is coupled via C314, from the collector of TR221 into the cathode of the c.r.t. in order to blank the trace during the switching transition.

Z Modulation

Signals applied to SKF on the rear panel pass via C313 to the grid of the c.r.t. where they produce trace intensity modulation.

4.12 TUBE NETWORK

The cathode of the c.r.t. draws current from the −1.2kV line through the BRILLIANCE control, R33. Clockwise rotation of this control decreases the grid potential, and hence varies the tube conduction from cut off to maximum. Electrons emitted from the cathode are focussed into a narrow beam by potentials on the focus and astigmatism electrodes. These potentials are approximately −850V and +80V, controlled by R34 and R332 respectively.

When a positive potential is applied to the blanking plates, the electron beam is deflected to one side of the tube, thus preventing the electrons striking the tube face. The geometry control R333 varies the potential on an electrostatic shield placed between the X and Y deflector plates to minimise interaction. After deflection by the X and Y plates, the electron beam is accelerated by the PDA potential of +2.4kV, to strike the phosphor coated tube face at high velocity, and produce a display.

Component List and Illustrations — Section 6

ABBREVIATIONS USED FOR COMPONENT DESCRIPTIONS

RESISTORS

CC	Carbon Composition	½W	10%	unless otherwise stated
CF	Carbon Film	⅛W	5%	unless otherwise stated
MO	Metal Oxide	½W	2%	unless otherwise stated
MF	Metal Film	¼W	1%	unless otherwise stated
WW	Wire Wound	6W	5%	unless otherwise stated
CP	Control Potentiometer		20%	unless otherwise stated
PCP	Preset Potentiometer Type MPD, PC		20%	unless otherwise stated

CAPACITORS

CE(1)	Ceramic		+ 80% − 25%	
CE(2)	Ceramic	500V	± 10%	unless otherwise stated
SM	Silver Mica			
PF	Plastic Film		± 10%	unless otherwise stated
PS	Polystyrene			
PE	Polyester		± 10%	unless otherwise stated
PC	Polycarbonate			
E	Electrolytic (aluminium)		+ 50% − 10%	
T	Tantalum		+ 50% − 10%	

Component List and Illustrations

Y AMPLIFIER

Ref	Value	Description	Tol %±		Part No.
RESISTORS					
R 201	10kl	MF	1		26338
R202	22k	CP			A4/32894
R203	18k	CF			21811
R204	470	CF			21797
R205	470	CF			21797
R206	39k	CF			28728
R207	470	CF			21797
R208	470	CF			21797
R209	6k8	CF			21807
R210	2k2	CF			21802
R211	2k	MO			26731
R212	18	CF			28709
R213	6k8	MO			28796
R214	220	CF			21796
R215	3k3	CF			21803
R216	3k3	CF			21803
R217	180	MO			26744
R218	180k	CF			21822
R219	12k	CF			21810
R220	10	CF			21793
R221	47	CF			28714
R222	100	PCP			28520
R223	330	CF			28721
R224	12k	CF			21810
R225	56	CF			28715
R226	3k3	CF	5	½W	18556
R227	1k2	CF			21800
R228	680	CF			28723
R229	10	CF			21793
R230	3k	MO	5	6W	33212
R231	47	CF			28714
R232	47	CF			28714
R233	22k	CF			21812
R234	120	CF			28718
R235	820	MO	5	4W	33212
R236	15k	CF			28727
R237	180	CF			21795
R238	47	CF			28714
R239	10	CF			21793
R240	3k	MO	5	6W	33212
R241	1k2	CF			21800
R242	2k7	CF			28726
R243	10	CF			21793
R244	560	CF			21798
R245	2k2	CF			21802
R246	2k2	CF			21802
R247	2k2	CF			21802
R248	2k2	CF			21802
R249	47	CF			28714
R250	10	CF			21793
R251	10kl	MF	1		26338
R252	22k	CP			A4/32894
R253	18k	CF			21811
R254	470	CF			21797
R255	470	CF			21797
R256	39k	CF			28728
R257	470	CF			21797
R258	470	CF			21797
R259	6k8	CF			21807
R260	2k2	CF			21802
R261	2k	MO			26731
R262	18	CF			28709
R263	6k8	MO			28796
R264	220	CF			21796
R265	3k3	CF			21803
R266	3k3	CF			21803
R267	180	MO			26744
R268	180k	CF			21822
R269	12k	CF			21810
R270	10	CF			21793
R271	6k8	MO			28796
R272	47	CF			28714
R273	2k	MO			26731
R274	2k2	CF			21802
R275	10	CF			21793
R276	22k	CF			21812
R277	1k8	CF			28725
R278	2k7	CF			28726
R279	1k8	CF			28725
R280	15k	CF			28727
R281	22k	CF			21812
R282	22k	CF			21812
R283	15k	CF			28727
R284	22k	CF			21812
R285	1k	CF			21799
R286	3.9k	CF			21804
R287	27k	CF			21813
R288	1k8	CF			28725
R289	4k7	CF			21805
R290	6k8	CF			21807
R291	10k	CF			21809
R292	27k	CF			21813
R293	33k	CF			21814
CAPACITORS					
C201	6pF	Trimmer			25750
C202	6pF	Trimmer			25750
C203					
C204	.01µF	CE(2)	25	250V	22395
C205	.01µF	CE(2)	25	250V	22395
C206	39pF	CE(2)			22371
C207	.01µF	CE(2)	25	250V	22395
C208	39pF	CE(2)			22371
C209	10/40pF	Trimmer			29483
C210	1000pF	CE(2)			22387

Y AMPLIFIER (Cont.)

Ref	Value	Description	Tol %±		Part No.
C211	10/40pF	Trimmer			29483
C212	220pF	PS	10	125V	11587
C213	270pF	CE(2)			22380
C214	68pF	CE(2)			22374
C215	.1μF	CE(1)		30V	19647
C216					
C217	560pF	CE(2)			22384
C218	68pF	CE(2)			22374
C219	.01μF	CE(2)	25	250V	22395
C220	47pF	CE(2)			22372
C221	6pF	Trimmer			25750
C222	6pF	Trimmer			25750
C224	.01μF	CE(2)	25	250V	22395
C225	.01μF	CE(2)	25	250V	22395
C226	47pF	CE(2)			22372
C227	.01μF	CE(2)	25	250V	22395
C228	27pF	CE(2)			22369
C229	27pF	CE(2)			22369
C230	.01μF	CE(2)	25	250V	22395
C231	15pF	CE(2)			22366
C232	15pF	CE(2)			22366
C233					
C234	.01μF	CE(2)	25	250V	22395
C235	.01μF	CE(2)	25	250V	22395
C236	47pF	CE(2)			22372
C237	39pF	CE(2)			22371
C238	100pF	CE(2)			22376
C239	.01μF	CE(2)	25	250V	22395
C240	.01μF	CE(2)	25	250V	22395
C241	.1μF	CE(1)		30V	19647
C242	.1μF	CE(1)		30V	19647
C243	.1μF	CE(1)		30V	19647
C244	330pf	CE(2)			22381
C245	0.1μF	CE(1)		30V	19647
C246	68pF	CE(2)			22374

TRANSISTORS

TR201, TR202	AE23 Matched Pair	A32957
TR203	2N3906	21533
TR204	2N3904	24146
TR205	2N3640	31781
TR206	2N3640	31781
TR207	2N3904	24146
TR208	2N2369	23307
TR209	2N2369	23307
TR210	BF380	32902
TR211	BF380	32902
TR212, TR213	AE23 Matched Pair	A32957
TR214	2N3904	24146
TR215	2N3640	31781
TR216	2N3640	31781
TR217	2N3904	24146
TR218	2N2369	23307
TR219	2N2369	23307
TR220	BC212	29327
TR221	BC212	29327
TR222	2N3906	21533

DIODES

D201	IN3595	29330
D202	IN3595	29330
D203	IN4148	23802
D204	IN4148	23802
D205	IN4148	23802
D206	IN4148	23802
D207	IN4148	23802
D208	IN4148	23802
D209	IN4148	23802
D210	IN4148	23802
D211	IN4148	23802
D212	IN4148	23802
D213	IN4148	23802
D214	IN4148	23802
D215	IN3595	29330
D216	IN3595	29330

MISCELLANEOUS

L201	33μH		33204
L202	33μH		33204
L203		Bead Ferrite FX1115	4442
L204		Bead Ferrite FX1115	4442

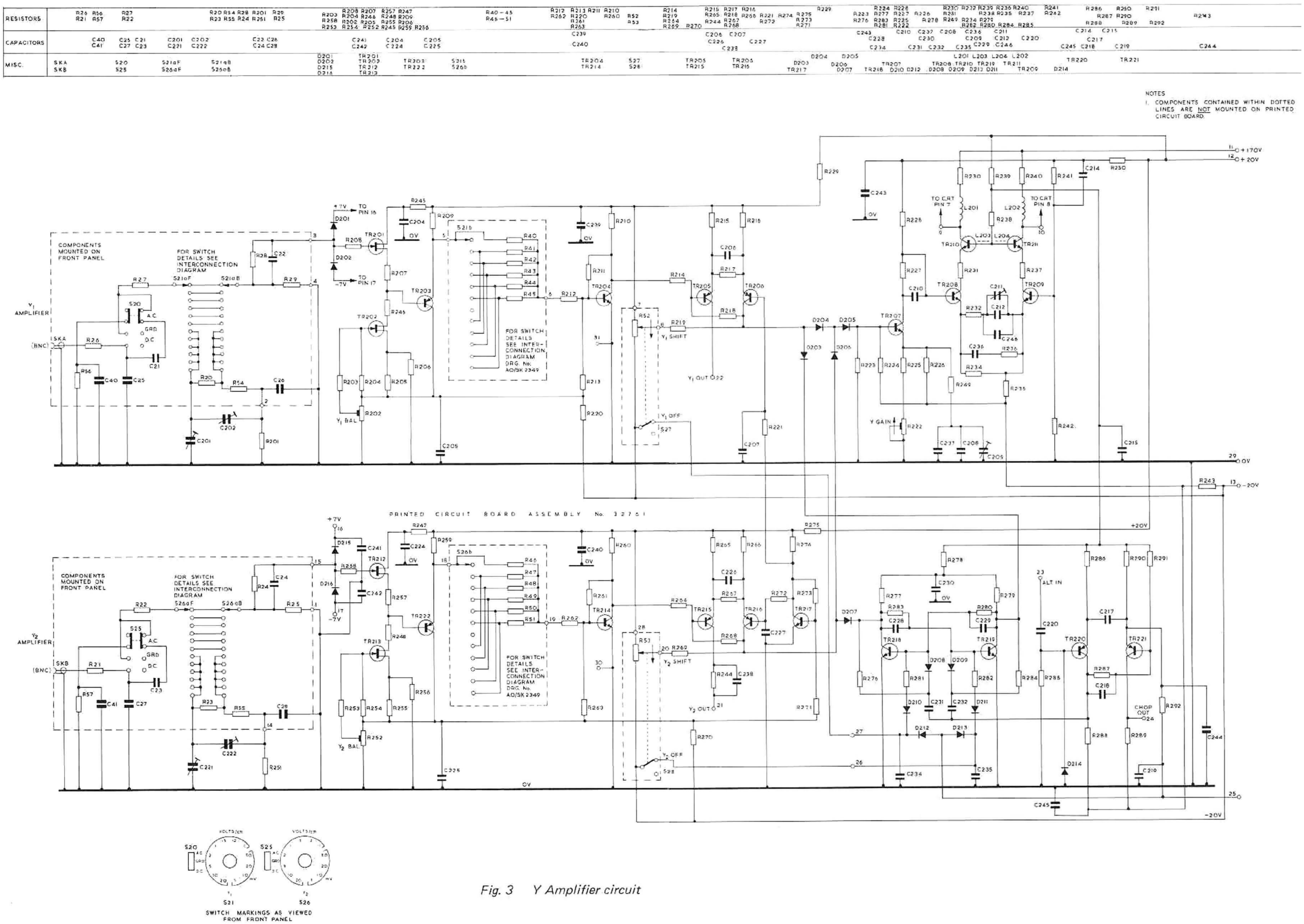

Fig. 3 Y Amplifier circuit

Component List and Illustrations — Section 6

TIMEBASE AND X AMPLIFIER

Ref	Value	Description	Tol %±		Part No.
RESISTORS					
R101	22k	CF			21812
R102	22k	CF			21812
R103	1k2	CF			21800
R104	47	CF			28714
R105	10	CF			21793
R106	100k	CF	5	1W	19061
R107	560	CF			21798
R108	220	CF			21796
R109	220	CF			21796
R110	620	MO			22485
R111	10	CF			21793
R112	390	CF			28722
R113	1k2	CF			21800
R114	3k3	CF	5	½W	18556
R115	1k2	CF			21800
R116	1k2	CF			21800
R117	10	CF			21793
R118	47	CF			28714
R119	100k	CF			21819
R120	6k8	CF			21807
R121	270	CF			28720
R122	1k5	CF			21801
R123	3k3	CF			21803
R124	1M	CF			31840
R125	100	CF			21794
R126	4k7	CF			21805
R127	10k	CF			21809
R128	2k2	CF			21802
R129	120	CF			28718
R130	1k	CF			21799
R131	1k	CF			21799
R132	2k7	CF			28726
R133	1k	CF			21799
R134	12k	CF			21810
R135	18k	CF			21811
R136	3k9	CF			21804
R137	3k9	CF			21804
R138	10k	CF			21809
R139	47k	CF			21815
R140	47k	CF			21815
R141	100k	CF			21819
R142	10k	CF			21809
R143	1k	CF			21799
R144	1k5	CF			21801
R145	100k	CF			21819
R146	15k	CF			28727
R147	2M2	CC			1180
R148	68k	CF			21816
R149	2k7	CF			28726
R150	100	CF			21794
R151	1k2	CF			21800
R152	56k	CF	5	1W	19058
R153	27k	CF			21813
R154	3k9	CF			21804
R155	18k	CF			21811
R156	100	CF			21794
R157	56k	CF	5	1W	19058
R158	220	CF			21796
R159	2k2	CF			21802
R160	10k	MO	5	4W	29481
R161	100	CF			21794
R162	100	PCP			28520
R163	2k	MO			26731
R164	1k8	CF			28725
R165					
R166	1k5	CF			21801
R167	100	CF			21794
R168	10k	MO	5	4W	29481
R169	1k	PCP			26870
R170	2k	MO			26731
R171	56k	CF	5	1W	19058
R172	1k8	CF			28725
R173	100	CF			21794
R174	1k8	CF			28725
R175	1k8	CF			28725
R176	10	CF			21793
R177	10k	CF			21809
R178	27	CF			28711
R179	270k	CF			32356
R180					
CAPACITORS					
C101	100pF	CE(2)			22376
C102	.01µF	CE(2)	25	250V	22395
C103	10µF	E		25V	32180
C104	.01µF	CE(2)	25	250V	22395
C105	.01µF	CE(2)	25	250V	22395
C106	33pF	CE(2)			22370
C107	.47µF	CE(1)		3V	35352
C108	33pF	CE(2)			22370
C109	270pF	CE(2)			22380
C110	.1µF	CE(1)		30V	19647
C111	27pF	CE(2)			22369
C112	22µF	E		25V	32181
C113	.47µF	CE(1)		3V	35352
C114					
C117	27pF	CE(2)			22369
C118	27pF	CE(2)			22369
C119	4700pF	CE(2)	25	500V	22393
C120	.01µF	CE(2)	25	250V	22395
C121	100pF	CE(2)			22376
C122	27pF	CE(2)			22369
C123	22pF	CE(2)			22368
C128	180pF	PS	5	125V	33343
C129	10pF	CE(2)			22364

Component List and Illustrations — Section 6

TIMEBASE AND X AMPLIFIER (Cont.)

Ref	Value	Description	Tol %±	Part No.
TRANSISTORS				
TR101		2N2369		23307
TR102		2N2369		23307
TR103		2N2369		23307
TR104		2N2369		23307
TR105		BC212		29327
TR106		BC182B		33205
TR107		BC182B		33205
TR108		2N2369		23307
TR109		2N2369		23307
TR110		2N2369		23307
TR111		BC212		29327
TR112		BC212		29327
TR113		BC182B		33205
TR114		BC212		29327
TR115		BF258		31490
TR116		BF258		31490
TR117		BC212		29327
DIODES				
D101		IN3595		29330
D102		IN4148		23802
D103		IN4148		23802
D104	8V2	ZENER	5	3798
D105		IN4148		23802
D106		IN4148		23802
D107		IN4148		23802
D108		IN4148		23802
D109		IN4148		23802
D110		IN4148		23802

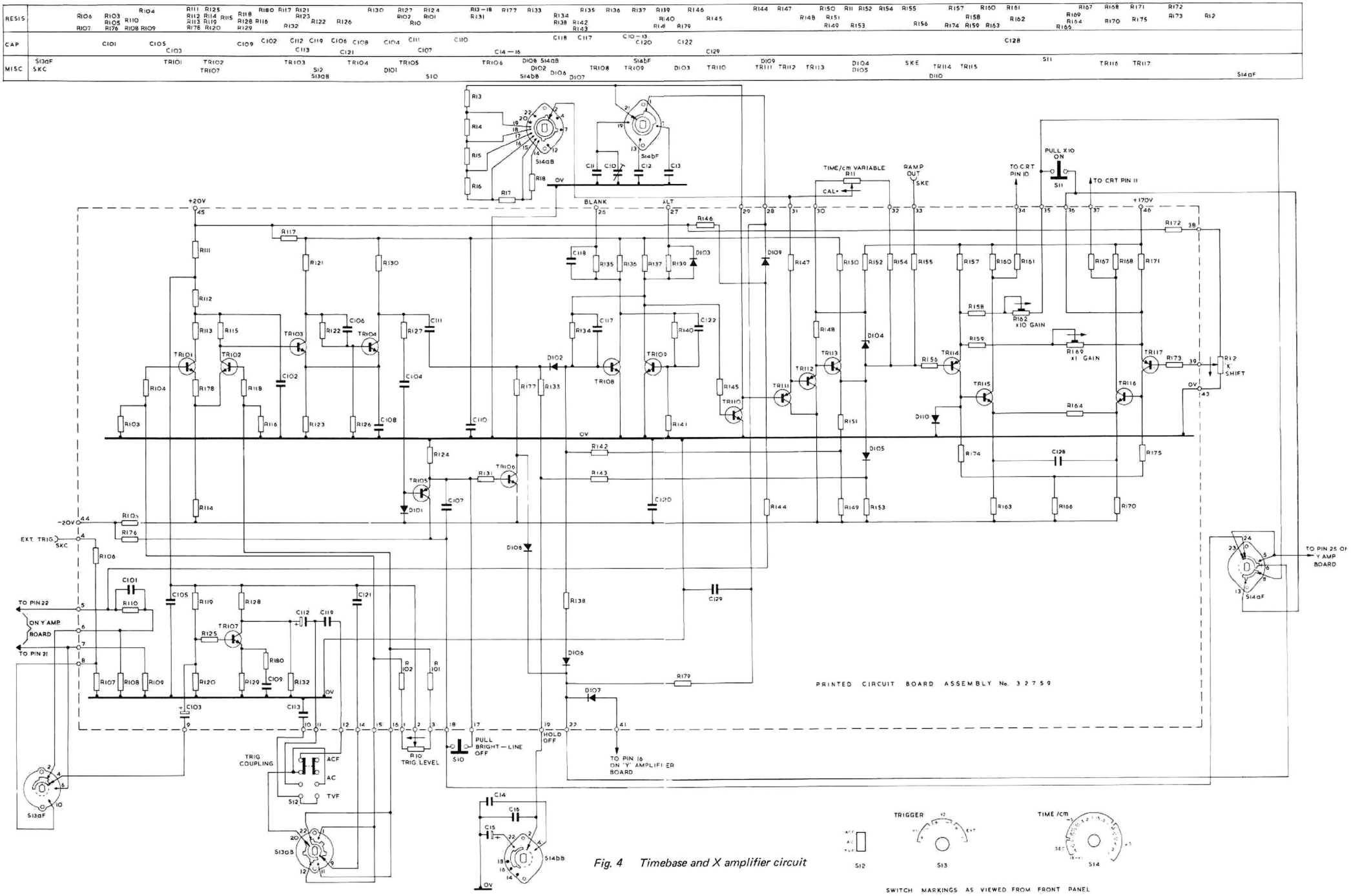

Fig. 4 Timebase and X amplifier circuit

Component List and Illustrations — Section 6

POWER SUPPLY

Ref	Value	Description	Tol %±		Part No.
RESISTORS					
R301	5k6	CF			21806
R302	1k	CF			21799
R303	8k2	CF			21808
R304	10k	PCP			28525
R305	100k	CF			21819
R306	47k	CF			21815
R307	82	CF			28717
R308	1k	CF			21799
R309	5R6	CF	5	½W	33210
R310	2k2	CF			21802
R311	1k3	CF			33338
R312	15k	CF			28727
R313					
R314	5R6	CF	5	½W	33210
R315	82	CF			28717
R316	2k2	CF			21802
R317	1k3	CF			33338
R318	47k	CF			21815
R319	43k	MO			28813
R320	10k	PCP			28525
R321	1M5	CC			7016
R322	3M3	CF	5	2W	29482
R323	2M2	CC			1180
R324	47k	CC			2933
R325					
R326	100k	CF			21819
R327	47k	CF			21815
R328	4M7	CC			597
R329	270k	CF			32356
R330					
R331	IM5	CC			7016
R332	220k	PCP			29363
R333	470k	PCP			28529
R334	100k	CF			21815
R335	27k	CF	5	2W	33211
R336	15k	CF	5	½W	18564
R337	22k	CF	5	½W	18566
R338	4k7	CC			3427
R339	2M2	CC			1180
R340					
R341	2M2	CC			1180
R342	2M2	CC			1180
CAPACITORS					
C301	4µF	E		450V	23599
C302	4µF	E		450V	23599
C303	4µF	E		450V	23599
C304	4µF	E		450V	23599
C305	.01µF	CE(2)	25	1.5kV	23603
C306	5000pF	CE(1)		3kV	1514
C307	5000pF	CE(1)		3kV	1514
C308	5000pF	CE(1)		3kV	1514
C309	4µF	E		450V	23599
C310	4µF	E		450V	23599
C311	4µF	E		450V	23599
C312	4µF	E		450V	23599
C313	.02µF	CE(1)		1.5kV	25223
C314	470pF	CE(2)	20	1.5kV	33207
C315	4µF	E		450V	23599
C316	4.7µF	E		63V	32195
C317	.01µF	CE(2)	25	250V	22395
C318/9	.01µF	CE(2)	25	250V	22395
TRANSISTORS					
TR301		MPS U10			32924
TR302		BC 182B			33205
TR303		BC 182B			33205
TR304		BC212			29327
TR305		BC212			29327
TR306		BC182B			33205
TR307		2N 2369			23307
TR308		2N 5831			33209
MR301		WO4			29367
DIODES					
D 301		MR995A			32903
D302		MR995A			32903
D303		MR995A			32903
D304		IN 4007			52337
D305		IN 4148			23802
D306		IN 4148			23802
D307		IN 4148			23802
D308		IN 4148			23802
D309		IN 4148			23802
D310		IN 4148			23802
D311		IN 4148			23802
D312		IN 4148			23802
D313		IN 4148			23802
D314		IN 4148			23802
D315	6V8	ZENER	5		4666
D316	6V8	ZENER	5		4666
D317		IN 4148			23802

RESISTORS	R306 R318 R307 R309 R310 R311 R317 R315 R314 R316 R304 R303 R305 R301 R302 R341 R342 R336 R339 R335 R338 R337 R323 R332 R333 R312 R321 R320 R319 R322 R334 R324 R328 R331 R329 R326 R327
CAPACITORS	C317 C318 C305 C306 C307 C315 C308 C316 C301~304 C309~312 C313 C314
MISC.	D308 D309 D306 D305 TR305 TR306 D316 D315 TR303 TR304 D310 D307 TR307 D311 D312 MR301 D303 D302 TR308 D313 TR301 D304 D301 TR302 D314 D317

NOTE.

1. COMPONENTS NOT ENCLOSED WITHIN THE DOTTED AREA ARE CALLED FOR ON INTERCONNECTION DIAGRAM SK.2349.

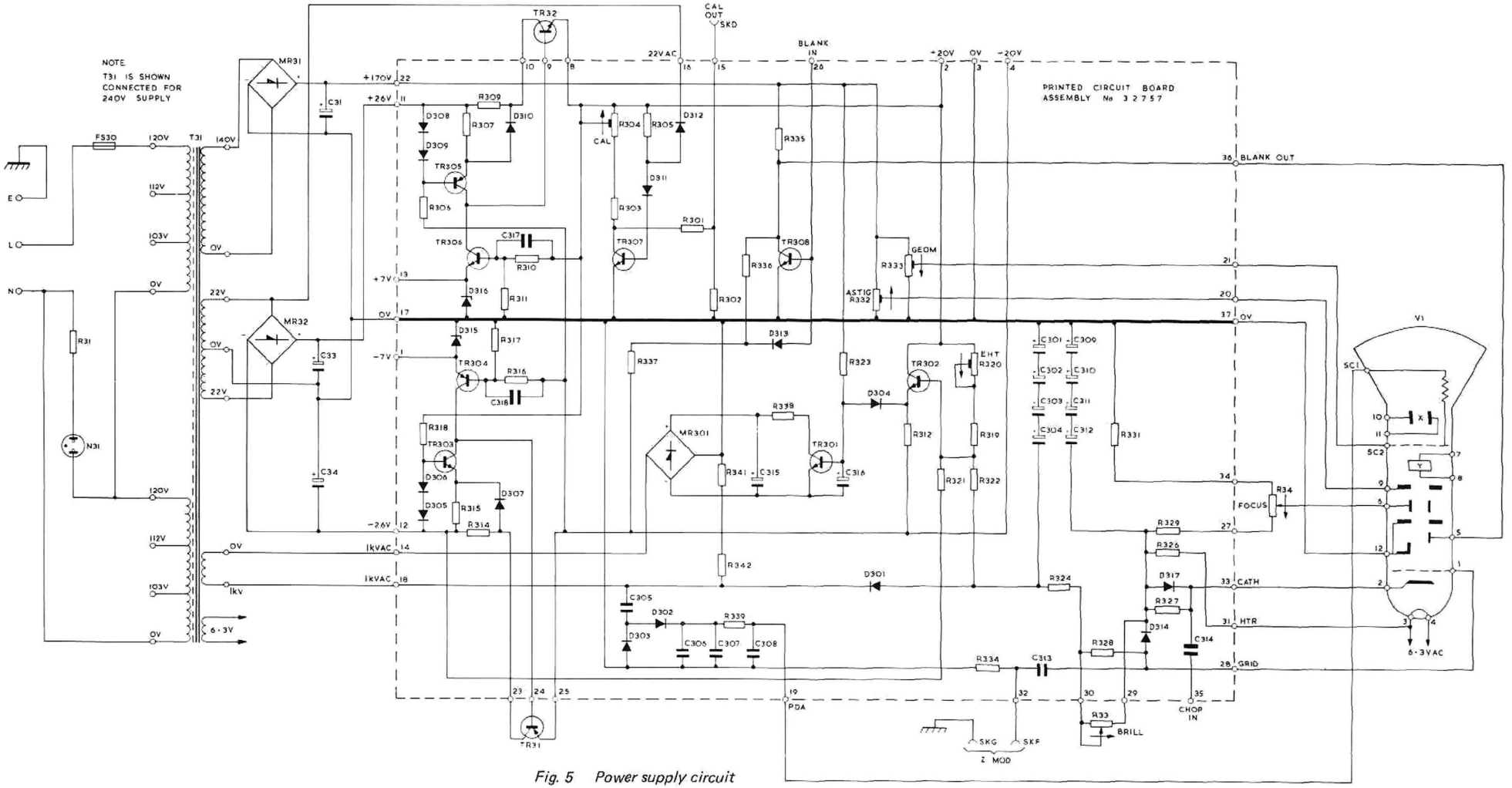

Fig. 5 Power supply circuit

Component List and Illustrations

Section 6

INTERCONNECTION

Ref	Value	Description	Tol %±		Part No.
RESISTORS					
R10	100k	CP With S10			A4/32897
R11	10k	CP With S11			A4/32898
R12	2k2	CP			A4/32896
R13	100k	MF	1		29476
R14	100k	MF	1		29476
R15	301k	MF	1		29477
R16	499k	MF	1		26342
R17	1M	MF	1		26346
R18	3M01	MF	1		29478
R20	990k	MF	1		26345
R21	22	CF			28710
R22	22	CF			28710
R23	990k	MF	1		26345
R24	470k	CC			4906
R25	1M	MF	1		26346
R26	22	CF			28710
R27	22	CF			28710
R28	470k	CC			4906
R29	1M	MF	1		26346
R31	68k	CF			21816
R33	220k	CP With S30			A4/32899
R34	1M	CP			A4/32893
R40	16k	MF	1		29361
R41	15k8	MF	1		33291
R42	5k23	MF	1		33290
R43	1k72	MF	1		33289
R44	787	MF	1		33288
R45	360	MF	1		33287
R46	16k	MF	1		29361
R47	15k8	MF	1		33291
R48	5k23	MF	1		33290
R49	1k72	MF	1		33289
R50	787	MF	1		33288
R51	360	MF	1		33287
R52	22k	CP With S27			A4/32895
R53	22k	CP With S28			A4/32895
R54	22	CF			28710
R55	22	CF			28710
R56/57	330k	CC			4408
CAPACITORS					
C10	6/25pF	Trimmer			23593
C11	68pF	SM	5		4513
C12	.01µF	PS	1		24886
C13	1µF	PC	2		33206
C14	.047µF	CE(1)		30V	2793
C15	4.7µF	E		63V	32195
C16	1000pF	CE(2)			22387
C21	.1µF	PE		400V	29495
C22	.01µF	CE(1)		500V	24902
C23	.1µF	PE		400V	29495
C24	0.1µF	CE(1)		500V	24902
C25	8.2pF	CE(2)	1pF	500V	22363

Ref	Value	Description	Tol %±		Part No.
C26	470pF	PS	10	125V	11492
C27	8.2pF	CE(2)	1pF	500V	22363
C28	470pF	PS	10	125V	11492
C31	100µF	E		275V	32906
C33	1000µF	E		40V	32907
C34	1000µF	E		40V	32907
C35	1000pF	CE(2)			22387
C40	5.6kpF	CE(2)			22394
C41	5.6kpF	CE(2)			22394
TRANSISTORS					
TR31		BD166			32901
TR32		BD165			32900
MR31		WO4			29367
MR32		WO4			29367
SOCKETS					
SKA		50ΩBNC			1222
SKB		50ΩBNC			1222
SKD		4mm Black			30097
SKE		4mm Black			30097
SKF		4mm Black			29492
SKG		4mm Black			29492
SKH		4mm Black			29492
SWITCHES					
S10		Part of R10			
S11		Part of R11			
S12					25869
S13					32636
S14					32634
S20					25869
S21					32635
S24					
S25					25869
S26					32635
S27		Part of R52			
S28		Part of R53			
S30		Part of R33			
S31					25869
MISCELLANEOUS					
V1		CRT D13-610 GH OR CRT D13-610 GM Long Persistence			32904 32905
FS30		FUSE 220V Supply 250mA OR FUSE 110V Supply 500mA			33684 33685
T31		Transformer			A1/32637
N31		Indicator Neon Type Q			26586
L10		Ferrite Bead FX1242			26986
L11		Ferrite Bead FX1242			26986

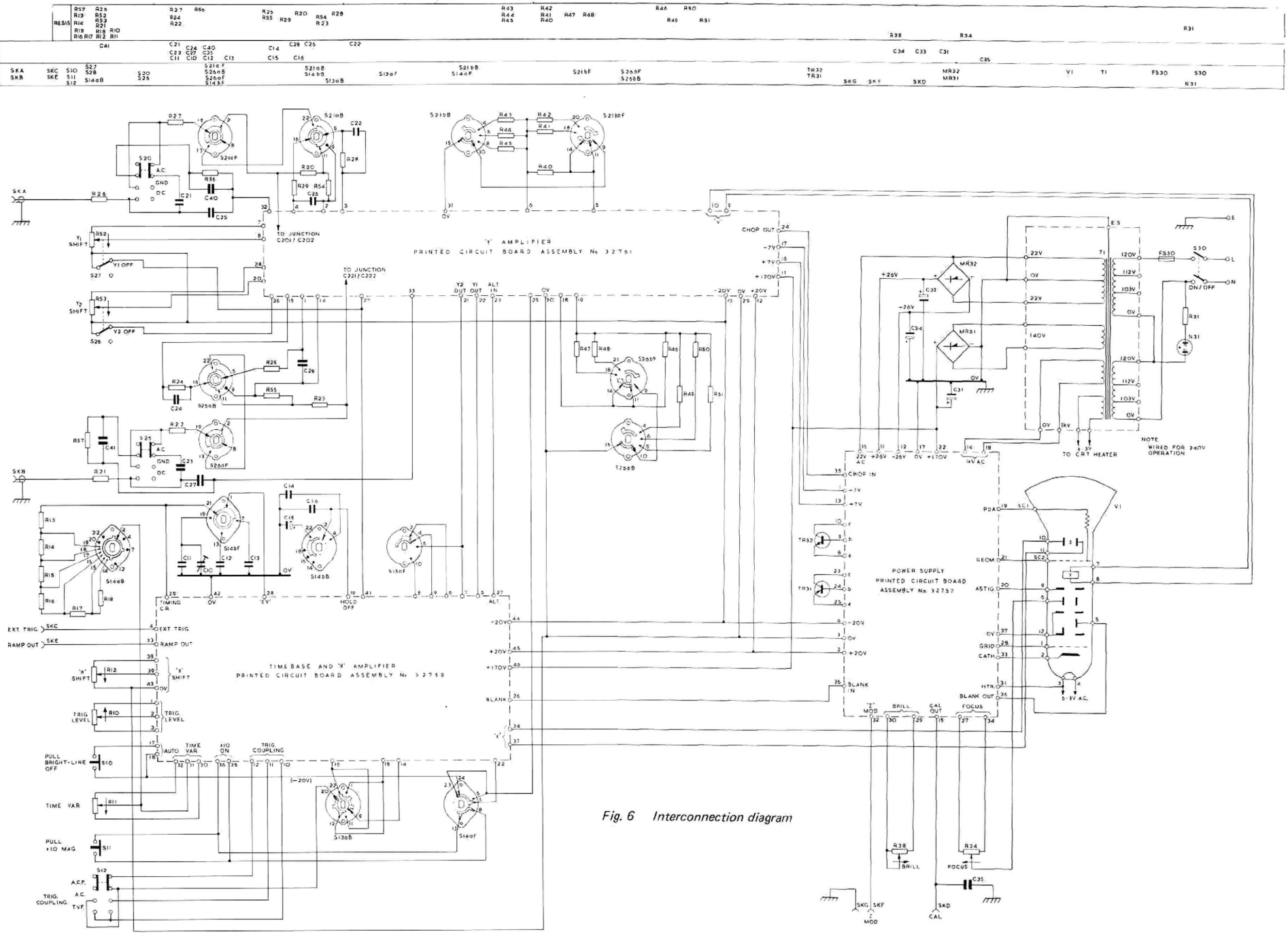

Fig. 6 Interconnection diagram

NOTE

R424	1k	CF	OS250 TV only	21799
R425	56k	CF	OS250 TV only	28729
S13			OS250 TV only	33995

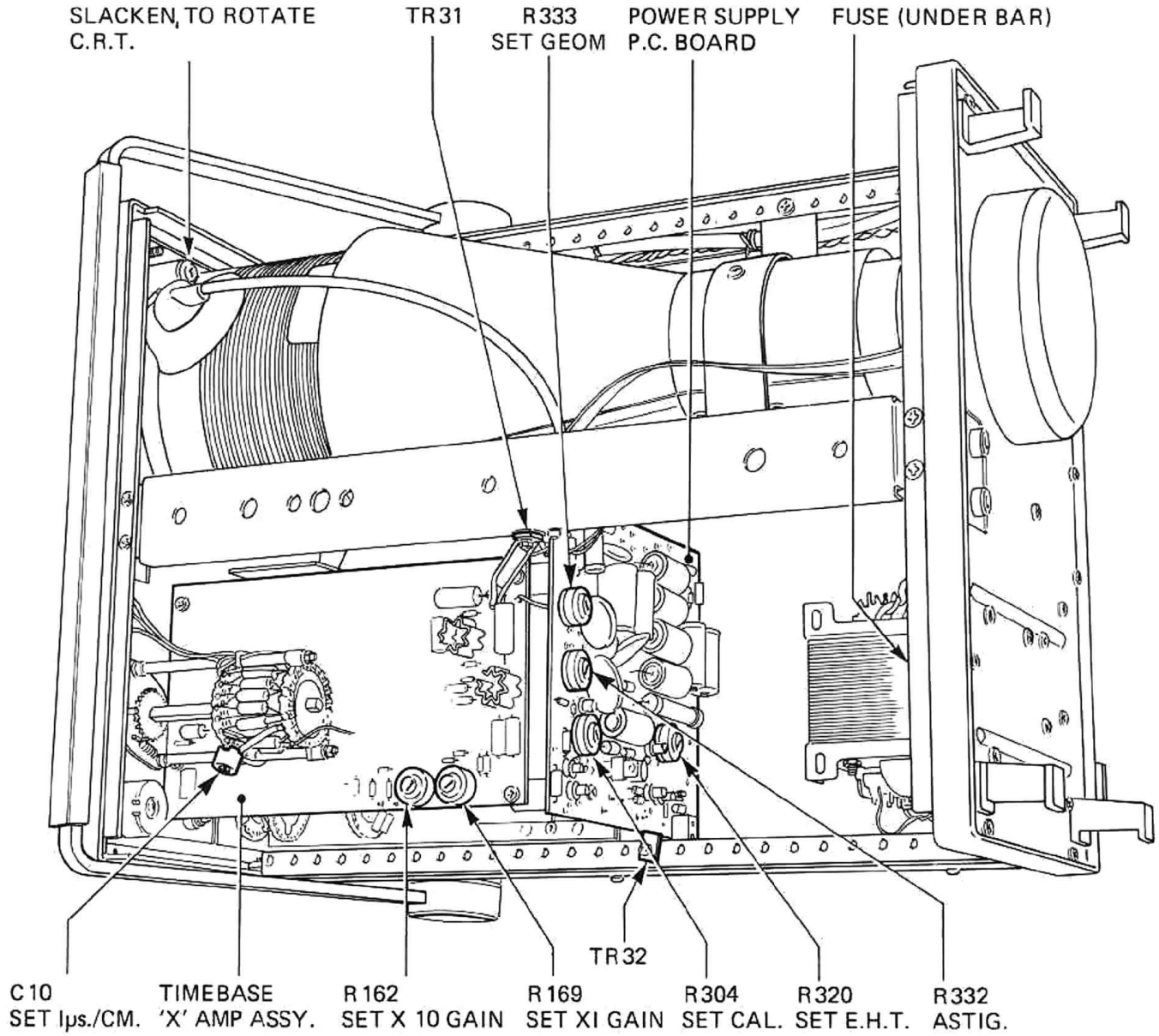

Fig. 7 Top view

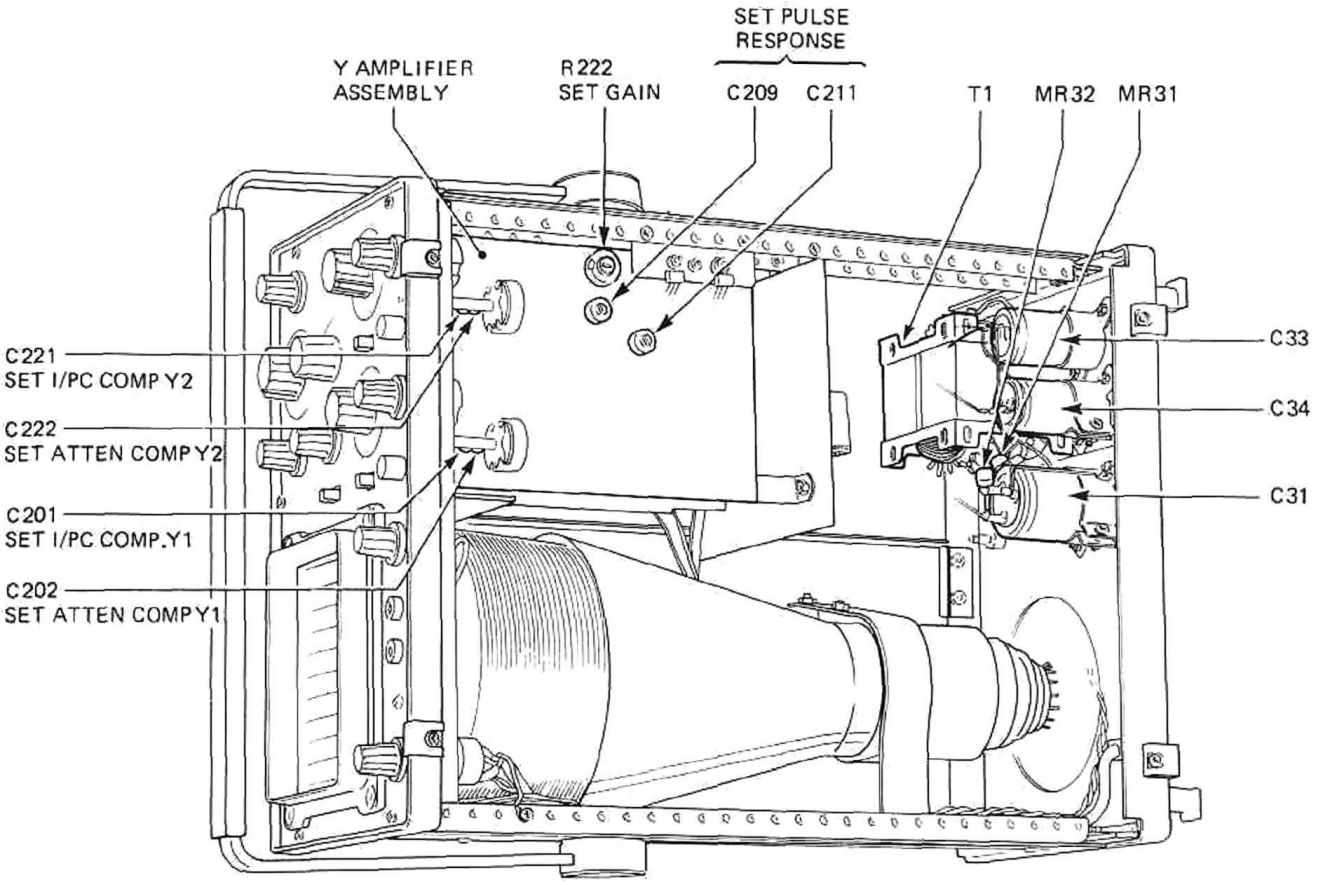

Fig. 8 Bottom view