"TRADER" SERVICE SHEET

RASED on the Ace U51 A.C./D.C. table receiver, with which is associated the 535 range of A.C./D.C. autoradiograms, this service Sheet also covers a number of other models. The model numbers of the receivers and radiograms covered are listed below, and in this list are included all A.C./D.C. models styled "Minigram" and "Mayfair," which differ only in cabinet style. No attempt is made to link a particular arrangement with each model number, but the five different arrangements are explained under "Modifications" overleaf. The basic table receiver is a 4-valve (plus rectifier) 3-band superhet designed to operate from A.C. or D.C. mains of 200-250 V. The mains frequency range (in radiograms) would be limited by the kind of motor employed. Where a radiogram is fitted with an A.C. motor, an electronic convertor unit supplies the motor with A.C. power. Waveband ranges are 16.5-50 m, 190-550 m and 800-2.100 m. The models covered in this service Sheet are, in the models covered in this service Sheet are, in the models are in the service of the ser

50 m, 190-550 m and 800-2,100 m.

The models covered in this service Sheet are, in numerical order:—
33U (table), 33UR, 33RG/DC, U51, MGU535, MGU535/C, MGUS535, MGUS535/C, RGU535, RGUS535/C, RGU535, RGUS535 and MRGU8635 are covered except for the omission of their C.R. tuning indicator. Export versions of all models are covered except for their waveband ranges.

Belease dates and original prices: 33U (table)

Release dates and original prices: 33U (table), November 1950, £15 15s; 33UR, November 1950, £41 18s 6d; 33RG/DC, November 1950, £43 7s 10d; U51, March 1951, £19 0s 6d, increased later to £19 2s 6d; MGU535 or MGU535/C, November

ACE A.C./D.C. RECEIVERS

Covering Model U51 and Ace A.C./D.C. "Minigram" and "Mayfair" Autoradiograms

1951, £60 6s 1d; MGUS535 or MGUS535/C, November 1951, £63 19s 7d; RGU535 or RGU535/C, November 1951, £47 16s 1d; RGUS535 or RGUS535/C, December 1951, £51 9s 7d; MRGU635, November 1951, £60 6s 1d; MRGUS635, November 1951, £63 19s 7d.

CIRCUIT DESCRIPTION

Aerial input is inductively coupled on S.W. by L2 and capacitatively "bottom" coupled on M.W. and L.W. by C5 to single tuned circuits L3, C40 (S.W.), L4, C40 (M.W.) and L5, C40 (L.W.) which precede triode-hexode valve (V1, Brimar 6K8GT) operating as frequency changer with internal coupling. C1 and C4 isolate the aerial and earth sockets from the chassis while R1 provides a D.C. path between the sockets to prevent the build up of static charges on the aerial. R2 prevents modulation hum.

Oscillator anode coils L8 (S.W.), L9 (M.W.) and L10 (L.W.) are tuned by C44. Parallel trimming by C41 (S.W.), C42 (M.W.) and C11, C43 (L.W.); series tracking by C8 (S.W.), C9 (M.W.) and C10 (L.W.). Reaction coupling from grid circuit across the common impedance of the trackers with additional inductive coupling via L6 (S.W.) and L7 (M.W.). Stabilization by R5, R6 and R7.

Second valve (V2, Brimar SK7GT) is a variable-mu R.F. pentode operating as intermediate frequency amplifier with tuned transformer couplings C6, L11, L12, C7 and C16, L13, L14, C17.

Intermediate frequency 472 kc/s.

Diode signal detector is part of double diode riode valve (V3, Brimar 6Q7GT). Audio fre-

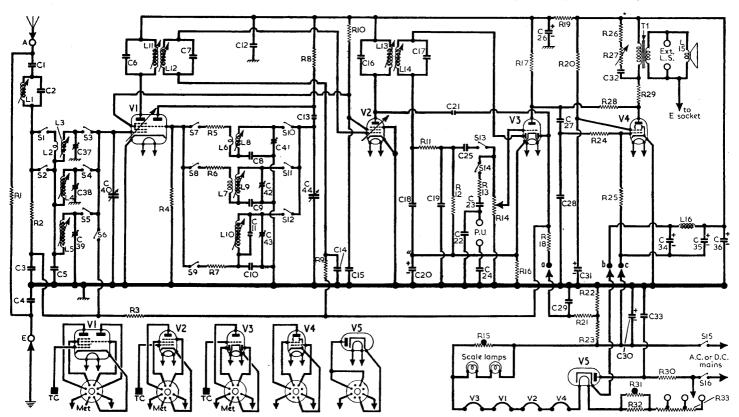
quency component in rectified output is developed across R12 and passed via C25 and volume control R14 to control grid of triode section, which operates as A.F. amplifier. I.F. filtering by C18, R11 and C19.

Second diode of V3 is fed from V2 anode via C21, and the resulting D.C. potential developed across its load resistor R18 is fed back as bias to V1 and V2 giving automatic gain control. Provision is made for the connection of a gramophone pick-up across R14 via S14 which closes in the gram position of the waveband switch. S6 closes and S13 opens on Gram to prevent radio break-through.

On the table model the P.U. sockets are isolated from chassis by C23 and C24, and shunted by C22. On the radiogram model a transformer isolates the P.U. sockets, one side of its primary being connected to the earth socket, and one side of its secondary to chassis.

Resistance-capacitance coupling via R17, C27 and R25 between V3 triode and beam tetrode output valve (V4, Brimar 25L6CT). Variable tone control by R26, R27 and G32 in V4 anode circuit. Fixed tone correction by negative feedback between the anodes of V4 and V3 via R28. Blas for V4 is obtained from the voltage drop across R22 and R23 in the H.T. negative lead to chassis. A proportion of this voltage, that dropped across R22, is fed via decoupling circuit R21, C29 to the A.G.C. diode and to provide bias for V1 and V2. Provision is made for the connection of a low impedance external speaker across T1 secondary.

H.T. current is supplied by I.H.C. half-wave rectifying valve (V5, Brimar 25Z4GT). Smooth-



Circuit diagram of the Ace U51 A.C./D.C. superhet, which is the same as that in all A.C./D.C. "Minigram" and "Mayfair" autoradiograms motors, an electronic convertor unit, whose diagram is shown on the right of the receiver diagram, is used to drive the motor with A.C. power from

ing by R19, choke L16 and electrolytic capacitors C26, C34, C35 and C36.

Valve heaters together with scale lamps, ballast and voltage adjustment resistors R32, R33 and thermistors R15, R31 are connected in series across the mains input. R15 shunts the scale lamps, and R31 protects the valve heaters from current surges.

In the radiogram models a D.C. to A.C. electronic convertor is fitted to supply the gram motor with A.C. from D.C. mains. When the receiver is operated from A.C. mains the convertor switch is set to A.C., opening S17, S18 and closing S19 which connects one side of the motor to the convertor chassis. Starting the motor by closing motor switch S20 connects the mains input across the motor coils via ballast resistor R46.

When the receiver is operated from D.C. mains, the convertor switch is set to D.C., opening S19 and closing S17, S18 which connect the motor coils directly across the output winding of T2. When the motor switch is now closed, the electronic convertor is switched on by having its H.T. line connected via S17, motor switch S20 and ballast resistor R46 to the D.C. mains input.

The convertor consists of a two valve 50 c/s

having its H.T. line connected via \$17, motor switch \$20 and ballast resistor R46 to the D.C. mains input.

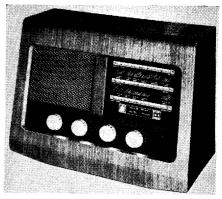
The convertor consists of a two valve 50 c/s multivibrator (V6a, V6b, Brimar 12AU7) whose frequency is governed by the time-constant of C46, R35 and C47, R34. The output from V6a and b is developed across anode load circuit L17, C48, which is tuned to 50 c/s, and passed via C49 and C50 to the control grids of the pushpull connected beam pentode output valves (V7, V8, Emitron or Cossor 185BT's). Output from V7, V8 is coupled via push-pull output transformer T2 and a four-way plug and socket 5, 6, 7, 8 to the gram motor (pin 7 is blank).

The heater ballast resistor R52 and associated components R50, R51, R53 are mounted on the convertor chassis in the radiogram models, and are connected by a four-way plug and socket 1, 2, 3, 4. The heaters of V6 are connected in parallel for 0.3 amp operation and together with the heaters in the radio chassis. Extra current is passed through V7, V8 heaters by ballast and voltage adjustment resistors R47, R48 and R49 to bring their total current, including the H.T. current from the receiver, up to 0.45 amp.

COMPONENTS AND VALUES

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		(1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		RESISTORS	Values	Loca- tions
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R1) Assistation (2·2kΩ	G4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R2	Aeriai snunts {	$10k\Omega$	F4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R3	A.G.C. decoupling	$1M\Omega$	F4
$ \begin{array}{c} R5 \\ R6 \\ R7 \\ R8 \\ R8 \\ Osc. anode load \\ R9 \\ A.G.C. \ decoupling \\ R10 \\ S.G. \ feed \\ R10 \\ R11 \\ I.F. \ stopper \\ R12 \\ Diode \ load \\ R13 \\ R14 \\ Volume \ control \\ R15 \\ R15 \\ R16 \\ R17 \\ V3 \ anode \ load \\ R17 \\ V3 \ anode \ load \\ R18 \\ R19 \\ R19 \\ R10 \\ R10 \\ R10 \\ R10 \\ R10 \\ R10 \\ R11 \\ R11 \\ R12 \\ R12 \\ R12 \\ R13 \\ R13 \\ R14 \\ R14 \\ Volume \ control \\ R15 \\ R15 \\ R16 \\ R17 \\ R18 \\ R20 \\ R17 \\ R20 \\ R21 \\ R21 \\ R21 \\ R21 \\ R22 \\ R22 \\ R23 \\ R22 \\ R23 \\ R24 \\ R24 \\ R25 \\ R25 \\ R26 \\ R27 \\ R27 \\ R27 \\ R28 \\ R29 \\ R29 \\ R29 \\ R20 \\ R20 \\ R21 \\ R21 \\ R21 \\ R22 \\ R23 \\ R22 \\ R23 \\ R23 \\ R24 \\ R24 \\ R25 \\ R26 \\ R27 \\ R27 \\ R27 \\ R28 \\ R29 \\ R29 \\ R29 \\ R29 \\ R30 \\ R29 \\ R31 \\ R40 \\ R4$	R4			G4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R5			F3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R6			
R8	R7	ers		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R8	Osc. anode load		G4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R9			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R10			F4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R11	I.F. stopper		F4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R12			F4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R13			F4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R14		$1M\Omega$	E3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R15			D3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R16		2.2kΩ	F4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R17			F4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R18		$1M\Omega$	F4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R19		1kΩ	D3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R20		$15k\Omega$	E4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R21		$1M\Omega$	D3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R22		68Ω	D3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R23	\ G.B. resistors \	22Ω	D3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R24	V4 grid stopper		E4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R25		$470 \mathrm{k}\Omega$	E4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R26	Part tone control	680Ω	D3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R27	Tone control	$50 \mathrm{k}\Omega$	D3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R28	Neg. feed-back	$1M\Omega$	F4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R29		47Ω	E4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R30	Surge limiter	68Ω	
	R31	Thermistor CZ2		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R32	Tractor ballant	140Ω	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R33	Heater banast	*530Ω	C2
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R34	Ves veh aa	$47 \mathrm{k}\Omega$	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R35	1) ' '	$47 \mathrm{k}\Omega$	
$ \left[\begin{array}{c} R37 \\ R38 \\ R39 \\ R39 \\ R40 \\ \end{array} \right] \begin{array}{c} \text{V7, V8 C.G.} & \dots \\ \left[\begin{array}{c} 100 \text{k}\Omega \\ 100 \text{k}\Omega \\ \text{L7} \\ \text{L8}\Omega \\ \end{array} \right] \begin{array}{c} \text{L6} \\ \text{L7} \\ \text{L8}\Omega \\ \text{L7} \\ \text{L8}\Omega \\ \end{array} $		H.T. smoothing	$\dagger 20 \mathrm{k}\Omega$	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	R37	Dyg ve aa		
R40 pers $R40$		1) '	$100 \mathrm{k}\Omega$	
R40 pers $R40$		7 V7, V8 C.G. stop- 3		
	R40		$1 \mathrm{k} \Omega$	L7
Continued next column		Continued next column		1

* Tapped at $410\Omega+60\Omega+60\Omega$ from R32. † Two $10k\Omega$ resistors in series.

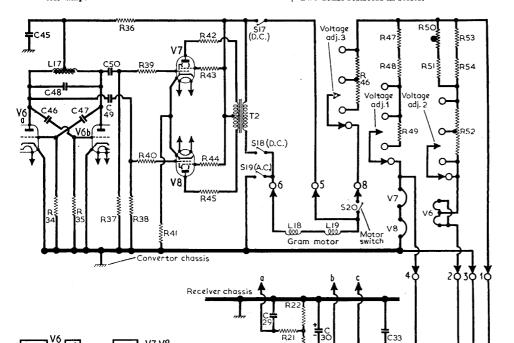


The appearance of the Ace U51 table receiver.

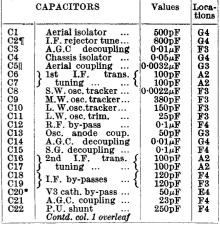
RESISTORS (continued)	Values	Loca- tions
R41	\$34Ω 68Ω 1·1kΩ 1·1kΩ 68Ω \$120Ω 1·49kΩ 500Ω 	M6 H5 L6 L7 H5 J5 J5 J7 L7 J5 J5 J5 J5

‡ Two 68Ω resistors in parallel. § Tapped at $60\Omega + 60\Omega$.

CAPACITORS



R15



 $\P Two$ capacitors, 300 pF+500 pF, in parallel. $\| Two$ capacitors, $0\cdot 0014 \mu F+0\cdot 0018 \mu F$ in parallel. *Electrolytic.

If the component numbers given in the accompanying tables are used when ordering replacement parts, dealers are advised

A.C. or D.C

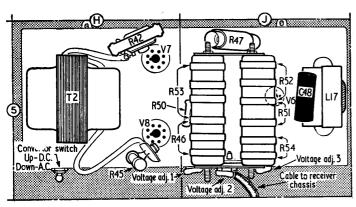
mains

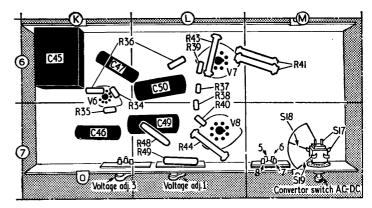
to mention the fact on the order as these numbers may differ from those used in the manufactu r e r s' diagram.

Values

which are fitted with A.C./D.C. gramophone motors. When the A.C./D.C. autoradiograms are fitted with A.C. D.C. mains. Switching arranges matters so that on A.C. mains the motor is connected directly across the mains. When the A.C./D.C. autoradiograms are fitted with A.C.

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Plan view (left) and underside (right) illustrations of the electronic convertor unit. The three voltage adjustment panels are grouped in a triangle at the rear. The A.C./D.C. change-over switch unit \$17-\$19 is replaced by a plug-and-socket device in later models. The 4-pin socket numbered 5, 6, 7, 8 accepts the motor plug.

CAPACIT (Continu		Values	Loca- tions
C23 } P.U. iso	lators {	$\begin{array}{c} 0.1 \mu \mathrm{F} \\ 0.1 \mu \mathrm{F} \end{array}$	F4 F4
$\begin{array}{c c} C24 \\ C25 \end{array}$ $A.F.$ cor	<u> </u>	$0.1 \mu F$	F3
	oothing	$8\mu F$	E3
C26* H.T. sm C27 A.F. co		$0.01 \mu F$	F4
		250pF	E4
C28 I.F. by- C29 A.G.C.	Lecoupling	$0.01 \mu F$	F4
C30* G.B. by		$50\mu F$	E3
	decoup.	8µF	E3
	e control	$0.05 \mu \mathrm{F}$	D3
C32 Mains R	.F. filter	$0.05 \mu F$	E4
C34*	($16\mu F$	$\overline{\text{C1}}$
$C35*$ \rightarrow H.T. sn	noothing	$16\mu F$	l či
C36* 11.1. sn	100 cmmg	$12 \mu F$	$\tilde{D3}$
C371 S.W. aet	rial trim		G3
	rial trim		G3
	rial trim		G3
C40† Aerial t			Al
C411 S.W. osc			F3
C421 M.W. os		_	F3
C43† L.W. os		. —	F3
	or tuning		A1
		$4\mu F$	K6
C46) Multi-vi	brator re-	$0.1 \mu F$	K7
C46 Multi-vi	coupling brator re- {	$0.1 \mu F$	K6
	de tune	$0.2 \mu F$	J5
C40)	($0.5 \mu F$	L7
C50 Sec. con	upnng {	$0.5 \mu F$	L6

*Electrolytic. †Variable. ‡Pre-set. §Paper type, not electrolytic.

отні	ER COMPONENTS	Approx. Values (ohms)	
$_{ m L2}^{ m L1}$	I.F. filter S.W. aerial coup.	1.8	G4 G3
L3 L4 L5	$ brace$ Aerial tuning ${ m coils}$	1·7 40·0	G3 G3 G3
L6 L7	Reaction coupling	$0.4 \\ 1.0$	F3 F3
L8 L9 L10	$\left. \left. \right. \right\}$ Oscillator tuning $\left\{ \left. \right \right. \right\}$	5·5 17·5	F3 F3 F3
L11 L12		9·0 9·0	A2 A2
L13 L14 L15	$\left. egin{array}{l} 2 ext{nd I.F. trans.} \left\{ egin{array}{l} ext{Pri.} \\ ext{Speech coil} \end{array} ight. \end{array} ight.$	$\begin{array}{c} 6.0 \\ 6.0 \\ 2.5 \end{array}$	A2 A2
L16 L17	Smoothing choke Converter osc. coil	$\begin{array}{c} 140.0 \\ 650.0 \end{array}$	C1 J5
L18 L19	Gram. motor coils {	$230.0 \\ 230.0 \\ 500.0$	_
T1 T2	O.P. trans. Sec.	0·5 50·0	E3
S1-S14	O.P. trans \Sec. Waveband switches	65.0	G3
S15, S16 S17-	Mains sw., g'd R14		E3
S19 S20	Converter switches Gram. motor sw	=	M7

VALVE ANALYSIS

Valve voltages and currents given in the table

Valve voltages and currents given in the table below are those measured in our receivers. The figures for V1-V5 were measured in a table model when it was operating from 230 V A.C. mains and tuned to the highest wavelength end of M.W. There was no signal input. The figures for V6-V8 were measured in the convertor unit of a radiogram model when it was switched to D.C., and operating from 230 V D.C. mains with the gram motor running.

Voltage readings were measured with an Avo Electronic TestMeter, and as this instrument draws no appreciable current, allowance must be made for the current drawn by other types of meter. The A.C. voltage measured across the gram motor input with the converter operating from 230 V D.C. mains was 230 V. The receiver chassis was the negative connection for voltage readings from V1-V5 and the converter chassis for readings from V6-V8.

Valve	Anode		Screen		Cath.
vaive	V	mA	v	mA	v
V1 6K8GT	192 Osci	$\left\{\begin{array}{c} 2.6 \\ \text{llator} \\ 4.0 \end{array}\right\}$	110	5.4	
V2 6K7GT	195	4.7	110	2.4	
V3 6Q7GT V4 25L6GT	$\begin{array}{c} 95 \\ 175 \end{array}$	0·4 66·0	135	4.5	1.2
V5 25Z4GT V6 fa	220†	3.0		_	230.0
12AU7 (b	68	3.0	105		-
V7 185BT V8 185BT	175 175	$115.0 \\ 115.0$	$\frac{165}{165}$	16·0 16·0	9.5

† A.C. reading.

DISMANTLING

Removing Chassis.—Remove control knobs (pull-

off) and felt washers; unsolder leads from speech coil tags on speaker; remove four 2BA bolts with washers securing chassis to cabinet and withdraw chassis.

The foregoing applies to the table models only; the fixing is different in the radiograms.

GENERAL NOTES

Switches.—S1-S12 are the waveband switches, and S13, S14 are the radio-gram change-over switches, ganged in a single rotary unit beneath the chassis. The unit is indicated in our underchassis illustration and shown in detail in the diagram in col. 4, where it is drawn as seen from the rear of an inverted chassis.

The table below it gives the switch positions for the four control settings, starting from the fully anti-clockwise position of the control knob. A dash indicates open, and C, closed.

S15, S16 are the Q.M.B. mains switches, in a double-pole unit ganged with the volume control R14.

Scale Lamps.—These are two M.E.S. lamps, with small clear spherical bulbs rated at 6.5 V, 0.3 A. They are shunted by a Brimistor CZ2, R15.

External Speaker.—Two sockets are provided at the rear of the chassis for the connection of a low impedance (about 3-4 \Omega) speaker.

Drive Cord Replacement.—About 50 inches of high-grade flax fishing line is required for a new drive cord, which should be run as shown in the sketch in col. 6 where it is drawn as seen from the rear of the chassis, neglecting obstructions, when the gang is at maximum capacitance. capacitance.

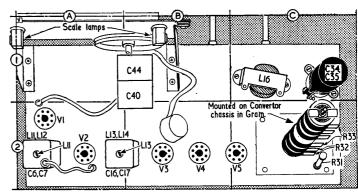
capacitance. Capacitor C4.—This is a $4\mu F$ paper type capacitor decoupling the H.T. feed to the convertor oscillator. An electrolytic should not be used as a replacement because if the mains plug is inserted with reversed polarity, this will be applied to the capacitor as soon as the motor is switched on. The motor, of course, will not run under these conditions as the H.T. supply to the anodes of the convertor is reversed.

Resistors R30, R42, R45.—These are $68\,\Omega$ resistors in the anode circuits of heavy-duty valves, and they are rated at 2 W dissipation.

MODIFICATIONS

Export models.—There are two versions of the U51 A.C./D.C. receiver for export, one with S.M.L. wavebands, as in the home version, and one with S.S.M. wavebands. The differences between the circuit of the home model and that of the export versions are that the latter are equipped with a cathode ray tuning indicator (Brimar 6U5G) and that the aerial circuit switching indicators in the content of the content o ing is omitted

Plan view of the receiver chassis as it is in the normal models. In those radiograms which use a convertor, the heater ballast resistor R32, R33 is the convertor unit.



Where we show \$1 in the home model, there is a short-circuit, and \$2 is omitted, as are \$6 and \$13 also. The switch unit is a simple rotary type with twelve contacts, the tags of two being nipped off, and it has four settings.

Autoradiograms.—There are several series of A.C./D.C. radiograms, with varying type numbers which need not be detailed here, but they divide up electrically into four kinds: (i) uses an unmodified U51 chassis with a single-speed A.C./D.C. record changer; (ii) is like (i) but has a 3-speed A.C./D.C. record changer; (iii) uses a modified U51 chassis with a single-speed A.C. record changer whose motor is run on D.C. mains from an electronic D.C. to A.C. convertor; (iv) is like (iii) but has a 3-speed A.C. record changer whose motor is run from an electronic D.C. to A.C. convertor. The model numbers covered are explained in the introduction and the title of this Service Sheet. Models designed for A.C. mains only are not covered at all.

Universal Motors.—Where the radiogram is fitted with an A.C./D.C. record-changer and the electronic convertor is not needed, a standard U51 chassis is employed, as used in the table receiver, but in some models R13, C22, C23 and C24 are omitted and the pick-up is fed in via a matching transformer. One end of the primary goes to the E socket, and one end of the secondary goes to chassis.

A.C. Motors.—Where the radiogram is fitted with an A.C. record changer, an electronic convertor is used on D.C. mains to supply A.C. to the motor, and the use of this involves physical changes in the chassis as compared with that in the U51 table model, although the circuit is not very different electrically. The same modification with regard to the pick-up input obtains as was described for universal motors.

Convertor Models.—The physical differences involved in the models using the convertor are associated with the power supply components, of which the heater ballast resistor is removed from the radio chassis and is included in the convertor.

In order to make this quite c

In order to make this quite clear, the affected part of the receiver circuit is redrawn, in our main diagram overleaf, beneath the convertor circuit as it is in the convertor models, although all the circuit shown below the chassis line of

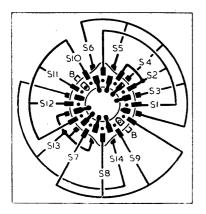


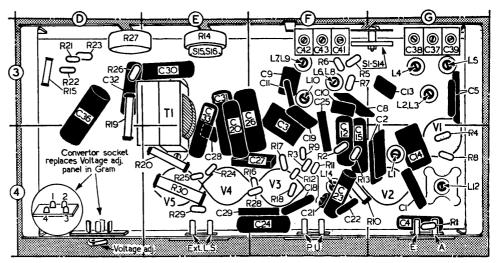
Diagram of the waveband switch unit, drawn as seen from the rear of an inverted chassis. Below is the associated switch table.

Swithces	S.W.	M.W.	L.W.	Gram.
S1 S2	С	_		
S2		С	C	
S3 S4 S5	C	_	_	_
S4		c		
S5		_	C	
S6		l —		C
S7	C			:
S8		С		
S9			C	_
S10	C	_		
S11	-	С		
S12	_		С	
S13	С	C	С	
S14		1 —		С

the convertor unit is actually in the receiver chassis. Points a, b and c show where the affected part of the circuit joins the rest of the

receiver.

It will be seen that the ballast circuit is a little different from that in the U51, and that



Underside drawing of the radio receiver chassis, with inset at the lower left-hand corner a diagram of the convertor socket which takes the place of the voltage adjustment panel in the convertor-type radiograms.

the heaters of the convertor valves are included in the series heater chain. The two halves of the V6 heater are connected in parallel to match the 0.3 A heater circuit, but the heaters of V7 and V8, which are rated at 0.45 A, are at the "earthy" end of the chain and have a separate ballast resistor R47, R48, R49 which passes 0.15 A, shunting the original heater circuit and bringing the total current for V7, V8 up to the rated value.

catory can of one chain and have a separate ballast resistor R47, R48, R49 which passes 0.15 A. shunting the original heater circuit and bringing the total current for V7, V8 up to the rated value.

Convertor Unit.—The convertor consists of a multi-vibrator type of 50 c/s oscillator driving a push-pull output stage of large-output valves whose output is transformer coupled to the A.C. motor of the gramophone, and it is required, of course, only when the A.C./D.C. receiver is operating from D.C. mains.

Change-over from A.C. to D.C. and vice versa is effected either by a double-pole 2-way switch or a plug-and-socket device. In either case the change-over is represented by switches \$17, \$18, \$19, as explained in "Circuit Description." When a switch is used, its toggle is up for D.C., and down for A.C.; when a plug-and-socket arrangement is used, the plug goes to the upper sockets for D.C.. and to the lower ones for A.C.

The gramophone motor is connected to the convertor unit by means of plug and socket 5, 6, 7, 8, the socket being mounted on the rear member of the convertor, and pin 7 being unused. The convertor is connected to the receiver by a similar plug, whose socket is mounted on the rear member of the receiver chassis (it takes the place occupied in normal U51 receivers by the voltage adjustment panel). The mains input to the convertor is via the receiver and then via pins 1 and 3 of the plug, and the heaters are connected in the series via pins 2 and 4. The chassis of the convertor is at a different potential from that of the receiver.

For D.C. operation the rramophone motor is connected directly across the convertor model is connected to D.C. mains, therefore, while adjusted for A.C. the motor will burn out.

Voltage adjustment in the convertor model is connected to D.C. mains, therefore, while adjusted for A.C. the motor will burn out.

Voltage adjustment in the convertor model is requires attention at three points, all located on the convertor unit. In our diagram they are numbered 1, 2 and 3. Unfort

adjustment No. 2 was mounted at right-angles to the other two.

H.T. current from the radio receiver, besides heater current from the receiver and the additional ballasting current from the voltage adjustment No. 1 ballast circuit, flows through the convertor output valve heaters V7 and V8, and the total current through them should be 0.45 A. The current through the oscillator valve heater V6 is 0.3 A through the two halves connected in parallel. The rated current for each half is 0.15 A.

CIRCUIT ALIGNMENT

CIRCUIT ALIGNMENT

It is necessary before carrying out the following alignment procedure to remove the chassis from its cabinet in order to make all the core and trimmer adjustments accessible.

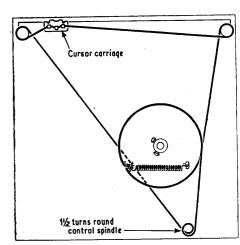
I.F. Stages.—Switch receiver to M.W. and turn gang to maximum capacitance. Connect output of signal generator, via 0.1 µF capacitor in each lead, to control grid (top cap) of V1 and chassis. Feed in a 472 kc/s (635.6 m) signal and adjust the cores of L14 (location reference F4), L13 (A2), L12 (G4) and L11 (A2) for maximum output. Repeat those adjustments.

R.F. and Oscillator Stages.—Transfer signal generator leads, via a suitable dummy aerial, to A and E sockets.

L.W.—Switch receiver to L.W., tune to 2,000 m, feed in a 2,000 m (150 kc/s) signal and adjust the cores of L10 (F3) and L5 (G3) for maximum output. Tune receiver to 1,000 m, feed in a 1,000 m (300 kc/s) signal and adjust C43 (F3) and C39 (G3) for maximum output.

M.W.—Switch receiver to M.W., tune to 500 m, feed in a 500 m (600 kc/s) signal and adjust the cores of L9 (F3) and L4 (G3) for maximum output. Tune receiver to 200 m, feed in a 200 m (1,500 kc/s) signal and adjust the cores of L9 (F3) and L4 (G3) for maximum output. Repeat these adjustments.

S.W.—Switch receiver to S.W., tune to 50 m, feed in a 50 m (6 Mc/s) signal and adjust the cores of L8 (F3) and L3 (G3) for maximum output. Tune receiver to 20 m, feed in a 20 m (15 Mc/s) signal and adjust C41 (F3) and C37 (G3) for, maximum output. Repeat these adjustments.



Sketch of the drive cord system, drawn as seen from the rear of the chassis, neglecting obstructions.