# "TRADER" SERVICE SHEET

ITTED with a ferrite rod A.M. aerial, which is rotatable by means of a control knob on the front of the receiver, the Philips 543A is a 6-valve (plus rectifier) A.M./F.M. table receiver. It is housed in a plastics cabinet, and is designed to operate from A.C. mains of 200-250V, 50-100 c/s. The waveband ranges are: F.M., 87.5-100 Mc/s; A.M., 25-51m, 187-580m, and 1,150-2,000m.

Model 643A employs the same basic chassis as the 543A, but it is housed in a wooden cabinet and has a tuning indicator. Other small differences between the

two receivers are indicated in the component tables.

Release date, both models, November, 1954. Original prices: 543A, £23 1s; 643A, £33 7s 9d. Purchase Tax extra.

#### CIRCUIT DESCRIPTION

A.M. aerial input via L8 (S.W.) and the common impedance of C15, R8 (M.W. and L.W.) to single tuned circuits L9, C74 (S.W.), L10, C74 (M.W.) and L11, C74 (L.W.). The M.W. and L.W. tuning coils L10, L11 are mounted at opposite ends of a length of ferrite rod to form the M.W. and L.W. internal aerial. C16, L12, C72 form a L.W. image filter and L13, C18, C19, L14 form an I.F. filter. Section b of V2 (Mullard ECH81)

operates as mixer, and section a as oscillator. Oscillator anode coils L17 (S.W.) and L18 (M.W. and L.W.) are tuned by C77. Parallel trimming by C25 (S.W.), C75 (M.W.) and C75, C23, C76 (L.W.); tracking by means of shaped vanes of oscillator section of the gang. Oscilla-

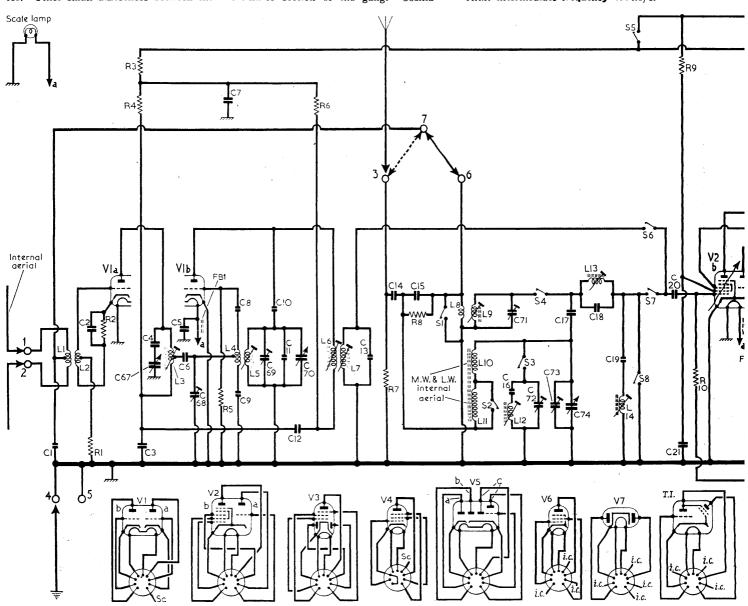


Appearance of the Philips 543A.

tor reaction coupling from grid circuit by L15 (S.W.), L16 (M.W. and L.W.).

Pentode section of diode pentode valve (V3, Mullard EBF80) operates as single-valve A.M. intermediate frequency amplifier with tuned transformer couplings C30, L21, L22, C31 and C36, L25, L26, C37.

A.M. intermediate frequency 470 kc/s.



# PHILIPS 543A 643A

Press-button A.M./F.M. Table Superhets for A.C. Mains

Diode section of V3 functions as A.M. plode section of V3 functions as A.M. signal detector, and the A.F. component in its rectified output is developed across load resistor R19 and passed via C48, volume control R26 and C52 to grid of V5c (triode section of V5, Mullard EABC80). I.F. filtering by C38, R16, C39.

D.C. potential developed across R19 is fed back as bias to V2b and V3 giving automatic gain control on the A.M. bands.

Resistance-capacitance coupling by R30, R31, R34, C54 and R38 between V5c ray, H31, H34, C34 and H38 between V5c and pentode output valve (V6, Mullard EL84). Tone correction by R28, C51 and R44, C65. Tone control by R37 in the negative feed-back network R39, R36, C58, R38, C59, R37, C57, R33, C55, R34, C56, R35 between windings e, d on output transformer T1, V6 cathode and control grid circuits, and V5c anode circuit. Switches S23, S26 are ganged with the tone control R37 and give bass-boost.

The tone control is connected to give top-cut when rotated in either direction from its mid-position setting, and switches \$23, \$25 open to give bass boost in the anti-clockwise direction only.

Provision is made for the connection of a gramophone pick-up across R26 via S22 which closes when the Gram key is depressed. S20 also closes and S21 opens to prevent radio break-through.

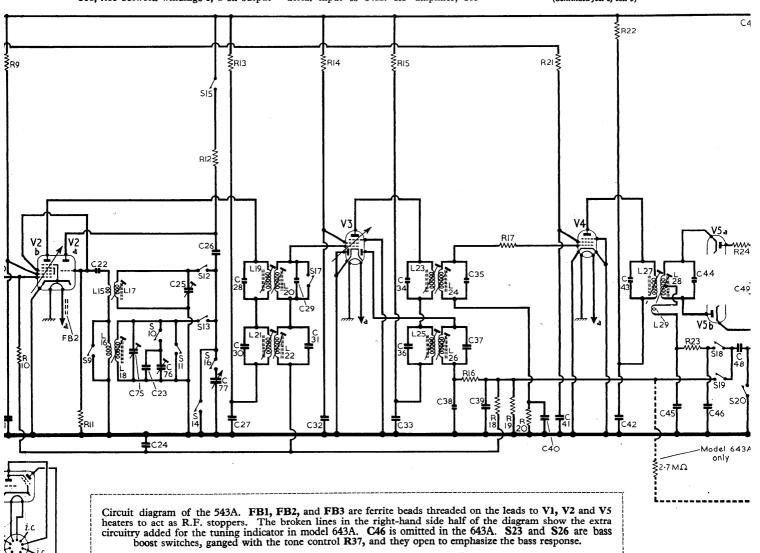
#### Operation on F.M.

Balanced 300 $\Omega$  or co-axial 75 $\Omega$  F.M. aerial input to F.M. RF amplifier, sec-

tion a of V1 (Mullard ECC85). The aerial input transformer L1, L2 is fixed-tuned to the centre of Band II, and the anode circuit is tuned by C67.

Section b of V1 operates as an oscillator/mixer stage with tuned oscillator anode circuit L5, C70. Oscillator temperature. ature drift is compensated for by negative temperature coefficient capacitor C11. The amplified output of V1a is coupled to The amplified output of V1a is coupled to V1b grid circuit by a tapping on the oscillator grid reaction coil L4. The selectivity of the R.F. tuned circuit is improved by a degree of regenerative coupling between the anode circuits of V1a and V1b via C12. F.M. tuning is by means of C67 and C70 which form two sections of the tuning gang.

(Continued foot of col. 9)



#### COMPONENT VALUES AND LOCATIONS

	RESISTORS	Values	Loca- tions
R1	} V1a G.B {	33Ω	H4
R2	γ τια α.υ ξ	$470\Omega$	H4
R3	} H.T. feed {	1kΩ	F3
R4	)	4·7kΩ	H4
R5	F.M. osc. C.G	$220 \mathrm{k}\Omega$	H4
R6	V1b H.T. feed	$10 \mathrm{k}\Omega$	H4
R7*	A.M. aerial shunt	180kΩ	G3
R8	A.M. aerial coup	$33k\Omega$	G3
R9	V2b S.G. feed	$39$ k $\Omega$	G3
R10	V2b C.G	$1.2M\Omega$	G3
R11†	V2a osc, C.G	$47k\Omega$	G4
R12	A.M. osc. H.T. feed	$33k\Omega$	G4
R13	V2b H.T. decoupling	$2.2k\Omega$	G4
R14	V3 S.G. feed	$82k\Omega$	G4
R15	V3 H.T. decoupling	6.8kΩ	F4
R16	A.M. I.F. stopper	180kΩ	G4
R17	V4 C.G. stopper	10Ω	F4
R18	A.G.C. decoupling	1.2MΩ	G4
R19	A.M. diode load	220kΩ	G4
$\tilde{R}20$	V4 C.G	100kΩ	F4
R21	V4 S.G. feed	56kΩ	F4

	RESISTORS (continued)	Values	
R22 R23 R24 R25 R26†† R27 R28‡ R30 R31* R32 R33 R34 R35	V4 H.T. decoupling De-emphasis Stabilizer D.C. load Yolume control Tone correctors V5c anode loads { Tone corrector Neg. feed-back tone correctors	2·2kΩ 180kΩ 150kΩ 2MΩ 2MΩ 82kΩ 68kΩ 10MΩ 100kΩ 47kΩ 2·7kΩ 2·8cΩ 22kΩ	F4 F4 F4 D1 E3 D1 E4 E4 E4 E3 E3
R36 R37 R38 R39 R40¶ R41 R42 R43 R44‡‡	Tone control  Neg. feed-back { V6 C.G  H.T. smoothing { V6 G.B Tone corrector	33kΩ 1MΩ 820kΩ 560Ω 39kΩ 1·8kΩ 18kΩ 180Ω 5·6kΩ	F3 E3 E4 F4 H4 H4 F4 D1

	CAPACITORS	Values	Loca- tions
C1	Aerial shunt	10pF	H4
C2 C3	171 AL L	1.500 pF	H4
C3	F.B. Coupling	200pF	H3
C4 C5	F.B. Coupling F.M. R.F. tun Heater by-pass F.M. R.F. coup. H.T. by-pass	220pF 4,700pF	H4 H4
Č6	F.M. R.F. coup.	100pF	H4
C7	H.T. by-pass	4.700pF	H4
C8 C9	F.M. Osc. coup-	33pF	H4 H4
C10	[ lings ]	12pF	H4
C11##	F.M. Osc. trim	18pF 4·7pF	H4
C12 C13	F.M. Osc. trim F.B. Coupling 1st F.M. I.F. trans.	4,700pr	
C14	tuning	15pF 560pF	A2 G3
C15	( lings )	$0.003 \mu F$	H3
C16 C17	L.W. image filter	47nF	$\mathbf{F}3$
C17	L.W. image filter A.M. aerial coup A.M. I.F. filter tun-	380pF 270pF	G3 G3
C19	ing {	12pF	G3
C20	V2b C.G	TOOTSE.	G4
C21 C22	V2b S.G. decoup	$0.01 \mu F$	G3
C22 C23	I.W. osc. trim	0.01µF 47pF 270pF	G4 F3
C24	y ing 12 y y y y y y y y y y y y y y y y y y	υ υιμε	G4
C25‡	S.W. osc. trim,		
C26 C27	A.M. osc. coupling	470pF 4,700pF	G3 G4
C28	2nd F.M. I.F.	33pF	B2
C29	trans. tuning {	33pF 33pF	B2
C30 C31	1st A.M. I.F.	110nF	B2
C31	trans. tuning \ V3 S.G. decoup.	195pF 4,700pF	B2 G4
C33	H.T. decoupling 3rd F.M. I.F.	0.800001	G4
C34 C35	3rd F.M. I.F. {	33pF 33pF	C2
C35	trans. tuning } 2nd A.M. I.F.	33pF 110pF	C2 C2 C2
C37	trans. tuning	195pF	$\tilde{c}_2$
C388	I.F. by-passes {	47pF	
C39		47pF 100pF	F4
C40 C41	V4 C.G. limiter V4 S.G. decoup.	4 700 nF	1774
C42	H.T. decoupling	6.800pF	F4
C43	V4 S.G. decoupl. H.T. decoupling 4th F.M. I.F. trans. tuning Discriminator load  Campinasio	22pF 47pF	$\frac{\text{C2}}{\text{C2}}$
C44 C45¶	Discriminator load	4700nF	C2 F4
C46§§	Discriminator load   De-emphasis }	4,700pF 0.001μF	F4
C47	H.T. by-pass	6,800pF 0·01μF	F4
C48	H.T. by-pass A.F. coupling D.C. reservoir I.F. by-pass		
C49* C50	I.F. by-pass	4,700pF 8,200pF 0:01μF	F4
C51		8,200pF	$\mathbf{E}_3$
C52	A.F. coupling	0·01μF	F4 F4
C53 C54	Heater by-pass A.F. coupling	$^{4,700}_{0.022\mu F}$	F4
C55	:) (	$0.1 \mu F$	<b>E</b> 3
C56	Neg. feed-back	(3.4) [ (4) [6]	H:X
C57 C58	Neg. feed-back tone correctors	560nF	E4
C59 C60*	.)	0·01μF 560pF 1,500pF 100μF	E3
C60*	V6 cath-by-pass	$100 \mu F$	E4
C61*	H.T. smoothing {	50μF 50μF	Δ2
C62*	Tone corrector	33nF	F4
C64	Mains R.F. by-pass	1,000pF 3,300pF	E4
C65 C66*	Tone corrector	$^{3,300\mathrm{pF}}_{50\mu\mathrm{F}}$	D1
C67+	F.M. R.F. tuning		B1
C68‡	F.M. R.F. trim.	30pF	H4
C69‡	F.M. osc. trim.	30pF	H3 B2
C71+	S.W. aerial trim.	20pF	- H1
Č721	L.W. image filter	58pF 20pF	Ğ4
C67† C681 C691 C70† C711 C721 C731 C74†	M.W. aerial trim.	20 <b>p</b> F	G3
C74†	A.M. aerial tuning	20pF	B1 F3
C751 C761 C77	Tone corrector H.T. reservoir F.M. R.F. tuning F.M. R.F. trim. F.M. osc. trim. F.M. osc. trim. I.W. image filter M.W. aerial trim. A.M. aerial tuning M.W. osc. trim. L.W. osc. trim. A.M. osc. trim. A.M. osc. trim. A.M. osc. tuning	100pF	G3
Č77†	A.M. osc. tuning		B2

\*Electrolytic, †Variable, ‡Pre-set, \$May be 100pF. ¶May be 2,200pF. §\$Omitted in 643A. ††May be 68 pF. ‡‡Neg. temp. coefficient. ||or 3,300pF.

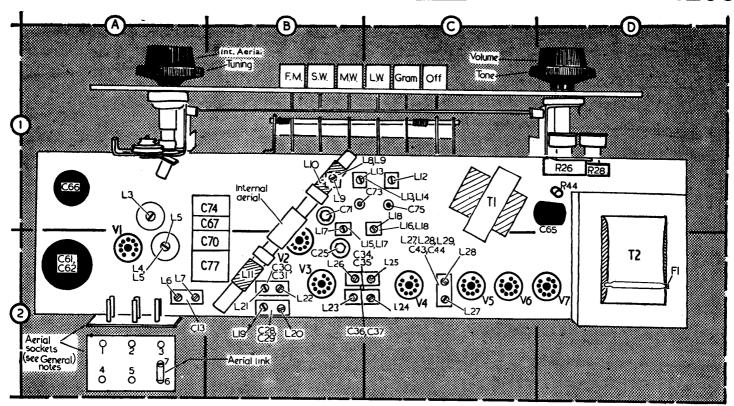
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Circuit Description—continued.

V2b, V3, V4 (Mullard EF85) form a three-valve F.M. intermediate frequency amplifier with tuned transformer couplings L6, L7, C13; C28, L19, L20, C29; C34, L23, L24, C35 and the discriminator transformer C43, L27, L28, C44. R20, C40 provide grid limiting.

F.M. intermediate frequency 10.7 Mc/s. Diode sections a and b of V5 operate in an F.M. ratio detector circuit, whose A.F. output is fed via de-emphasis circuit R23, C46 to R26.

	* May be 100kΩ. † May be 27kΩ.	¶ May be $2 \cdot 7 k\Omega$ .	* May be 100kΩ. ‡ May be 47kΩ.	†† Tapped at $400k\Omega$ from chassis. ‡‡ May be $2\cdot 2\ k\Omega$ .
C47 R24 44 C49 S18 S18 S22 S19 S20 P.U.	C52	R30 \$25 R34 \$26 C54 V5c \$33 C54 V5c \$4 R32 R32 R32 R32	S27 C57 C59 R37	R42 S28  R42  T1  Ext. L.S.  A B C C C C C C C C C C C C C C C C C C
Aodel 643A only	8-2 MΩ	Model 643A only 0·047μF	470 k Ω TI	V7



Plan illustration of the chassis showing the rotatable A.M. internal aerial and the 6-pin aerial connecting panel.

OTHE	R COMPONENTS	Approx. Values (ohms)	Loca- tions
$ \begin{array}{c} L1 \\ L2 \\ L3 \\ L4 \\ L5 \\ L6 \\ L7 \\ L8 \end{array} $	F.M. aerial coupling coils	   1.75 1.75 2.2	H4 H4 A1 A2 A2 A2 A2 B1
$egin{array}{ccc} L9 & \{\\ L10 & \{\\ L11 & \{\\ L12 & \{\\ L13 & \{\\ L14 & \{\\ \\ \end{array}\} \} \end{array}$	S.W. aerial coils { M.W., L.W.internal aerial coils { L.W.image filter I.F. filter coils {	1·0 3·0 8·0 2·75 45·0	B1 B1 B2 C1 B1 B1
$ \begin{array}{c} \text{L15} \\ \text{L16} \\ \text{L17} \\ \text{L18} \\ \text{L19} \\ \text{L20} \end{array} \right\} $	A.M. osc. reaction { coils A.M. osc. tuning { coils 2nd F.M. {Pri. 1.F. trans. { Sec.	3·5 7·0	B1 C1 B1 C1 B2 B2
$egin{array}{ccc}  ext{L21} & \{ \  ext{L22} & \{ \  ext{L23} & \{ \  ext{L24} & \{ \  ext{L25} $	1st A.M. {Pri. I.F. trans. {Sec. 3rd F.M. {Pri. I.F. trans. {Sec. 2nd A.M. {Pri.	8·0 5·0 — 8·0	B2 B2 B2 C2 B2
L26   { L27   } L28   { L29   } L30	I.F. trans. \Sec. \\ 4th F.M. \Sec. \Sec. \Tert. \Speech coil	5·0 1·25 — 3·5	C2 C2 C2 C2
Γ1	O.P. trans. $\begin{cases} \mathbf{a} & \dots \\ \mathbf{b} & \dots \\ \mathbf{c} & \dots \\ \mathbf{d} & \dots \end{cases}$	295·0 — 60·0	C1
Т2	$\begin{array}{c} \text{Mains} \\ \text{trans.} \end{array}  \begin{cases} \begin{array}{c} \mathbf{a} & \dots \\ \mathbf{b} & \dots \\ \mathbf{c} & \dots \\ \mathbf{d}, \text{ total} \end{array} \end{cases}$	100·0 100·0 43·0	D2
	Waveband and tone }		F3
S30, }	Mains switches		F3

#### **GENERAL NOTES**

Switches.—S1-S29 are the A.M./F.M./ Gram and tone switches, ganged (with exception of \$17, \$23, \$24 and \$26) in five rotary units beneath the chassis. These units are press-key operated, and are identified in locations F3, G3 in the underside illustration of the chassis,

where they are numbered 1-5 to correspond with the detailed diagrams of the units at the foot of column 9.

\$17 is a separate switch in location G4, but it is not shown. It is ganged to switch unit 5 by means of a length of nylon braided glass yarn.

\$24 is shown in location F3 and consists of a small spring strip which shortcircuits the grid circuit of V6 to chassis when the "Off" key is depressed.

\$23, \$26 are the bass boost switches

ganged with the tone control R37.

Aerial Connections.—The receiver provided with an internal dipole for F.M. reception and a rotatable ferrite rod aerial for M.W. and L.W. reception. The aerial input circuit is provided with six input sockets and a change-over link to provide for the use of various combinations of internal and external F.M. and A.M. aerials. A table showing the connections for these various combinations appears below. The socket numbers correspond with those used in the circuit diagram and in the plan illustration above.

Tuning Drive Cord.—Two lengths of

nylon braided glass yarn are required for

a new tuning drive, a short length of 65cm (26in) and a longer length of 98cm These are labelled short cord and long cord respectively in the sketch of the tuning drive system at the top of columns 4 and 5.

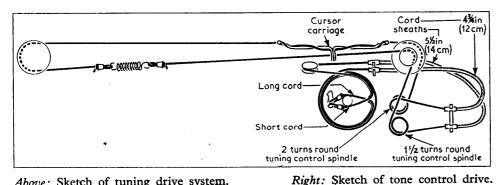
Anchor one end of the long cord to the lug in the drive drum and take it 13 turns clockwise round the drum. Thread the shorter cord sheath on the cord. Anchor one end of the short cord to the lug in the drive drum and pass it a quarter turn anti-clockwise round the drum and round the top pulley. Thread the longer cord sheath on the cord.

Wind the ends of the cords round the tuning spindle and run on as shown in the sketch, finally fitting the spring.

Tone Control Drive. - About 14in of drive wire is required for a new control drive. The control should be turned fully anti-clockwise, and a small brass collar threaded on to the wire and clamped at its centre.

The two ends of the wire should be threaded through the two small holes in the top flange of the upper drum, and pulled through so that the brass collar

Connections		Socket Numbers					
		1	2	3	4	5	3, 6, 7 (Link)
Ext. 300Ω dipole (F.M.)		Dipole	Dipole	_			6–7
Ext. A.M. aerial (A.M. and F.M.)		Aerial			Earth		3-7
Ext. 300Ω dipole (A.M. and F.M.)		Dipole	Dipole	_	Earth		3-7
Ext. 300Ω dipole (F.M.) Ext. A.M. aerial (A.M.)		Dipole	Dipole	Aerial	Earth	! !	6-7
Ext. 75Ω dipole (F.M.)		Dipole			Dipole		6-7
Ext. 75Ω dipole (A.M. and F.M.)	·	Dipole		_	Dipole	Earth	3-7
Ext. 75Ω dipole (F.M.) Ext. A.M. aerial (A.M.)		Dipole		Aerial	Dipole	Earth	6–7



Above: Sketch of tuning drive system.

Scale Lamp.—This is a 6.2 V, 0.3 A tubular lamp with an S.B.C. base.

rests between the two holes on the front of the drum flange. The two ends of the wire should then be run as indicated in the sketch in column 6, finally pulling the ends of the wire through the holes in the lower drum and clamping a brass collar on each. The wire should be taut.

Internal Aerial Drive Cord .- An overall length of about 20in of nylon braided glass yarn is required for a new drive cord which should be run as shown in the sketch at the foot of column 7.

With the control knob at the centre of its rotation, the stud on the control spindle should be at the top. With the knob in this position, the axis of the internal A.M. aerial should be parallel to the edge of the chassis, with the stud on its shaft towards the front of the chassis.

Make the cord up to the dimensions shown in the sketch and with the internal A.M. aerial set to its mid-position, pass the middle loop on the cord over the stud on the aerial shaft. Take the longer end of the cord and wind it three turns anticlockwise (viewed from above) round the shaft. Run on as indicated in the sketch, finally taking the other end of the cord and winding it  $1\frac{1}{2}$  turns clockwise round the shaft and hooking it to the spring.

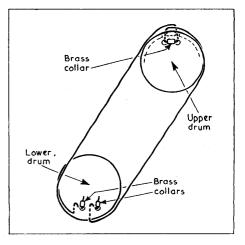
### VALVE ANALYSIS

Valve voltages given in the table below are those derived from the manufacturers' information. They were measured with a valve voltmeter when the receiver was operating from A.C. mains of 245V. Except where otherwise indicated, the receiver was switched to M.W. Chassis was the negative connection in every case.

The voltage measured across C61 was 285V for A.M. operation and 190V for F.M. operation.

Valve	Anode V	Screen V	Cath. V
vi nagar (a	150§		2§
V1 ECC85 { a b	120\$		i —
vo rottoi (a	120**		_
V2 ECH81 { a b	225††	70	
V3 EBF80	195	75	ļ
V4 EF85	185	85	
WE TARGOO (a, b			
V5 EABC80 $\begin{cases} a, b \\ c \end{cases}$	76		
V6 EL84	245	285‡‡	7
V7 EZ80	230*		285†
T.I. EM80	_		<u> </u>

\* A.C., each anode. † Cathode current, 190 mA (A.M.), 220 mA (F.M.). § Receiver switched to F.M. \*\* Zero (F.M.). †† 165 (F.M.). ‡‡ 250 (F.M.).



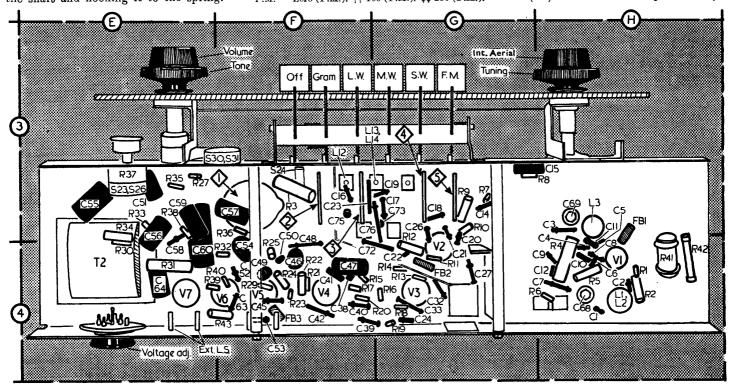
CIRCUIT ALIGNMENT

A.M. I.F. Stages.—Switch receiver to M.W. and set gang to its mid-position. Fully unscrew the cores of L21 (location reference B2), L22 (B2), L25 (C2) and L26 (B2). Connect output of signal generator, via an  $0.05\mu\text{F}$  capacitor in the "live" lead, to control grid (pin 2) of V2b and chassis.

Feed in a modulated 470 kc/s signal and adjust the cores of L26, L25, L21 and L22 in that order for maximum output. Finally re-adjust the core of L25 for maximum but do not disturb other cores.

1.F. Filter .- Fully unscrew the cores of L13 (G3) and L14 (B1). Connect the signal generator output, via a dummy aerial, to sockets 3 and 4 (A and E respectively) on the aerial panel. Feed in a 470 kc/s signal and adjust the core of L13 (G3) for minimum output.

Short-circuit the internal aerial coils L10, L11 (B1, B2), and adjust the core of L14 (B1) for minimum output. Re-adjust



Underside view of chassis. The waveband/tone switch units in the diagrams at the foot of col. 9 are identified in locations F3, G3

the core of L13 for minimum output. Remove short-circuit from L10, L11.

A.M. R.F. and Oscillator Stages .-Check that, with the gang at minimum capacitance, the cursor coincides with the datum mark at the low wavelength end of

the M.W. tuning scale.

S.W.—Switch receiver to S.W. and tune to 46.4m. With signal generator output connected, via a dummy aerial, to aerial sockets 3 and 4, feed in a 46.4m (6.47 Mc/s) signal and adjust the cores of L17 (B1) and L9 (B1) for maximum output. Tune receiver to 25.6m, feed in a 25.6m (11.73 Mc/s) signal and adjust C25 (B2) and C71 (B1) for maximum output.

M.W.—Switch receiver to M.W. and turn gang to maximum capacitance. Short-circuit L10, L11 and feed in a 581.5m (516~kc/s) signal. Adjust the core of L18 (C1) for maximum output. Tune receiver to 200m, feed in a 200m (1,500 kc/s) signal and adjust C75 (C1) for

maximum output.

Remove short-circuit from L10, L11. Tune receiver to 475m, feed in a 475m (630 kc/s) signal and adjust the inductance of L10 (B1) for maximum output by sliding the coil along the ferrite rod. Tune receiver to 200m, feed in a 200m (1,500 kc/s) signal and adjust C73 (B1) for maximum output.

L.W.—Switch receiver to L.W., tune to 1,750m and short-circuit L10, L11. Feed in a 1,750m (171.5 kc/s) signal and adjust C76 (G3) for maximum output. Remove short-circuit from L10, L11 and at the same frequency, adjust the inductance of L11 (B2) for maximum output by sliding the coil along the ferrite rod.

L.W. Image Filter.—Switch receiver to L.W. and tune to 1,304m. Screw the core of L12 (C1) fully in to the coil former. With the signal generator output connected to aerial sockets 3 and 4, feed in a 1,170 kc/s (256.4m) signal and unscrew the core of L12 for minimum output, pass-

ing first through a maximum peak.

F.M. I.F. Stages.—Switch receiver to F.M. and turn gang to maximum capacitance. Connect valve voltmeter, via a  $100k\Omega$  resistor, across **C49** (F4), and connect output of signal generator, via a 1,500pF capacitor in "live" lead, to control grid (pin 2) of **V3** and chassis. Turn volume control to minimum. During the

following adjustments, it is important that the voltage across C49 should not exceed 6-8V, and the output of the signal generator should be adjusted to keep the voltage below this level.

Connect  $47k\Omega$  damping resistor across L23, and, feeding in an unmodulated 10.7 Mc/s signal, adjust the core of L24 (C2) for maximum output. Transfer damping unit from L23 to L24, and adjust the core of L23 (B2) for maximum output. Re-

move damping unit.

Adjust the core of L27 (C2) for maximum output, and then adjust the signal generator output to give an output reading of 8V across C49.

Connect valve voltmeter to junction of R23, C46 (F4) and to chassis. Adjust the core of L28 (C2) for a 4V reading on the meter. Re-connect valve voltmeter across C49. Transfer live signal generator lead to control grid (pin 2) of V2b.

Connect damping unit across L20 and adjust the core of L19 (B2) for maximum output. Transfer damping unit to L19 and adjust the core of L20 (B2) for maximum output. Remove damping unit.

Transfer live signal generator lead to anode (pin 1) of V1b. Connect damping unit across L7 and adjust the core of L6 (A2) for maximum output. Remove damping unit and adjust the core of L7 (A2)

for maximum output.

Adjust the output of the signal generator to give an 8V reading across C49. Tune the signal generator around 10.7 Mc/s, and check that the maximum reading does not exceed 8.5V and that it occurs between 10.67 Mc/s and 10.73 Mc/s. If the I.F. response does not fall within these limits, the F.M. I.F. alignment adjustments should be repeated.

F.M. R.F. and Oscillator Stages .-With the receiver still switched to F.M., tune it to 8 on the F.M. logging scale. Adjust C69 (H3) to half maximum capacitance and adjust C68 (H4) to minimum

capacitance. Screw the core of L5 (A2) fully out, and screw core of L3 (A1) halfway out of its coil former. Connect signal generator output to aerial sockets 1 and 2.

With the valve voltmeter connected across C49, feed in an unmodulated 87.5 Mc/s signal and adjust the cores of L5 and L3 for maximum output.

Tune receiver to 100 Mc/s, and, feeding in an 87.5 Mc/s signal, adjust C69 for maximum output (setting it to the first peak from minimum capacitance).

Tune receiver to 87.5 Mc/s and, feeding in an 87.5 Mc/s signal, re-adjust the core of L3 for maximum output.

Tune receiver to  $100\,\mathrm{Mc/s}$ , and, feeding in an 87.5 Mc/s signal, adjust C68 for maximum output.

Switch Table

Sw.	Off	Gram	L.W.	M.W.	S.W.	F.M.
S1	000     0     0   0   0   0   0   0   0	С	С	C	_	C
S2	ç	C		00       0   0   0   0   0   0   0   0	ccc     c   ccc   ccc   c   cc   ccc	000 00 0         00     0   0   0   00
S4					Ğ	
S5	_	-			_	C
S6		_		_	_	C
S7	С	С	С	C	С	_
89	_		_		C	
S10			C			-
S11	_			-	C	i —
S12	_	_	_	_	C	0
S14			_			č
815	С	С	С	С	С	_
S16	Ç	C	Ç	C	Ç	-
817	C	C	C	C	C	0
S19	C	C	C	С	C	
S20		C				_
S21	С	_	C	C	С	C
S22 S24	C	C			_	
S25	č	C	C	C	C	-
S27	C	C	C	C	C	-
S28	_	_	_	_		C
829	C	6	Č	C	Č	C
\$1 \$2 \$3 \$3 \$4 \$5 \$6 \$57 \$88 \$95 \$10 \$11 \$12 \$13 \$14 \$15 \$15 \$17 \$18 \$17 \$19 \$17 \$18 \$17 \$19 \$19 \$19 \$19 \$11 \$11 \$11 \$11 \$11 \$11	_	000       0           0   000   00   0   00   000	0 0   0   0   0   0   0   0   0   0   0	č	č	Č

Right: Diagram of waveband switches. Below: Sketch of internal aerial drive cord system.

